

**FUNCTIONAL SERVICING &
STORMWATER MANAGEMENT REPORT**

**ALTA SUBDIVISION PHASE II
TOWN OF THE BLUE MOUNTAINS**

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1.0 INTRODUCTION

C.F. Crozier & Associates Inc. (Crozier) was retained by Tabera Ltd. (Tabera) to complete a Functional Servicing and Stormwater Management Report in support of the relevant planning applications for the proposed Alta Phase II Subdivision located in the Town of The Blue Mountains (Town). The proposed development will herein be referred to as the Subject Lands. The Subject Lands are intended to be rezoned to Low-Density Recreational Residential.

The Subject Lands cover approximately 30 hectares of land and are legally described as Part of Lots 23 and 24, Concession 4, Town of The Blue Mountains, County of Grey. The Subject Lands are bounded by Hidden Lake Road to the north and Craigleith Provincial Park to the east. Alta Phase I development lands are located to the south and privately owned lands are situated to the west of the Subject Lands. Refer to **Figure 1** for a Site Location Plan.

The Draft Plan (February 2022) proposes 60 single-family residential units for the Subject Lands. The proposed development will also include a 20 m Right-of-Way (ROW), a stormwater management block and open space blocks for drainage and trail network purposes. In addition, the open space blocks contain both the Nipissing Ridge, which is situated along the north-easterly limits of the development lands and the Niagara Escarpment, which is located to the west of the development lands. The Draft Plan has been included in this report as **Figure 2**.

A Functional Servicing and Preliminary Stormwater Management Report (Crozier, January 2008) was originally submitted to the Town in 2008 for the Subject Lands. Through consultation discussions with the Town of The Blue Mountains in 2008, it was agreed that the analysis should include an evaluation of the drainage corridor downstream of the Subject Lands to the outlet at Georgian Bay. This Functional Servicing and Stormwater Management Report serves as an update to the report prepared in 2008 and outlines the proposed servicing, grading and stormwater management strategy for the Subject Lands as well as the evaluation of the drainage corridor downstream of the Subject Lands.

2.0 BACKGROUND

The proposed development lies within Subwatersheds 21 and 22 as defined in the *Craigleith Camperdown Subwatershed Study* (GSCA, 1993). The Craigleith Camperdown Subwatershed Study (CCSS) was prepared to identify opportunities and constraints for developments within the subwatersheds identified in the report. Specific areas of concern that were evaluated include flooding, stream channel erosion, groundwater recharge, water quality treatment and environmental resources. The CCSS establishes the framework of the proposed stormwater management strategy outlined in this report.

The Subject Lands are situated along the servicing boundary for the Camperdown Service Area and the Craigleith Service Area. The Alta Phase II lands were originally situated within the Camperdown Service Area per the *Comprehensive Environmental Study Report for the Lora Bay, Clarksburg, Thornbury and Camperdown Service Areas, Phase 2 Report* (MacViro, 2002). The MacViro report stated that the Alta Phase II lands could be temporarily serviced within the Craigleith Service Area via a temporary sewage pump station (SPS) pumping to the existing SPS constructed in Alta Phase I on Oak Court.

Prior to the execution of the Camperdown External Services contract, further investigation of the Wards Road and Hidden Lake Road area was completed to determine the practicality of servicing these lands as part of the Camperdown Service Area. This re-investigation was warranted because of the excessive depth of the sanitary sewers and SPS located at Delphi Point to provide for a gravity

sanitary conveyance system from the Wards Road and Hidden Lake Road service area to the Delphi SPS. The major concern was the associated construction costs with the sanitary sewers depth and the relationship to the bedrock and groundwater elevations.

As a result of the re-evaluation of servicing for the Wards Road and Hidden Lake Road areas, an *Addendum to the Comprehensive ESR* (MacViro, 2005) was issued. The Addendum report recommended Hidden Lake/Wards Road and Alta Phase II be transferred to the Craigleith Service Area.

The Town of The Blue Mountains also proceeded with the *Combined EA Master Plan for Craigleith, Castle Glen and Osler* (MacViro, 2006), which established the servicing requirements for the development lands associated with Craigleith, Castle Glen and Osler. The preferred servicing strategy for Alta Phase II was established in the Master Plan EA.

