PRELIMINARY GEOTECHNICAL INVESTIGATION
PROPOSED RESIDENTIAL SUBDIVISION
GREY ROAD 21
TOWN OF BLUE MOUNTAINS, ONTARIO

for
ROYALTON HOMES INC.

PETO MacCALLUM LTD.
25 SANDFORD FLEMING DRIVE
UNIT 2
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PML Ref.:  18CF004
Report:  1
June 2018
Dear Mr. Chaaya

Preliminary Geotechnical Investigation
Proposed Residential Subdivision
Grey Road 21
Town of Blue Mountains, Ontario

Peto MacCallum Ltd. (PML) is pleased to present the results of the preliminary geotechnical investigation recently completed at the above noted project site. Authorization for this work was provided by Mr. J. Acres of C.C. Tatham & Associates Ltd. (CCT) in an email dated March 19, 2018, on behalf of the Client.

A 150 to 200 unit residential subdivision is proposed for the approximate 21 ha parcel of land just north of the Scandinave Spa on the west side of Grey Road 21 in the Town of Blue Mountains. A concept plan for the site has not been established at this time, however, full site servicing and paved roads are proposed.

A preliminary geotechnical investigation has been requested to determine the general subsurface conditions at the site, and based on this information, provide preliminary assessment of the geotechnical conditions for preliminary planning and design of the proposed residential subdivision, including earthworks, house foundations, service installation and pavement design.

A limited chemical testing program was included with the geotechnical work to check the geoenvironmental quality of the site soils in order to provide comments regarding on-site reuse or off-site reuse/disposal options for excess excavated soil.

The comments and recommendations provided in this report are based on the site conditions as revealed in a limited number of boreholes and test pits at the time of the investigation. Design is in the conceptual stages and the details of the development plans, including final grades were not available at the time of this study. Accordingly, the comments and recommendations provided in this report are general in nature and suitable only for preliminary design and planning purposes. When design details are available, supplementary investigation and analysis will be required to finalize the geotechnical recommendations.
INVESTIGATION PROCEDURES

The field work for this investigation consisted of Boreholes 2 to 4, 7 and 8, drilled to 6.2 to 6.5 m depth on April 20 and 23, 2018 and Test Pits 1, 5 and 6, excavated to 2.9 to 3.0 m depth on May 11, 2018. Borehole and Test Pit locations are shown on the Borehole/Test Pit Location Plan, Drawing 1, appended. It is noted that Boreholes 1, 5 and 6 were inaccessible with a drill rig. Test pits were carried out at the borehole locations and the numbering system was kept the same.

The locations of the boreholes and test pits were established in the field by PML during a site meeting with the Client and CCT. Co-ordination of clearances of underground utilities was provided by PML. Boreholes were drilled and test pits excavated cognizant of underground utilities.

The boreholes were advanced using continuous flight solid stem augers, powered by a track mounted D-50 drill rig, equipped with an automatic hammer, supplied and operated by a specialist drilling contractor working under the full time supervision of a member of our engineering staff.

The test pits were excavated using a track mounted excavator, operated by an excavating company working for the Client, supervised by a member of our engineering staff.

Representative samples of the subgrade soils in the boreholes were recovered at frequent depth intervals for identification purposes using a conventional split spoon sampler. Standard penetration tests were carried out simultaneously with the sampling operations to assess the strength characteristics of the substrata. The ground water conditions in the boreholes were assessed during drilling by visual examination of the soil samples, the sampler, and drill rods, as the samples were retrieved and measurement of the water level in the open boreholes, if any. The topsoil thicknesses at the surface in the boreholes were measured.

In the test pits the topsoil thickness was measured and the subsurface soil and ground water conditions were logged. Samples of the subgrade units were collected for identification purposes.
Piezometers comprising 19 mm diameter pipe (slots cut in bottom 1.5 m) with filter sand, bentonite seal and above grade protective casing were installed in three of the boreholes. A standpipe comprising 19 mm diameter pipe (slots cut in bottom 1.0 m) and native backfill was installed in one test pit. As per O.Reg. 903, the piezometers and standpipe become the property of the Owner and will have to be decommissioned when no longer required. PML would be pleased to assist in this regard.

A year long ground water level monitoring program is being conducted by PML and results will be provided under separate cover.

The boreholes without piezometers were decommissioned as per O.Reg. 903. The test pits were backfilled with excavated material.

Ground surface elevations of the boreholes and test pits were provided by CCT.

All recovered soil samples were returned to our laboratory for moisture content determinations and detailed examination to confirm field classification. Grain size analyses were carried out on three soil samples with accompanying Atterberg Limits testing. The results are displayed on Figures 1 to 3, appended.

Three soil samples from the boreholes and one from the test pits were submitted for chemical analysis. Geoenvironmental procedural protocols and analytical chemical testing results are presented and discussed later in the report.

**SITE DESCRIPTION AND SUMMARIZED SUBSURFACE CONDITIONS**

The property is flanked by the Grey Road 21 to the east, a portion of the Monterra golf course to the north, the Scandinave Spa to the south and formerly wooded lots (which have been clear-cut to accommodate new subdivisions) to the west/southwest. A densely wooded unevaluated wetland/creek identified by the Ministry of Natural Resources cuts through the centre of the site. The portion of the site west of the wetland is lightly wooded, while east of the wetland/creek the site comprises farmland. The site has about 8 m of relief, based on the boreholes, dropping from the southwest to the northeast.
Reference is made to the appended Log of Borehole sheets for details of the subsurface conditions, including soil classifications, topsoil thicknesses, inferred stratigraphy, Standard Penetration N values (N-Values), ground water observations, piezometer installation details and the results of laboratory water content determinations and Atterberg Limits testing.

Reference is also made to the appended Log of Test Pit sheets for details of the subsurface conditions, including soil classifications, stratigraphy, ground water observations, standpipe installation details and the results of laboratory water content determinations and Atterberg Limits testing.

Due to the soil sampling procedures and limited sample size, the depth demarcations on the borehole logs must be viewed as "transitional" zones between layers, and cannot be construed as exact geologic boundaries between layers. PML should be retained to assist in defining the geologic boundaries in the field during construction, if required.

The stratigraphic profile of the site comprises topsoil, locally overlying sand, over a major sand and silt layer, over clayey sandy silt till, locally underlain by a silt deposit.

**Topsoil**

A 100 to 400 mm thick layer of silty sand to sand topsoil was encountered at the surface of all boreholes and test pits.

**Sand**

A layer of sand with trace to some silt and trace gravel was noted below the topsoil in Boreholes 4 and 8, at the east end of the site, extending to 2.1 m depth (elevation 205.7 to 207.9). The layer was very loose to compact (N Values of 3 to 17) and moist to wet with depth, with moisture contents of 9 to 24%.
Silt and Sand

Underlying the topsoil, locally the sand unit in the east, a major sand and silt deposit was encountered in all boreholes and test pits, extending to 0.7 to 2.9 m depth (elevation 206.9 to 214.75) in Boreholes 2, 3 and 7 and Test Pits 1, 5 and 6, and to the 6.4 m depth of exploration in Boreholes 4 and 8. The deposit comprised silty fine sand to fine sandy silt, with trace clay and locally some gravel or trace organics noted. A sample of the material was submitted for grain size analysis and the results are presented on Figure 1, appended. Atterberg Limits testing showed the material to be non-plastic. The layer was judged to be loose in the test pits and was revealed as loose to very dense with depth in the boreholes. The unit was typically very moist to wet with depth, with moisture contents ranging from 11 to 24%.

Clayey Sandy Silt Till

Underlying the sand and silt in Boreholes 2 and 7 and Test Pits 1, 5 and 6, a clayey sandy silt till deposit was encountered, being penetrated at 5.5 m depth (elevation 204.3) in Borehole 7, and continuing to the 2.9 to 6.2 m depth of drilling/excavation in Borehole 2 and Test Pits 1, 5 and 6. A sample of the material was submitted for grain size analysis and the results are presented on Figure 2, appended. Accompanying Atterberg Limits testing showed the material to have a plastic limit of 11% and a liquid limit of 19%. The deposit was very stiff to hard (N Values greater than 50 in boreholes). The material was generally drier than plastic limit, locally about plastic limit with water contents of 6 to 13%. Wet layers were noted in the till in the test pits, as seepage was observed.