3.0 SITE DESCRIPTION

The Subject Lands are physiographically distinguished by five areas: the Escarpment face located at the southwest portion of the development lands, an intermediate plateau on which proposed Street 'C' and Lots 44 – 55 are located, an intermediate ridge located immediately east of Street 'C', and the "flatlands" on which the balance of the development will occur. The Nipissing Ridge is also located north and east of the "flatlands" which abuts Hidden Lake Road and Craigleith Provincial Park. The Subject Lands generally fall from south to north, with gradients ranging from 2% within the flatlands to approximately 30% across the Escarpment face and Nipissing Ridge lands. Refer to **Figure 2** for the proposed development layout, site topography and existing configuration of adjacent lands.

Existing access to the Subject Lands is provided by a single farm lane off Hidden Lake Road which traverses the face of the Nipissing Ridge. The laneway provides access to two existing agricultural structures currently located on-site. These structures were used in the past during agricultural operations across the flatlands. These lands are currently idle and not actively used for agricultural operations.

The soils on site are classified as Dunedin Clay and Kemble Silty Clay (Soil Survey Complex, 2019). These soils are classified as Hydrologic Soil Groups D and C, respectively.

4.0 ROAD STANDARD

Access to the site will be provided via Alta Road and Hidden Lake Road. Alta Road is proposed to be extended northwest from its westerly terminus in Phase I to Hidden Lake Road.

Within the development, there is one north-south road (Alta Road) and two looped roads (Street B and C). Alta Road will be constructed according to Town standards with a 20.0 m urban Right-of-Way (ROW) and 8.5 m pavement width complete with mountable curb and gutter. Due to the large lots and character of the development, Street B and C will be constructed according to Town standards with a 20.0 m rural ROW and 6.0 m pavement width. The pavement structure for the roadways will be constructed as per municipal standards and recommendations of the geotechnical engineer. Street C will also have five cross culverts to convey external drainage.

A 2.0 m wide sidewalk was constructed within the boulevard of Alta Road within Phase 1 from Hemlock Court to the temporary turning circle. It is proposed to continue the 2.0 m wide sidewalk along Alta Road to Hidden Lake Road per the typical road standard used in Phase I.

The reader is directed to the Traffic Impact Study (C. F. Crozier & Associates Inc., February 2022) submitted under separate cover, which identifies future operating conditions of the boundary road network surrounding the development.

5.0 SANITARY SERVICING

5.1 Existing Sanitary System Infrastructure

Sanitary Servicing Background

The *Combined EA Master Plan for Craigleith, Castle Glen and Osler* (MacViro, 2006) and *Addendum to the Phase 2 Comprehensive ESR* (MacViro, 2005) provides the framework for the sanitary servicing in Alta Phase II.

The above-mentioned reports recommended the Hidden Lake area, consisting of Alta Phase II, Ward's Road, and Hidden Lake Road, should be serviced as part of the Craigleith Service Area. The Craigleith Wastewater Treatment Plant (WWTP) is currently operating at 42% of the built capacity (2020 Town of The Blue Mountains Year End Water & Wastewater Capacity Assessment). It is understood there is an uncommitted reserve capacity within the WWTP to accommodate the 60 residential lots of Alta Phase II.

The Hidden Lake area, including Alta Phase II, has been studied through the initiation of an Environmental Assessment (EA) by the Town. Preliminary EA findings have suggested the proposed area is to be serviced via a proposed SPS situated at the intersection of Hidden Lake Road and Highway 26, ultimately pumping flows east to the Craigleith Sewage pumping station. However, the timeline to complete the EA and construct the infrastructure identified as the preferred alternative is unknown and is very likely still many years away. The proposed sanitary servicing strategy for the Subject Lands will allow development to proceed in advance of the Town completing the Hidden Lake Road improvements, without impeding the Town's ability to complete the EA. The proposed strategy is outlined in more detail in Section 5.2.

Existing Sanitary System Infrastructure

There is an existing 200 mm diameter sanitary stub in Alta Phase I at the northwesterly terminus of Alta Road. This 200 mm diameter sanitary sewer drains to the Alta Phase I SPS on Oak Court, which then pumps sewage to the Margaret Drive SPS.