Silt

A localized deposit of silt was encountered in Boreholes 3 and 7 (central/east part of the site) beneath the till or sand and silt, extending to the 6.4 to 6.5 m depth of exploration. The silt was very dense with N Values greater than 50. A sample of the material was submitted for gradation and the results are presented on Figure 3, appended. Atterberg Limits testing showed the silt to be non-plastic. The material was very moist to moist with water contents of 12 to 18%.
Ground Water

The first ground water strike (water first noticed during drilling), the water level or wet cave observations in the boreholes/test pits upon completion, and the water levels in the piezometers/standpipe on May 4 and June 11, 2018 are noted in the table below:

<table>
<thead>
<tr>
<th>BOREHOLE / TEST PIT</th>
<th>FIRST GROUND WATER STRIKE</th>
<th>SEEPAGE / WATER / WET CAVE LEVEL UPON COMPLETION</th>
<th>WATER LEVEL IN PIEZOMETERS MAY 4, 2018</th>
<th>WATER LEVEL IN PIEZOMETERS / STANDPIPE JUNE 11, 2018</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>2.9 / 209.8</td>
<td>Seepage at 2.9 / 209.8</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>2</td>
<td>1.2 / 209.8</td>
<td>Water at 0.1 / 210.9</td>
<td>-1.0 / 212.0</td>
<td>-0.6 / 211.6</td>
</tr>
<tr>
<td>3</td>
<td>0.9 / 208.7</td>
<td>Water at 2.7 / 206.9</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>4</td>
<td>2.0 / 205.8</td>
<td>Wet Cave at 1.8 / 206.0</td>
<td>1.2 / 206.6</td>
<td>1.9 / 205.9</td>
</tr>
<tr>
<td>5</td>
<td>2.9 / 212.6</td>
<td>Seepage at 2.9 / 212.6</td>
<td>--</td>
<td>0.5 / 215.0</td>
</tr>
<tr>
<td>6</td>
<td>1.0 / 211.0</td>
<td>Seepage at 1.0 / 211.0</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>7</td>
<td>0.8 / 209.0</td>
<td>Water at 0.6 / 209.2</td>
<td>0.4 / 209.4</td>
<td>1.2 / 208.6</td>
</tr>
<tr>
<td>8</td>
<td>1.5 / 208.5</td>
<td>Water at 1.8 / 208.2</td>
<td>--</td>
<td>--</td>
</tr>
</tbody>
</table>

* - Negative water level is above existing grades.

Ground water was generally encountered within the more pervious sand, or sand and silt deposits, perched within 1 to 2 m of the ground surface, over the less pervious clayey sandy silt till.

The piezometer in Borehole 2 also demonstrates the ground water is locally under some artesian pressure, as evidenced by the water levels noted above existing site grades at this location.

A year-long water level monitoring program has been undertaken in an attempt to gain an appreciation for the seasonal variations of the ground water table. Results will be provided under separate cover.

Ground water levels are subject to seasonal variation and will fluctuate in response to precipitation.
GEOTECHNICAL ENGINEERING CONSIDERATIONS

General

A 150 to 200 unit residential subdivision is proposed for the approximate 21 ha parcel of land just north of the Scandinave Spa on the west side of Grey Road 21 in the Town of Blue Mountains. A concept plan for the site has not been established at this time, however, full site servicing and paved roads are proposed.

The site is characterized by topsoil, locally overlying sand, over a major sand and silt layer, over clayey sandy silt till, locally underlain by a silt deposit. Ground water levels were typically perched within 1 to 2 m of the ground surface. Local artesian ground water is present.

The soils are relatively competent and will provide adequate bearing for residences and other infrastructure. The high ground water level will impact construction and if basements are proposed grades will need to be raised.

The comments and recommendations provided in this report are preliminary in nature and are based on the subsurface conditions as revealed in a limited number of boreholes and test pits at the site. Details of the development plans, including layout and final grades were not available at the time of this study. Accordingly, the comments and recommendations provided in this report are general in nature, and suitable only for preliminary design and planning purposes. When design details are available, supplementary investigation and analysis will be required to finalize the geotechnical recommendations.

Site Grading and Engineered Fill

Grading at the site has yet to be established however it is anticipated that some cut/fill operations will be carried out. The site currently maintains about 8 m of relief, dropping from the southwest to the northeast.
Any upfilling under structures must be constructed as engineered fill. Topsoil and very loose to loose soil should be removed and engineered fill can be placed on the native very stiff to hard/compact to very dense soils encountered throughout the site typically below 0.5 to 1.0 m locally 1.5 m depth. Further recommendations can be provided, if required.

**Foundations**

House foundations can typically be supported on conventional spread and strip footings founded on the very stiff to hard/compact to very dense native soils typically encountered below 0.5 to 1.0 m depth, locally 1.5 m deep, across the site.

A net geotechnical bearing resistance at Serviceability Limit State (SLS) of 100 to 150 kPa, and a factored bearing resistance at Ultimate Limit State (ULS) of 150 to 225 kPa are available for design. Higher bearing capacities are available at increased depths.

Footings can also be supported on engineered fill where a net geotechnical bearing resistance at SLS of 150 kPa and factored bearing resistance at ULS of 225 kPa can be assumed for design.

The geotechnical bearing resistance at SLS is based on 25 mm or settlement in the bearing stratum with differential settlement of 75% of the value.

Footings subject to frost action should be provided with a minimum 1.2 m of earth cover or equivalent.

It is noted that if the subgrade soils are wet in-situ or allowed to become wet due to weather they will become easily disturbed under construction or pedestrian traffic. If the footing subgrade is disturbed it will have to be sub-excavated. As such, the contractor should adopt construction methodology and equipment to suit. Concrete skim coats may be required in some areas.

Prior to placement of structural concrete, all founding surfaces should be reviewed by PML to verify the design bearing capacity is available, or to reassess the design parameters based on the actual conditions revealed in the excavation.
**Basement Walls and Floor Slabs**

It is currently unknown if basements are planned.

Basement floor slabs should be established a minimum 0.5 m above the ground water level. In general grades will need to be raised in order to accommodate basements due to the high ground water levels.

A year long ground water level monitoring program is currently being conducted. Results will be provided under separate cover.

Basement walls must be designed to resist the unbalanced horizontal earth pressure imposed by the backfill adjacent to the walls. Also, basement wall backfill should comprise free draining granular material conforming to OPSS Granular B. Further recommendations can be provided if required.

Basement floor slab-on-grade construction is feasible on native soils or locally engineered fill. In general, a minimum 150 mm thick base layer of crushed stone (nominal 19 mm size) is recommended directly under the slab.

Exterior grades should be established to promote surface drainage away from the buildings.

**Site Servicing**

Design details were not finalized at the time of this report. However for purposes of this report it is assumed service inverts will be a maximum 3.0 m below existing grade.

Native clayey sandy silt till, silt, or sand and silt is expected at invert levels which is considered satisfactory for pipe support.

Native backfill is generally satisfactory for trench backfill, however, the high ground water table will require most of the soil to be dried out in order to achieve compaction.
Backfill in trenches should comprise select inorganic site soil at a suitable moisture content and be placed in maximum 200 mm thick loose lifts compacted to at least 95% Standard Proctor maximum dry density to minimize post construction settlement in the backfill.

Earthworks operations should be inspected by PML to verify subgrade preparation, backfill materials, placement and compaction efforts and ensure the specified degree of compaction is achieved throughout.

**Excavation and Ground Water Control**

Finished site grades are not known at this time.

Excavation is anticipated to a maximum of 3 m depth and will encounter topsoil and the underlying native sand, sand and silt, and clayey sandy silt till units. Perched ground water is anticipated within 1 to 2 m of the ground surface. Harder digging and the presence of cobbles and boulders should be anticipated in the till deposit.

Subject to effective ground water control, the site soils should be considered as Type 3 soil requiring excavation side walls to be constructed at no steeper than one horizontal to one vertical (1H:1V) from the base of the excavation in accordance with the Occupational Health and Safety Act.

In general for excavation to 1.0 to 1.5 m seepage volumes are expected to be handled by conventional sump pumping techniques. Deeper excavation or excavation adjacent the existing wetland/creek or in lower lying areas of the site will yield higher seepage volumes which will necessitate more aggressive ground water control measures such as pumping from keg wells, or possibly the use of well points.

Excavation should be carried out during the dry time of the year to minimize ground water control requirements.
A year-long water level monitoring program has been undertaken in an attempt to gain an appreciation for the seasonal variations of the ground water table. Results will be provided upon its projected completion in April 2019.

**Pavement Design and Construction**

The location of the roadways have yet to be finalized and grading is still to be determined. Based on the boreholes and test pits, it is anticipated that the pavement subgrade will comprise near surface soil (moderately to highly frost susceptible native sand/sand and silt, typically very moist or wet). The following preliminary pavement structure thicknesses are recommended and should be reviewed when grading/subgrade conditions have been finalized:

<table>
<thead>
<tr>
<th></th>
<th>Light Duty (Local Roads)</th>
<th>Heavy Duty (Collector Roads)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Asphalt (mm)</td>
<td>90</td>
<td>110</td>
</tr>
<tr>
<td>Granular A Base Course (mm)</td>
<td>150</td>
<td>150</td>
</tr>
<tr>
<td>Granular B Subbase Course (mm)</td>
<td>400</td>
<td>600</td>
</tr>
<tr>
<td>Total Thickness (mm)</td>
<td>640</td>
<td>860</td>
</tr>
</tbody>
</table>

**Geotechnical Review**

It is recommended that the final drawings be submitted to PML for general geotechnical review for compatibility with the site conditions and the recommendations provided in this report.

The comments and recommendations provided in the report are based on the site conditions as revealed in a limited number of boreholes and test pits at the time of the investigation. Further, details of the development plans, including layout and final grades were not available at the time of this study. Accordingly, the comments and recommendations provided in this report are general in nature and suitable only for preliminary design and planning purposes. When design details are available, they should be submitted for review by PML to verify the applicability of the recommendations presented in this report and may require additional investigation and/or analysis.
GEOENVIRONMENTAL CONSIDERATIONS

A limited chemical testing program was carried out to check the geoenvironmental quality of the soil at selected sampling locations in order to provide comments regarding on site reuse or off-site disposal options for excess excavated soil.

A Phase One Environmental Site Assessment (ESA) was not within the scope of work for this assignment. Accordingly, soil impairment that has not been identified by the limited chemical testing program may exist at the site. The limited chemical testing program does not constitute an Environmental Site Assessment as defined under the Environmental Protection Act and O. Reg. 153/04, as amended.

Chemical Testing Protocols

As part of the geoenvironmental procedural protocol, all recovered soil samples were examined for visual and olfactory evidence of potential contamination. It is noted that none of the samples contained olfactory evidence of contamination.

The selected geoenvironmental soil samples were placed in laboratory air tight glass containers and stored in an insulated cooler for transportation to our laboratory for detailed visual examination.

Soil samples were submitted for chemical analysis to a Canadian Association for Laboratory Accreditation Inc. (CALA) accredited laboratory. The chemical analyses conducted were in accordance with the O. Reg. 153/04, as amended Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act dated March 9, 2004, amended as of July 1, 2011.

For general environmental quality characterization, soil samples were tested for the following analyte groups:

- Metals and Inorganics;
- Petroleum Hydrocarbons (F1 to F4 fractions).
The following soil samples were submitted for chemical testing:

- Borehole 2 SS 1, (sand and silt – 0.1 to 0.6 m)
- Borehole 4 SS 2, (sand – 0.8 to 1.4 m)
- Borehole 7 SS 3, (sand and silt – 1.5 to 2.1 m)
- Test Pit 5 GS 2, (till – 0.7 to 2.0 m)

**Site Condition Standards**

In general, the applicable environmental quality guidelines depend on the site location, land use, soil texture and source of potable water at the site. In this regard, PML selected the Generic Criteria of the O. Reg. 153/04, as amended, Soil, Ground Water and Sediment Standards for Use Under Part XV.1 of the Environmental Protection Act dated April 15, 2011.

Based on Sections 41 and 43 of O.Reg. 153/04, as amended, and a review of readily available information, the site is considered a sensitive site. The subject site is considered sensitive due to the presence of an area of natural significance. An unevaluated wetland identified by the Ministry of Natural Resources (MNR), traverses the centre of the site.

Further, the site was reviewed against the County of Grey’s Intake Protection Zones (Map 2, June 2013) and other maps for watercourses and private wells as part of the protocol to determine the applicable Site Condition Standards (SCSs) for the site. In this regard, the site is not within an intake protection zone, however, has private drinking water wells within 250 m of the site based on the MOECC well records website, and is within 30 m of a water body as a creek/wetland passes through the middle of the site.

Based on the above reviews, the criteria of Table 1: Full Depth Background Site Condition Standards, Table 1 SCSs, are considered applicable to the site.
Analytical Findings and Conclusions

The Certificates of Analyses for Chemical Testing are included in Appendix A.

On-Site Reuse

In summary, the concentration of the tested parameters in the submitted soil samples were in conformance with the Table 1 SCSs applicable to the site. Accordingly, based on the testing results, excavated soil can be reused on-site, subject to geotechnical requirements.

It should be noted that there is no legal imperative to remove or treat soil that exceeds the applicable SCSs provided it is demonstrated that there is no off-site impact or adverse effect. If contaminated soil is left on-site, the landowner assumes liability associated with the site contamination and potential of off-site contamination. The liability concerns could include potential scrutiny from the MOECC and the public, potential for decreased value for the land, and issues during potential divesting of the property due to environmental liability concerns on the part of the future owners or their financiers/insurers.

It should also be noted that the soil conditions between and beyond the sampled locations may differ from those encountered during this assignment. PML should be contacted if impacted soil conditions become apparent during future development to further assess and appropriately handle the materials, if any, and evaluate whether modifications to the conclusions documented in this report are necessary.

This assessment is subject to the Statement of Limitations that is included with this report (Appendix B) which must be read in conjunction with the report.

Off-Site Reuse/Disposal

O. Reg. 153/04, as amended has nine tables outlining SCSs (Tables 1 to 9) for evaluating Environmental Soil Characteristics. These tables are further divided based on land use. The chemical testing results from this project were compared to the various SCSs to evaluate where the excess soil can be transported.
Based on the limited chemical testing results the site soil meets the most stringent SCSs (Table 1) and can be transported to any landsite, subject to approval of receiving site authority.

Alternatively, excess excavated soil can be transported to a landfill site, however, additional testing for Toxicity Characteristic Leaching Procedure (TCLP) will be required, in accordance with Ontario Regulation 347, Schedule 4, as amended to Ontario Regulation 558/00, dated March 2001.

When transporting excavated site soil to another site the following are recommended:

- The work must be completed in accordance with local by-laws governing soil movement and/or placement at other sites;
- All analytical results and environmental assessment reports must be fully disclosed to the receiving site owners/authorities and they have agreed to receive the material;
- The applicable SCSs for the receiving site have been determined, as confirmed by the environmental consultant and the SCSs are consistent with the chemical quality of the soil originating at the source site;
- Transportation and placement of the surplus soil is monitored by the environmental consultant to check the material is appropriately placed at the pre-approved site;
- The receiving site must be arranged and/or approved in advance of excavation in order to avoid delays during construction. As well, it is noted the chemical testing requirements for various receiving sites is site-specific and additional testing may be required, beyond that provided in this limited sampling and testing report;
- The excavation work should be conducted in accordance with a written Soil Management Plan prepared by a qualified professional to ensure that all surplus excavated material is tested and managed appropriately, and that imported fill material is of suitable quality and meets the SCSs applicable to the site. Reuse of surplus excavated soil on site is also subject to acceptance for reuse by the geotechnical consultant at the time of construction based on geotechnical considerations;
- Additional sampling and chemical testing should be carried out during construction to verify the chemical quality of the excess soil to assess the appropriate management/disposal options for the actual soil leaving the site;
• It is recommended that transportation of fill material from the Source Site (s) to the Receiving Site (s) be carried out in accordance with the MOECC document *Management of Excess Soil – A Guide for Best Management Practices* dated January 2014.