Presently, the Margaret Drive SPS receives sewage from Alta Phase I, Alpine Flatlands Phase I and II, Arrowhead Crescent and Alpine Ski Club. The sewage is pumped to a 200 mm diameter gravity sewer located further south and east on Sleepy Hollow Road. Previously, the Town had considered decommissioning the Margaret Drive SPS in the future upon completion of a trunk gravity sewer through the Georgian Woodlands Phase IV lands. Said sewer would connect to the existing 450 mm diameter sanitary sewer located on Old Lakeshore Road, which conveys sewage to the Craigleith Pump Station.

However, recent discussions with the Town indicate that the Margaret Drive SPS may not be decommissioned and would continue to convey sewage from developments in the area, including future phases of the Georgian Woodlands development. The capacity of the downstream sanitary sewer infrastructure will be assessed during detailed design to identify any required external improvements.

5.2 Proposed Sanitary Servicing Strategy

There were two (2) internal sanitary servicing strategies considered for Alta Phase II. They are described below.

Option 1: New Pumping Station on Alta Phase II

Option 1 consists of providing a network of gravity sewers within the development that drain towards a new SPS located within Block 61 south of the existing ridge and bordering on Lot 9. The new SPS would pump flows to the existing sanitary system in Alta Phase I and ultimately to the Margaret Drive SPS. If a future SPS at Hidden Lake Road and Highway 26 is constructed and gravity services are extended along Hidden Lake road in the future, the Alta Phase II sanitary sewers could be connected to the permanent SPS through Hidden Lake Road. The proposed SPS in Alta Phase II could then be decommissioned by the Town if so desired.

Option 2: Combination of Gravity and Low-Pressure Forcemain Sewers

Option 2 consists of providing a combination of gravity and low-pressure forcemain sewers within the development that drain towards the existing sanitary system in Alta Phase I. Lots 44 – 55 would be serviced by gravity and the remaining lots would be serviced by low-pressure forcemain due to the natural grading of the Subject Lands. The sanitary flows would then be conveyed to the Alta Phase I SPS and ultimately the Margaret Drive SPS.

Proposed Sanitary Servicing Solution

Option 1 was chosen as the preferred sanitary servicing solution for the Subject Lands. It allows for the original sanitary servicing strategy for the Subject Lands to be implemented.

Internal sanitary servicing for the Subject Lands will be provided via a network of gravity sewers that follow the alignment of the internal roadways and drain to the proposed SPS within the SWM Facility block. Sanitary sewers will be designed and constructed in accordance with Town design standards, at a size and depth sufficient to service each lot and building. Refer to **Figure 3** for the internal sanitary sewage conveyance system. Refer to **Figure 4** for the external sanitary sewage conveyance system.

Preliminary sanitary flows for the site were estimated using Town standards. Applicable design criteria have been summarized in **Table 1**.

Table 1: Sanitary Design Criteria

Criteria	Standard
Average Flow Rate (L/cap/day)	450
Infiltration (L/s/ha)	0.23
Peaking Factor (Harmon Formula)	4.19
Population Density (PPU)	2.3

Based on the above criteria and the proposed unit total, it is estimated that peak sanitary flow from the Subject Lands is 6.84 L/s. Sanitary flow calculations have been provided in **Appendix A**.

Both the Alta Phase I SPS on Oak Court (originally designed to service Phase II Lands) and the Margaret Drive SPS (currently operating less than 20% capacity, based on discussions with the Town) have the capacity to service the proposed lands. The capacity of the downstream gravity sewer infrastructure from the outlet of the Margaret Drive SPS would be confirmed at the detailed design stage and external sewer improvements (if any) identified in consultation with the Town.

6.0 WATER SERVICING

6.1 Existing Water System Infrastructure

Water supply for the Subject Lands will be supplied by the Thornbury Water Treatment Plant (WTP), which also services areas within Thornbury, Clarksburg, Camperdown, Lora Bay, Swiss Meadows and Craighleith. The WTP is owned by the Town of The Blue Mountains.

The Thornbury WTP has a capacity of 15,140 m³/day, with an additional 1,250 m³/day water supply available from the Town of Collingwood. There is currently a demand of 11,057 m³/day connected or allocated to the water system, with an additional 2,988 m³/day reserved. This leaves 2,345 m³/day of water supply available (2020 Town of The Blue Mountains Year End Water & Wastewater Capacity Assessment).

An existing 200 mm diameter watermain stub currently exists at the northwesterly terminus of Alta Road. A 150 mm diameter watermain is located along Hidden Lake Road and services the existing lots fronting Hidden Lake Road.

6.2 Proposed Water Servicing Strategy

The proposed servicing solution for the Subject Lands will be to connect to the existing 200 mm diameter watermain on Alta Road and 150 mm diameter watermain on Hidden Lake Road.

The internal watermain distribution system will follow the alignment of the internal roadways complete with individual service connections for each lot and building. Fire hydrants will be spaced as required to provide the necessary fire protection and to meet municipal standards. The preliminary water distribution layout has been presented in **Figure 5**.

Preliminary water demands for the Subject Lands have been estimated in conjunction with Town standards that concur with Table 3-1 of the Ministry of Environment, Conservation and Parks (MECP) Design Guidelines for Drinking Water Systems. Applicable design criteria have been summarized in **Table 2** below.

Table 2: Watermain Design Criteria

Criteria	Standard
Average Flow Rate (L/cap/day)	450
Maximum Day/Peak Hour	2.0/4.5
Single Family Density (PPU)	2.3

The following water demands have been calculated for the Subject Lands per Town standards identified above:

- Average Daily Flow Rate – 0.72 L/s
- Max Daily Flow Rate – 1.44 L/s
- Peak Hour Flow Rate – 3.23 L/s

Refer to **Appendix B** for the water demand calculations.

Streets B and C will have a minimum 150 mm diameter watermain installed and looped back to the 200 mm diameter main on Alta Road. This sizing will be subject to completing a distribution analysis during the detailed design process to verify that maximum day demands, and fire flow requirements are met.

Fire Flow Estimates

Per municipal requirements, the Water Supply for Fire Protection, A Guide to Recommend Practice (Fire Underwriters Survey (FUS), 1999) was used to estimate fire flows for the Subject Lands. Fire flow demand was calculated based on a collection of single detached residential dwellings two (2) stories in height or less with minimum setbacks of 3m. As per the FUS Calculation Note J, the proposed fire flow was calculated using the short method. The required fire flow for the development is approximately 67 L/s. Fire flow calculations have been provided in **Appendix B**. Fire hydrant testing may be completed during detailed design to confirm that sufficient fire flows are available.

7.0 STORMWATER MANAGEMENT

SWM and drainage conditions for the proposed development must comply with the policies and standards of:

- The Town of The Blue Mountains (Town);
- The Grey Sauble Conservation Authority (GSCA); and,
- The Ministry of the Environment, Conservation and Parks (MECP).

The stormwater management criteria that will be met with the development of Alta Phase II are as follows:

- Water Quantity Control
 - o "Post to pre" control for storms up to and including the 100-year storm event.
- Water Quality Control
 - o "Enhanced Protection" given Georgian Bay as the ultimate receiver.
- Erosion Control
 - o 24-hour detention of the 25mm event runoff.
- Development Standard
 - o Urban cross section complete with 5-year storm sewer;
 - o Rural cross section complete with complete with ditches with 3:1 side slopes;
 - o Lot grading at 2% optimum; and
 - o Minor and major drainage systems to convey frequent and infrequent rainfall/runoff events respectively.

7.1 Existing Drainage Conditions

As indicated in Section 2.0, the Subject Lands are located within Subwatersheds 21 and 22 as identified in the CCSS and illustrated in **Figure 6**. Field reconnaissance conducted by Crozier staff in 2007 suggests that the western portions of Subwatershed 21 and eastern portions of Subwatershed 22 drain to Georgian Bay via separate outlets. Consequently, a new subwatershed, referred to as Subwatershed 21A, that bisects Subwatersheds 21 and 22 has been delineated. **Figure 6** illustrates both the original GSCA (1993) and above-noted revised subwatershed boundaries.