This assessment is subject to the Statement of Limitations that is included with this report (Appendix B) which must be read in conjunction with the report.
CLOSURE

We trust this report is complete within our terms of reference, and the information presented is sufficient for your present purposes. If you have any questions, or when we may be of further assistance, please do not hesitate to call our office.

Sincerely

Peto MacCallum Ltd.

Richard Blair, P.Eng.
Project Engineer, Geotechnical Services

Geoffrey R. White, P.Eng.
Associate
Manager, Geotechnical and Geoenvironmental Services

Enclosure(s):
Figures 1 to 3 – Particle Size Distribution Charts
List of Abbreviations
Log of Test Pit No’s 1, 5, 6
Log of Borehole No’s 2 to 4, 7, 8
Drawing No. 1 – Borehole/Test Pit Location Plan
Appendix A - Certificates of Analyses for Chemical Testing
Appendix B - Statement of Limitations
REMARKS:
Borehole 3, SS 3, 1.5 to 1.9 m depth; SAND AND SILT, Trace Clay; Non-Plastic

SYMBOL | BH No. | SAMPLE No. | DEPTH (ft) | WL | WP | PI
--- | --- | --- | --- | --- | --- | ---
● | 3 | 3 | 5-7 | |

REMARKS: Borehole 3, SS 3, 1.5 to 1.9 m depth; SAND AND SILT, Trace Clay; Non-Plastic
REMARKS: Test Pit 5, GS 3, 2.0 to 2.9 m depth; Clayey Sandy Silt Till, Trace Gravel; Plastic Limit: 11%; Liquid Limit: 19%;
REMARKS: Borehole 3, SS 5, 3.1 to 3.5 m depth; SILT, Some Sand, Trace Clay; Non-Plastic
LIST OF ABBREVIATIONS

PENETRATION RESISTANCE

Standard Penetration Resistance N: - The number of blows required to advance a standard split spoon sampler 0.3 m into the subsoil. Driven by means of a 63.5 kg hammer falling freely a distance of 0.76 m.

Dynamic Penetration Resistance: - The number of blows required to advance a 51 mm, 60 degree cone, fitted to the end of drill rods, 0.3 m into the subsoil. The driving energy being 475 J per blow.

DESCRIPTION OF SOIL

The consistency of cohesive soils and the relative density or denseness of cohesionless soils are described in the following terms:

<table>
<thead>
<tr>
<th>CONSISTENCY</th>
<th>N (blows/0.3 m)</th>
<th>c (kPa)</th>
<th>DENSENESS</th>
<th>N (blows/0.3 m)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Very Soft</td>
<td>0 - 2</td>
<td>0 - 12</td>
<td>Very Loose</td>
<td>0 - 4</td>
</tr>
<tr>
<td>Soft</td>
<td>2 - 4</td>
<td>12 - 25</td>
<td>Loose</td>
<td>4 - 10</td>
</tr>
<tr>
<td>Firm</td>
<td>4 - 8</td>
<td>25 - 50</td>
<td>Compact</td>
<td>10 - 30</td>
</tr>
<tr>
<td>Stiff</td>
<td>8 - 15</td>
<td>50 - 100</td>
<td>Dense</td>
<td>30 - 50</td>
</tr>
<tr>
<td>Very Stiff</td>
<td>15 - 30</td>
<td>100 - 200</td>
<td>Very Dense</td>
<td>&gt; 50</td>
</tr>
<tr>
<td>Hard</td>
<td>&gt; 30</td>
<td>&gt; 200</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

WTLL Wetter Than Liquid Limit
WTPL Wetter Than Plastic Limit
APL About Plastic Limit
DTPL Drier Than Plastic Limit

TYPE OF SAMPLE

<table>
<thead>
<tr>
<th>SS</th>
<th>Split Spoon</th>
<th>ST</th>
<th>Slotted Tube Sample</th>
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<tbody>
<tr>
<td>WS</td>
<td>Washed Sample</td>
<td>TW</td>
<td>Thinwall Open</td>
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<tr>
<td>SB</td>
<td>Scraper Bucket Sample</td>
<td>TP</td>
<td>Thinwall Piston</td>
</tr>
<tr>
<td>AS</td>
<td>Auger Sample</td>
<td>OS</td>
<td>Oesterberg Sample</td>
</tr>
<tr>
<td>CS</td>
<td>Chunk Sample</td>
<td>FS</td>
<td>Foil Sample</td>
</tr>
<tr>
<td>GS</td>
<td>Grab Sample</td>
<td>RC</td>
<td>Rock Core</td>
</tr>
</tbody>
</table>

PH Sample Advanced Hydraulically
PM Sample Advanced Manually

SOIL TESTS

<table>
<thead>
<tr>
<th>Qu</th>
<th>Unconfined Compression</th>
<th>LV</th>
<th>Laboratory Vane</th>
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<tr>
<td>Q</td>
<td>Undrained Triaxial</td>
<td>FV</td>
<td>Field Vane</td>
</tr>
<tr>
<td>Qcu</td>
<td>Consolidated Undrained Triaxial</td>
<td>C</td>
<td>Consolidation</td>
</tr>
<tr>
<td>Qd</td>
<td>Drained Triaxial</td>
<td></td>
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### Soil Profile

<table>
<thead>
<tr>
<th>Depth Elevation (meters)</th>
<th>Description</th>
<th>Strat Plot Number</th>
<th>Type</th>
<th>TC Values</th>
<th>Shear Strength (kPa)</th>
<th>Plastic Natural Moisture Content</th>
<th>Liquid Limit</th>
<th>Unit Weight</th>
<th>Ground Water Observations and Remarks</th>
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<tr>
<td>0.0</td>
<td>Surface Elevation 212.70</td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>0.3</td>
<td>Topsoil: Black, silty sand, trace gravel, very moist</td>
<td>1</td>
<td>GS</td>
<td>212</td>
<td></td>
<td></td>
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</tr>
<tr>
<td>1.0</td>
<td>Sand and silt: Loose, brown to grey, silty fine sand to fine sandy silt, trace clay, moist to very moist</td>
<td>2</td>
<td>GS</td>
<td>211</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2.2</td>
<td>Clvey sandy silt till: Very stiff to hard, brown, clayey sandy silt, trace gravel, cobbles and boulders, DTPL</td>
<td></td>
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<tr>
<td>3.0</td>
<td>Becoming grey, APL: wet layers</td>
<td>3</td>
<td>GS</td>
<td>210</td>
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**Notes:**
- Upon completion of test pit
- Seepage at 2.9 m
- No sidewall sloughing
LOG OF BOREHOLE NO. 2

PROJECT: Proposed Residential Subdivision
LOCATION: Grey Road 21, Town of Blue Mountains, Ontario
BORING METHOD: Continuous Flight Solid Stem Augers

SOIL PROFILE

DEPTH (m) | DESCRIPTION |
--- | --- |
0.0 | SURFACE ELEVATION 210.95 |
210.95 | TOPSOIL: Dark brown, sand, trace silt, trace gravel, wet |
2.9 | SAND AND SILT: Loose to very dense, brown, silty fine sand to fine sandy silt, trace clay, wet |
2.9 | CLAYEY SANDY SILT TILL: Hard, grey, clayey sandy silt, trace gravel, cobbles and boulders, DTPL |
4.2 | BOREHOLE TERMINATED AT 6.2 m |

SHEAR STRENGTH (kPa)

| STRAT PLOT | NUMBER | TYPE | ELEVATION (m) |
--- | --- | --- | --- |
1 | SS | 8 | 0.0 |
2 | SS | 25 | 2.9 |
3 | SS | 41 | 2.9 |
4 | SS | 74/250mm | 2.9 |
5 | SS | 50/140mm | 4.2 |
6 | SS | 92/270mm | 4.2 |
7 | SS | 50/140mm | 4.2 |

GROUNDBED OBSERVATIONS AND REMARKS

- Stick-up casing Concrete
- First water strike at 1.2 m Bentonite Seal
- 19 mm slotted pipe Filter sand
- Upon completion of auguring Water at 0.1 m Cave at 4.9 m Water Level Readings:
  - Date: 2016-05-04 Depth: 1.0 Elevation: 212.0
  - Date: 2016-05-11 Depth: -0.6 Elevation: 211.6

NOTES
1. Sample submitted for chemical testing.
LOG OF BOREHOLE NO. 3
177 506382E 4926194N

PROJECT  Proposed Residential Subdivision
LOCATION  Grey Road 21, Town of Blue Mountains, Ontario
BORING METHOD  Continuous Flight Solid Stem Augers
BORING DATE  April 23, 2018

SOIL PROFILE

<table>
<thead>
<tr>
<th>ELEV (metres)</th>
<th>DESCRIPTION</th>
<th>STRAT PLOT</th>
<th>NUMBER</th>
<th>TYPE</th>
<th>NY VALUES</th>
<th>SHEAR STRENGTH (kPa)</th>
<th>PLASTIC LIMIT</th>
<th>NATURAL MOISTURE LIMIT</th>
<th>LIQUID LIMIT</th>
<th>UNIT WEIGHT</th>
<th>GRAIN SIZE DISTRIBUTION (%)</th>
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</thead>
<tbody>
<tr>
<td>0.0</td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>1.8</td>
<td>TOPSOIL: Black to dark brown, silty sand and trace gravel, very moist</td>
<td>1</td>
<td>SS</td>
<td>4</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
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</tr>
<tr>
<td>2.0</td>
<td>SAND AND SILT: Loose to dense, brown to grey, silty fine sand to fine sandy silt, trace clay, very moist to wet</td>
<td>2</td>
<td>SS</td>
<td>40</td>
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<tr>
<td>2.1</td>
<td>SILT: Very dense, grey, silt, some sand, trace clay, very moist to moist</td>
<td>3</td>
<td>SS</td>
<td>34</td>
<td></td>
<td></td>
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<tr>
<td>207.5</td>
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<td>4</td>
<td>SS</td>
<td>68</td>
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<td>204.2</td>
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<td>5</td>
<td>SS</td>
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</tr>
<tr>
<td>203.2</td>
<td>BOREHOLE TERMINATED AT 6.4 m</td>
<td></td>
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</tr>
</tbody>
</table>

NOTES

First water strike at 0.9 m
Non plastic
Non plastic

Upon completion of augering
Water at 2.7 m
cave at 3.3 m
**LOG OF BOREHOLE NO. 4**

**PROJECT** Proposed Residential Subdivision

**LOCATION** Grey Road 21, Town of Blue Mountains, Ontario

**BORING METHOD** Continuous Flight Solid Stem Augers

**SOIL PROFILE**

<table>
<thead>
<tr>
<th>Depth (m)</th>
<th>Description</th>
<th>Strat Plt</th>
<th>Type</th>
<th>N' Values</th>
<th>SHEAR STRENGTH (kPa)</th>
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<tr>
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<td>SS</td>
<td>4</td>
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<td>206</td>
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<td>0.1</td>
<td>TOPSOIL: Black to dark brown, silty sand, trace gravel, moist</td>
<td>SS</td>
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<td>3</td>
<td>205</td>
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<tr>
<td>2.1</td>
<td>SAND: Loose to compact, brown, sand, trace silt, trace gravel, moist to wet</td>
<td>SS</td>
<td>17</td>
<td>4</td>
<td>203</td>
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<tr>
<td>3.0</td>
<td>SAND AND SILT: Dense to very dense, brown, silty fine sand to fine sandy silt, trace clay, very moist to wet</td>
<td>SS</td>
<td>33</td>
<td>5</td>
<td>204</td>
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<td>6.4</td>
<td>6 SS 83/290mm</td>
<td>SS</td>
<td>290</td>
<td>7</td>
<td>202</td>
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**GROUND WATER OBSERVATIONS AND REMARKS**

- Stick-up casing Concrete
- Bentonite Seal
- First water strike at 2.0 m
- 19 mm slotted pipe Filter sand
- Upon completion of auguring Wet cave at 1.6 m

**NOTES**

1. Sample submitted for chemical testing.
## LOG OF TEST PIT NO. 5

**PROJECT** Proposed Residential Subdivision  
**LOCATION** Grey Road 21, Town of Blue Mountains, Ontario  
**BORING DATE** May 11, 2018  
**ENGINEER** GW  
**TECHNICIAN** AT

<table>
<thead>
<tr>
<th>DEPTH ELEV. (M)</th>
<th>SOIL PROFILE</th>
<th>DESCRIPTION</th>
<th>STRAT PLOT NUMBER</th>
<th>TYPE</th>
<th>SAMPLE ELEV.</th>
<th>SHEAR STRENGTH (kPa)</th>
<th>DYNAMIC CONE PENETRATION TEST</th>
<th>GRAIN SIZE DISTRIBUTION (%)</th>
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<td>SURFACE ELEVATION 215.45</td>
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<tr>
<td>0.30</td>
<td>TOPSOIL</td>
<td>Black to brown, silty sand, trace gravel, very moist to wet</td>
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<td>GS</td>
<td>215</td>
<td>10 20 40 60 80</td>
<td>10 20 30 40</td>
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<tr>
<td>215.15</td>
<td>SAND AND SILT</td>
<td>Loose, brown, silty fine sand to fine sandy silt, some gravel, trace organics, wet</td>
<td>2</td>
<td>GS</td>
<td>214</td>
<td>10 20 40 60 80</td>
<td>10 20 30 40</td>
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<tr>
<td>214.75</td>
<td>CLAYEY SANDY SILT TILL</td>
<td>Very stiff to hard, brown, clayey sandy silt, trace gravel, cobbles and boulders, DTPL</td>
<td>3</td>
<td>GS</td>
<td>213</td>
<td>10 20 40 60 80</td>
<td>10 20 30 40</td>
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<tr>
<td>2.9</td>
<td>Becoming grey, wet layers</td>
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<td>212.6</td>
<td>TEST PIT TERMINATED AT 2.9 m</td>
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### OBSERVATIONS AND REMARKS

- Native backfill
- 19 mm slotted pipe
- Upon completion of test pit
- Seepage at 2.9 m
- No sidewall sloughing

**WATER LEVEL READINGS:**
- Date: 2018-06-11
- Depth: 0.5
- Elev: 215.0

**NOTES:** 1 - Sample submitted for chemical testing.
<table>
<thead>
<tr>
<th>Depth (m)</th>
<th>Description</th>
<th>Stratum Plot</th>
<th>Sample Type</th>
<th>Elevation Scale</th>
<th>Shear Strength (kPa)</th>
<th>Plastic Natural Limit</th>
<th>Unit Weight</th>
<th>Grain Size Distribution (%)</th>
<th>Remarks</th>
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<td>0.00</td>
<td>TOPSOIL: Black, sand, some silt, trace gravel, very moist</td>
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<tr>
<td>2.09</td>
<td>TEST PIT TERMINATED AT 2.9 m</td>
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Upon completion of augering, Seepage at 1.0 m
Sidewall sloughing at 1.0 m
LOG OF BOREHOLE NO. 7
177 556418E 492807N

PROJECT Proposed Residential Subdivision
LOCATION Grey Road 21, Town of Blue Mountains, Ontario
BORING METHOD: Continuous Flight Solid Stem Augers