Generally, drainage from the Subject Lands (and the upgradient Niagara Escarpment) shed in a northerly direction toward Hidden Lake Road, concentrating at three (3) locations. These are identified and described in this report as Outlet A, B and C. The drainage areas which contribute to these outlets are delineated in **Figure 7** and discretized to facilitate hydrologic modelling. The following sections describe the existing drainage conditions associated with each outlet.

Outlet A

The contributing area to Outlet A is approximately 13.2 ha and extends from the tablelands of the Escarpment to Hidden Lake Road. The contributing area has been discretized into five subcatchments, EXT-1 – EXT-3, INT-1, and INT-4, as illustrated in **Figure 7**. Outlet A directs drainage to an existing 825 mm dia. culvert beneath Hidden Lake Road. Outlet A is located within Subwatershed 22.

Subcatchments EXT-1, EXT-2, and EXT-3 contribute drainage from the Escarpment face and reach the proposed development lands as sheet flow within incised channels. A series of manmade ditches located on the flatlands of the site direct the drainage towards Hidden Lake Road. Subcatchment INT-4 also contributes drainage from the toe of the escarpment slope via sheet flow and incised channels to the above-noted interceptor ditches. These interceptor ditches were constructed during historic agricultural operations and extend across subcatchment INT-1 to the existing 825 mm dia. culvert beneath Hidden Lake Road. It should be noted that a portion of subcatchment INT-1 consists of sheet flow drainage from the flatlands located on the south side of Hidden Lake Road. The existing 825 mm dia. culvert conveys runoff across Hidden Lake Road towards a low-lying and poorly drained area before reaching Highway 26 and Georgian Bay. A detailed description of the drainage corridor north of Hidden Lake Road is described in Section 8.0 (External Drainage Corridor Analysis).

Outlet B

The contributing area to Outlet B is approximately 11.2 ha. Similar to Outlet A, the drainage area extends from the tablelands of the Escarpment to Hidden Lake Road and consists of four subcatchments: EXT-4, INT-2, INT-5 and UNC-3. Outlet B directs drainage to an existing 900 mm dia. culvert beneath Hidden Lake Road. Outlet B is located within Subwatershed 22.

Subcatchments EXT-4 and INT-5 contribute sheet flow from various portions of the Escarpment face to a manmade agricultural ditch extending from the upstream limit of subcatchment INT-2 across the flatlands to an existing 900 mm dia. culvert beneath Hidden Lake Road. Subcatchment UNC-3 contributes both sheet flow and concentrated flow from the face of the Nipissing Ridge.

The existing farm laneway that extends from Hidden Lake Road to the top of the Nipissing Ridge acts as a drainage divide between the areas contributing to Outlet B and C. Interceptor ditches along each side of the laneway direct the intercepted sheet flow to the Hidden Lake Road drainage corridor. The west interceptor ditch ultimately directs drainage to Outlet B. The east ditch directs drainage to Outlet C.

Outlet C

The contributing area to Outlet C is approximately 14.0 ha. The drainage area extends to the tablelands of the Escarpment and consists of four subcatchments: EXT-5, INT-3, INT-6 and UNC-4. Outlet C directs drainage to Watercourse 21A and is located in Subwatershed 21A.

Subcatchments EXT-5 and INT-6 contribute drainage from the Escarpment face, which reaches subcatchments INT-3 and UNC-4 as sheet flow within incised channels. Drainage from these subcatchments ultimately reaches Watercourse 21A at the 90-degree bend of Hidden Lake Road.

Watercourse 21A was identified by Crozier as a drainage feature independent of Watercourse 21 as originally identified in the CCSS. Originally, the CCSS suggested that Watercourse 21A combines with Watercourse 21. Based on a review of watershed topography and field reconnaissance, it was confirmed that Watercourse 21A drains directly to Georgian Bay along the east roadside ditch of Hidden Lake Road and through the Craigeleith Provincial Park north of Highway 26.

Also evident from the field reconnaissance and watershed topography is the proximity of Watercourse 21A to a tributary of Watercourse 21 in the vicinity of the 90-degree bend at Hidden Lake Road. Given the topography in this area and geometry of Watercourse 21A, spill flow conditions may occur towards Watercourse 21 during large storm events.