DEPTH (metres) 0.0 1.0 2.0 3.0 4.0 5.0 6.0 7.0
ELEVATION 209.80

SURFACE ELEVATION 209.80

TOPSOIL: Dark brown, silty sand, trace gravel, moist
SAND AND SILT: Loose to very dense, brown, silty fine sand to fine sandy silt, trace clay, very moist to wet

CLAYEY SANDY SILT TILL: Hard, clayey sandy silt, trace gravel, cobbles and boulders, DTPL

SILT: Very dense, grey, silt, trace sand, trace clay, moist

BOREHOLE TERMINATED AT 6.5 m

NOTES 1 - Sample submitted for chemical testing.
LOG OF BOREHOLE NO. 8
177 556575E 4928104N

PROJECT: Proposed Residential Subdivision
LOCATION: Grey Road 21, Town of Blue Mountains, Ontario
BORING METHOD: Continuous Flight Solid Stem Augers

<table>
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<tr>
<th>DEPTH (metres)</th>
<th>DESCRIPTION</th>
<th>STRAT PLOT NUMBER</th>
<th>TYPE</th>
<th>TF VALUES</th>
<th>SHEAR STRENGTH (kPa)</th>
<th>PLASTIC LIMIT</th>
<th>LIQUID LIMIT</th>
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<tr>
<td>0.0</td>
<td>SURFACE ELEVATION 210.00</td>
<td>1 SS 3</td>
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<td>2.1</td>
<td>TOPSOIL: Brown, sand, trace silt, trace gravel, moist</td>
<td>2 SS 12</td>
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<td>3.0</td>
<td>SAND: Very loose to compact, brown, sand, trace to some silt, trace gravel, very moist to wet</td>
<td>3 SS 13</td>
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<td>3.1</td>
<td>SAND AND SILT: Very dense, brown, silty fine sand to fine sandy silt, very moist to wet</td>
<td>4 SS 56</td>
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<td></td>
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<td>5.0</td>
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<td>5 SS 75</td>
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<td>5.4</td>
<td></td>
<td>6 SS 83/270mm</td>
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<tr>
<td>6.4</td>
<td>BOREHOLE TERMINATED AT 6.4 m</td>
<td>7 SS 83/270mm</td>
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GROUNDFWATER OBSERVATIONS AND REMARKS
First water strike at 1.5 m
Upon completion of auguring
Water at 1.8 m
Cave at 2.7 m

NOTES
APPENDIX A

Certificates of Analyses for Chemical Testing
CERTIFICATE OF ANALYSIS
Final Report

C.O.C.: G75184

REPORT No. B18-10833 (I)
Rev. 1

Report To:
Peto MacCallum Ltd
19 Churchill Drive,
Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18
DATE REPORTED: 15-Jun-18
SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories
112 Commerce Park Drive
Barrie ON L4N 8W8
Tel: 705-252-5743
Fax: 705-252-5746

JOB/PROJECT NO.: P.O. NUMBER: 18CF004
WATERWORKS NO.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Qty</th>
<th>Site Analyzed</th>
<th>Analyst Initials</th>
<th>Date Analyzed</th>
<th>Lab Method</th>
<th>Reference Method</th>
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<tr>
<td>Cyanide</td>
<td>3</td>
<td>Kingston</td>
<td>US</td>
<td>01-May-18</td>
<td>A-CN s K</td>
<td>in house</td>
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<td>Conductivity</td>
<td>3</td>
<td>Richmond Hill</td>
<td>ABL</td>
<td>30-Apr-18</td>
<td>A-COND-02 s RH</td>
<td>MOEE3138</td>
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<td>pH</td>
<td>3</td>
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<td>ABL</td>
<td>27-Apr-18</td>
<td>A-pH-02 (rh)</td>
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<td>Chromium (VI)</td>
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<td>D-CrVI-02 s RH</td>
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<td>Holly Lane</td>
<td>PBK</td>
<td>27-Apr-18</td>
<td>D-HG-01 (o)</td>
<td>EPA 7471A</td>
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<td>Sodium Adsorption Ratio</td>
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<td>Holly Lane</td>
<td>TPR</td>
<td>27-Apr-18</td>
<td>D-ICP-01 SAR (o)</td>
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<td>Metals - ICP-OES</td>
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<td>RPE</td>
<td>27-Apr-18</td>
<td>D-ICPMS-01 (o)</td>
<td>EPA 6020</td>
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µg/g = micrograms per gram (parts per million) and is equal to mg/Kg
F1 C6-C10 hydrocarbons in µg/g, (F1-btax if requested)
F2 C10-C16 hydrocarbons in µg/g, (F2-naph if requested)
F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)
F4 C34-C50 hydrocarbons in µg/g
This method complies with the Reference Method for the CWS PHC and is validated for use in the laboratory.
Any deviations from the method are noted and reported for any particular sample.
nC6 and nC10 response factor is within 30% of response factor for toluene:
nC10, nC16 and nC34 response factors within 10% of each other:
C50 response factors within 70% of nC10+nC16+nC34 average:
Linearity is within 15%:
All results expressed on a dry weight basis.
Unless otherwise noted all chromatograms returned to baseline by the retention time of nC50.

O. Reg. 153 - Soil, Ground Water and Sediment Standards
Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Corr/Commun

R.L. = Reporting Limit
Test methods may be modified from specified reference method unless indicated by an *
Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie

The analytical results reported herein refer to the samples as received. Reproduction of this analytical report in full or in part is prohibited without prior consent from Caduceon Environmental Laboratories.

Page 1 of 3.

Christine Burke
Lab Manager
CERTIFICATE OF ANALYSIS

Final Report

REPORT No. B18-10833 (I)
Rev. 1

C.O.C.: G75184

Report To:
Peto MacCallum Ltd
19 Churchill Drive,
Barrie ON L4N 8Z5
Attention: Geoff White

DATE RECEIVED: 25-Apr-18
DATE REPORTED: 15-Jun-18
SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories
112 Commerce Park Drive
Barrie ON L4N 8W8
Tel: 705-252-5743
Fax: 705-252-5746
JOB/PROJECT NO.: P.O. NUMBER: 18CF004
WATERWORKS NO.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Units</th>
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<th>O. Reg. 153 Tbl. 1 - All</th>
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<td>Beryllium</td>
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<td>Boron</td>
<td>µg/g</td>
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<td>Cadmium</td>
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<td>µg/g</td>
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<td>92</td>
</tr>
<tr>
<td>Lead</td>
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<td>Mercury</td>
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<td>Molybdenum</td>
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<td>µg/g</td>
<td>1</td>
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<td>µg/g</td>
<td>0.5</td>
<td>1.5</td>
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<tr>
<td>Silver</td>
<td>µg/g</td>
<td>0.2</td>
<td>0.5</td>
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<td>Thallium</td>
<td>µg/g</td>
<td>0.1</td>
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<tr>
<td>Zinc</td>
<td>µg/g</td>
<td>3</td>
<td>290</td>
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1. Revised report to change guidelines as per client request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards
Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit
Test methods may be modified from specified reference method unless indicated by an *
Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie

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Christine Burke
Lab Manager

Page 2 of 3.
CERTIFICATE OF ANALYSIS

Final Report

REPORT No. B18-10833 (I)

C.O.C.: G75184

Report To:
Peto MacCallum Ltd
19 Churchill Drive,
Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18
DATE REPORTED: 15-Jun-18
SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories
112 Commerce Park Drive
Barrie ON L4N 8W8
Tel: 705-252-5743
Fax: 705-252-5746

JOB/PROJECT NO.: P.O. NUMBER: 18CF004
WATERWORKS NO.

Summary of Exceedances

O. Reg. 153 - Soil, Ground Water and Sediment Standards
Tbl. 1 - Al - Table 1 - Res/Park/Institutional/Indus/Com/Commun

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Christine Burke
Lab Manager

Page 3 of 3.
% Moisture  3  Richmond Hill  FAL  26-Apr-18  A-% moisture RH  CWS Tier 1
PHC(F2-F4)  3  Kingston  KPR  26-Apr-18  C-PHC-S-001 (k)  CWS Tier 1
PHC(F1)  3  Richmond Hill  FAL  26-Apr-18  C-VPHS-01 (rh)  CWS Tier 1
µg/g = micrograms per gram (parts per million) and is equal to mg/Kg
F1 C6-C10 hydrocarbons in µg/g, (F1-btlex if requested)
F2 C10-C16 hydrocarbons in µg/g, (F2-naph if requested)
F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)
F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is
validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

nC6 and nC10 response factor is within 30% of response factor for toluene:
nC10,nC16 and nC34 response factors within 10% of each other:
C50 response factors within 70% of nC10+nC16+nC34 average:
Linearity is within 15%.

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention
time of nC50.

O. Reg. 153 - Soil, Ground Water and Sediment Standards
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Christine Burke
Lab Manager

Page 1 of 3.
<table>
<thead>
<tr>
<th>Parameter</th>
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<th>BH 2 SS 1</th>
<th>BH 4 SS 2</th>
<th>BH 7 SS 3</th>
<th>O. Reg. 153</th>
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<tr>
<td>PHC F1 (C6-C10)</td>
<td>µg/g</td>
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<td>&lt; 10</td>
<td>&lt; 10</td>
<td>&lt; 10</td>
<td>25</td>
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<tr>
<td>PHC F2 (&gt;C10-C16)</td>
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<td>7</td>
<td>6</td>
<td>&lt; 5</td>
<td>10</td>
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<tr>
<td>PHC F3 (&gt;C16-C34)</td>
<td>µg/g</td>
<td>10</td>
<td>15</td>
<td>18</td>
<td>&lt; 10</td>
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<td>PHC F4 (&gt;C34-C50)</td>
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<td>6.8</td>
<td>16.0</td>
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</table>

1. Revised report to change guidelines as per client request.

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Lab Manager
Summary of Exceedances

O. Reg. 153 - Soil, Ground Water and Sediment Standards
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Christine Burke
Lab Manager
### TESTING REQUIREMENTS
- [ ] O.Reg 153
- [ ] MISA Guidelines
- [ ] Surface Soil
- [ ] O.Reg 558 Leachate Analysis
- [ ] Sub Surface Soil
- [ ] Disposal Site: ____________________________________________
- [ ] Record of Site Condition: (O.Reg 153)
- [ ] Landfill Monitoring
- [ ] Provincial Water Quality Objectives
- [ ] Other: ____________________________________________________

### REPORT NUMBER (Lab Use)
- B18-10833

### Are any samples to be submitted intended for Human Consumption under any Drinking Water Regulations?
- [ ] Yes
- [ ] No

### Indicate Laboratory Samples are submitted to:
- [ ] Kingston
- [ ] Ottawa
- [ ] Richmond Hill
- [ ] Windsor
- [ ] Barrie
- [ ] London

### ANALYSES REQUESTED (Print Test in Boxes)
- [ ] PNC (FI-FY)
- [ ] CH (SI-FY)

### TURNAROUND SERVICE REQUESTED (see back page)
- [ ] Platinum: 200% Surcharge
- [ ] Gold: 100% Surcharge
- [ ] Silver: 50% Surcharge
- [ ] Bronze: 25% Surcharge
- [ ] Standard: 5-7 days

### Sample Matrix Legend:
- WW=Waste Water
- SW=Surface Water
- GW=Groundwater
- LS=Liquid Sludge
- SS=Solid Sludge
- S=Soil
- Sed=Sediment
- PC=Paint Chips
- F=Filter
- O=Oil

---

### Lab No. | Sample Identification | S.P.L. | Sample Matrix | Date Collected | Time Collected | Indicate Test For Each Sample | Field | # Bottles | Field Filtered/Y/N
---|------------------------|-------|---------------|----------------|----------------|-----------------------------|-------|-----------|------------------
BH 2 | 551 | 5 | 18-04-23 | |
BH 4 | 552 | 5 | 18-04-20 | |
BH 7 | 553 | 5 | 18-04-28 | |

---

### SAMPLE SUBMISSION INFORMATION
- Sampled by: ____________________________
- Submitted by: ____________________________
- Print: ____________________________
- Sign: ____________________________

### SHIPPING INFORMATION
- Client's Courier: ____________________________
- Caduceon's Courier: ____________________________
- Drop Off: ____________________________
- Caduceon (Pick-up): ____________________________
- # of Pieces: ____________________________

### REPORTING / INVOICING
- Invoice: ____________________________
- Report by Fax: ____________________________
- Report by Email: ____________________________
- Invoice by Email: ____________________________
- Invoice by Mail: ____________________________

### SAMPLE RECEIVING INFORMATION [LABORATORY USE ONLY]
- Received By (print): ____________________________
- Date Received (yy-mm-dd): ____________________________
- Time Received: ____________________________
- Signature: ____________________________
- Laboratory Prepared Bottles: ____________________________
- Yes: ____________________________
- No: ____________________________
- Sample Temperature °C: ____________________________
- Labeled by: ____________________________

### Comments:
- Date (yy-mm-dd)/Time: ____________________________
- Date (yy-mm-dd)/Time: ____________________________

---

### Notes:
- "pee cup 00"  
  "ger -OK"  
  "ger viable pH"
CERTIFICATE OF ANALYSIS

C.O.C.: G75186

REPORT No. B18-12842 (I)

Rev. 1

Report To:       Caduceon Environmental Laboratories

Peto MacCallum Ltd
19 Churchill Drive,
Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 14-May-18
DATE REPORTED: 15-Jun-18
SAMPLE MATRIX: Soil

Job/Project No.: P.O. Number: 18CF004

WATERWORKS NO.

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<th>Parameter</th>
<th>Qty</th>
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<th>Analyst Initials</th>
<th>Date Analyzed</th>
<th>Lab Method</th>
<th>Reference Method</th>
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<td>EPA 6020</td>
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µg/g = micrograms per gram (parts per million) and is equal to mg/Kg
F1 C6-C10 hydrocarbons in µg/g, (F1-bt bx if requested)
F2 C10-C16 hydrocarbons in µg/g, (F2-naph if requested)
F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)
F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.
nC6 and nC10 response factor is within 30% of response factor for toluene:
nC10,nC16 and nC34 response factors within 10% of each other:
C50 response factors within 70% of nC10+nC16+nC34 average:
Linearity is within 15%:
All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention time of nC50.

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Christine Burke
Lab Manager

Page 1 of 3.
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<td>pH @25°C</td>
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<td>Cyanide (Free)</td>
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<td>Beryllium</td>
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<td>Thallium</td>
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<tr>
<td>Zinc</td>
<td>µg/g</td>
<td>3</td>
<td>290</td>
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</table>

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REPORT No. B18-12842 (ii)

C.O.C.: G75186

Final Report

Rev. 1

Report To:
Peto MacCallum Ltd
19 Churchill Drive,
Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 14-May-18
DATE REPORTED: 15-Jun-18
SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories
112 Commerce Park Drive
Barrie ON L4N 8W8
Tel: 705-252-5743
Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER: 18CF004
WATERWORKS NO.:

<table>
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<tr>
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<th>Qty</th>
<th>Site Analyzed</th>
<th>Analyst Initials</th>
<th>Date Analyzed</th>
<th>Lab Method</th>
<th>Reference Method</th>
</tr>
</thead>
<tbody>
<tr>
<td>% Moisture</td>
<td>1</td>
<td>Richmond Hill</td>
<td>JE</td>
<td>15-May-18</td>
<td>A-% moisture RH</td>
<td>CWS Tier 1</td>
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<tr>
<td>PHC(F2-F4)</td>
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<td>KPR</td>
<td>15-May-18</td>
<td>C-PHC-S-001 (k)</td>
<td>CWS Tier 1</td>
</tr>
<tr>
<td>PHC(F1)</td>
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<td>Richmond Hill</td>
<td>JE</td>
<td>15-May-18</td>
<td>C-VPHS-01 (rh)</td>
<td>CWS Tier 1</td>
</tr>
</tbody>
</table>

\( \mu g/g = \text{micrograms per gram (parts per million)} \) and is equal to mg/Kg
F1 C6-C10 hydrocarbons in \( \mu g/g \), (F1-btex if requested)
F2 C10-C16 hydrocarbons in \( \mu g/g \), (F2-naph if requested)
F3 C16-C34 hydrocarbons in \( \mu g/g \), (F3-pah if requested)
F4 C34-C50 hydrocarbons in \( \mu g/g \)
This method complies with the Reference Method for the CWS PHC and is validated for use in the laboratory.

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C50 response factors within 70% of nc10+nc16+nc34 average:
Linearity is within 15%:
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Christine Burke
Lab Manager

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<table>
<thead>
<tr>
<th>Parameter</th>
<th>Units</th>
<th>R.L.</th>
<th>O. Reg. 153 Tbl. 1 - All</th>
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</thead>
<tbody>
<tr>
<td>PHC F1 (C6-C10)</td>
<td>µg/g</td>
<td>10</td>
<td>25</td>
</tr>
<tr>
<td>PHC F2 (&gt;C10-C16)</td>
<td>µg/g</td>
<td>&lt; 5</td>
<td>10</td>
</tr>
<tr>
<td>PHC F3 (&gt;C16-C34)</td>
<td>µg/g</td>
<td>14</td>
<td>240</td>
</tr>
<tr>
<td>PHC F4 (&gt;C34-C50)</td>
<td>µg/g</td>
<td>&lt; 10</td>
<td>120</td>
</tr>
<tr>
<td>% moisture</td>
<td>%</td>
<td>8.4</td>
<td></td>
</tr>
</tbody>
</table>

1. Revised report to change guidelines as per client request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards
Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit
Test methods may be modified from specified reference method unless indicated by an *
Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie

The analytical results reported herein refer to the samples as received. Reproduction of this analytical report in full or in part is prohibited without prior consent from Caduceon Environmental Laboratories.

Christine Burke
Lab Manager
# Summary of Exceedances

O. Reg. 153 - Soil, Ground Water and Sediment Standards  
Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

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R.L. = Reporting Limit  
Test methods may be modified from specified reference method unless indicated by an *  
Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie  
The analytical results reported herein refer to the samples as received. Reproduction of this analytical report in full or in part is prohibited without prior consent from Caduceon Environmental Laboratories.

Christine Burke  
Lab Manager
### Testing Requirements

- O.Reg 153: Table
- Surface Soil: Yes
- Sub Surface Soil: No
- Record of Site Condition: O.Reg 153
- O.Reg 558 Leachate Analysis: Disposal Site: No
- Provincial Water Quality Objectives: Yes
- Sewer Use By-Law: No
- MISA Guidelines: No
- Landfill Monitoring: No

### Report Number (Lab Use)

- B8-12842

### Are any samples to be submitted intended for Human Consumption under any Drinking Water Regulations?

- Yes [ ]
- No [ ]

- If yes, submit all Drinking Water Samples on a Drinking Water Chain of Custody

### Indicate Laboratory Samples are submitted to:

- Kingston [X]
- Ottawa [X]
- Richmond Hill [X]
- Windsor [X]
- Barrie [X]
- London [X]

### Organization:

- Wetmore Consultants

### Address and Invoicing Address (if different):

- 101 New Street

### Contact:

- Geoff White

### Tel:

- 705-734-3900

### Fax:

- 705-734-9111

### Quote No.:

- 18C004

### Project Name:

- 18C004

### Additional Info:

- Email: geoff@wetmoreconsultants.com

### Lab No. Sample Identification

<table>
<thead>
<tr>
<th>Lab No.</th>
<th>Sample Identification</th>
<th>S.P.L.</th>
<th>Date Collected</th>
<th>Time Collected</th>
</tr>
</thead>
<tbody>
<tr>
<td>TPS 6S 2</td>
<td></td>
<td>S</td>
<td>5</td>
<td>18-05-11</td>
</tr>
</tbody>
</table>

### Indicate Test For Each Sample

- By Using A Check Mark In The Box Provided

### Field

- pH
- Temp.
- Sample
- Filtered (y/n)

### Field

- 4

### Turnaround Service Requested (see back page)

- Platinum 20% Surcharge
- Gold 100% Surcharge
- Silver 50% Surcharge
- Bronze 25% Surcharge
- Standard 5-7 days

### Specific Date:

- [ ]

### Sample Submission Information

- Sampled by: Alan Turner
- Submitted by: Caduceon's Courier
- Print: 2018-05-11
- Sign: 2018-05-11

### Comments:

- Specimen for RH & vigoro.
  - [x]
  - [y]
  - [z]

### Shipping Information

- Client's Courier [ ]
- Caduceon's Courier [ ]
- Drop Off [ ]
- Caduceon (Pick-up) [ ]

### Reporting / Invoicing

- Invoice [ ]
- Report by Fax [ ]
- Report by Email [ ]
- Invoice by Email [ ]
- Invoice by Mail [ ]
- Laboratory Prepared Bottles: Yes [X]

### Sample Receiving Information (Laboratory Use Only)

- Received By (print): 2018-05-14
- Signature: [Signature]
- Date Received (yy-mm-dd): 2018-05-14
- Time Received: 12:30
- Labeled by: [Signature]

### Sample Temperature °C:

- 12.6
APPENDIX B

Statement of Limitations
This report is prepared for and made available for the sole use of the client named. Peto MacCallum Ltd. (PML) hereby disclaims any liability or responsibility to any person or entity, other than those for whom this report is specifically issued, for any loss, damage, expenses, or penalties that may arise or result from the use of any information or recommendations contained in this report. The contents of this report may not be used or relied upon by any other person without the express written consent and authorization of PML.

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The report is based solely on the scope of services which are specifically referred to in this report. No physical or intrusive testing has been performed, except as specifically referenced in this report. This report is not a certification of compliance with past or present regulations, codes, guidelines and policies.

The scope of services carried out by PML is based on details of the proposed development and land use to address certain issues, purposes and objectives with respect to the specific site as identified by the client. Services not expressly set forth in writing are expressly excluded from the services provided by PML. In other words, PML has not performed any observations, investigations, study analysis, engineering evaluation or testing that is not specifically listed in the scope of services in this report. PML assumes no responsibility or duty to the client for any such services and shall not be liable for failing to discover any condition, whose discovery would require the performance of services not specifically referred to in this report.
STATEMENT OF LIMITATIONS

The findings and comments made by PML in this report are based on the conditions observed at
the time of PML’s site reconnaissance. No assurances can be made and no assurances are
given with respect to any potential changes in site conditions following the time of completion of
PML’s field work. Furthermore, regulations, codes and guidelines may change at any time
subsequent to the date of this report and these changes may effect the validity of the findings and
recommendations given in this report.

The results and conclusions with respect to site conditions are therefore in no way intended to be
taken as a guarantee or representation, expressed or implied, that the site is free from any
contaminants from past or current land use activities or that the conditions in all areas of the site
and beneath or within structures are the same as those areas specifically sampled.

Any investigation, examination, measurements or sampling explorations at a particular location
may not be representative of conditions between sampled locations. Soil, ground water, surface
water, or building material conditions between and beyond the sampled locations may differ from
those encountered at the sampling locations and conditions may become apparent during
construction which could not be detected or anticipated at the time of the intrusive sampling
investigation.

Budget estimates contained in this report are to be viewed as an engineering estimate of probable
costs and provided solely for the purposes of assisting the client in its budgeting process. It is
understood and agreed that PML will not in any way be held liable as a result of any budget
figures provided by it.

The Client expressly waives its right to withhold PML’s fees, either in whole or in part, or to make
any claim or commence an action or bring any other proceedings, whether in contract, tort, or
otherwise against PML in anyway connected with advice or information given by PML relating to
the cost estimate or Environmental Remediation/Cleanup and Restoration or Soil and Ground
Water Management Plan Cost Estimate.