7.2 Proposed Drainage Conditions

The proposed development will be constructed to a fully urbanized system complete with curb and gutter and storm sewers on Alta Road. Street B and C will have rural cross-sections complete with ditches with 3:1 side slopes. A dual drainage approach will consist of minor and major stormwater flow routes to ensure adequate conveyance for runoff. The minor drainage system will consist of storm sewers, catchbasins and ditches sized to convey the 5-year design storm event, per municipal standards. The major drainage system will provide overland flow routes within the road allowance.

In order to meet the SWM criteria, the minor and major storm flows will be conveyed to a SWM facility located in the northeast corner of the site within block 62 on "Street B", to be treated and controlled prior to being released. The SWM facility will provide the necessary water quality, quantity and erosion controls. The proposed pond design and location is presented in **Figure 10**. The SWM facility outlet structure will consist of three outlets to discharge the treated runoff. The proposed outlets will be constructed under "Street B" to an engineered conveyance channel proposed along the existing farm laneway toward Hidden Lake Road. The proposed SWM pond outlet will include an orifice for extended detention, a rectangular weir to convey active storage flows, and a culvert receiving flows conveyed over the proposed SWM pond spillway. The culvert downstream of the proposed spillway will be sized to convey regional flows at the detailed design stage. The outlets will discharge to the engineered conveyance channel and will convey treated stormwater north to the existing 900 mm dia. CSP culvert at Hidden Lake Road (Outlet B).

Preliminary site grading has been completed to ensure that the proposed minor and major storm drainage systems to the SWM facility are feasible. The post-development drainage plan and preliminary site grading plan are provided as **Figures 8** and **9**, respectively.

A series of interceptor ditches are proposed to manage both external and internal runoff and direct it to the appropriate outlets. The proposed locations, alignments and cross-sectional configurations of these ditches have been incorporated into the development and are illustrated in **Figure 9**.

As illustrated in **Figure 8**, the drainage areas contributing to each outlet will have minor modifications in post-development conditions. The following sections describe the proposed drainage conditions associated with each outlet.

Outlet A

The drainage area contributing to Outlet A is reduced from 13.2 ha to 4.5 ha as a result of a series of interceptor ditches and conveyance of runoff across the Subject Lands. This will improve downstream drainage capacity issues. In post-development conditions, Outlet A is located within Subwatershed 22 and consists of three (3) subcatchments: EXT-1, INT-3, and UNC-1.

Outlet B

The drainage area contributing to Outlet B will increase from 11.2 ha to 22.80 ha. This is primarily a result of regrading the site and controlling the runoff within the SWM facility. The SWM facility will drain to the existing 900 mm dia. cross-culvert, respecting its capacity. The stormwater quantity and quality control requirements and preliminary configuration of the proposed SWM facility are described in

Sections 7.3 and 7.4, respectively. In post-development conditions, Outlet B is located within Subwatershed 22 and consists of eight (8) subcatchments: EXT-2, EXT-3, INT-1, INT-2, INT-4, UNC-2, UNC-3 and the SWM Facility.

Outlet C

The drainage area contributing to Outlet C will decrease from 14.0 ha to 11.0 ha. In post-development conditions, Outlet C is located in Subwatershed 21A and consists of four (4) subcatchments: EXT-4, EXT-5, INT-5 and UNC-4. Drainage from subcatchments EXT-4 and EXT-5 will be conveyed via interceptor ditches along the southwest limit of the Subject Lands and directed to Watercourse 21A. Similarly, subcatchment INT-5 will convey a nominal drainage area, consisting only of Escarpment slope, directly to Watercourse 21A. The balance of the area contributing to Outlet C in post-development conditions consists of the Nipissing Ridge, located at the northeast corner of the Subject Lands.

7.3 Hydrologic Analysis

Hydrologic modelling was prepared for the pre-development and post-development scenarios using the stormwater management hydrologic computer program SWMHYMO (Sabourin, 1998). The purpose of the modelling was to determine the detention storage volumes required for the Subject Lands to ensure post-development peak flow rates do not exceed the pre-development target flows (i.e. quantity control). Three points of interest (Outlets A, B and C) were examined.

To accurately assess the peak flows from the individual catchments, the NASHYD command in SWMHYMO was used to model rural conditions, whereas the STANHYD command was used to model urban development conditions. 2, 5, 10, 25, 50 and 100-year rainfall events were simulated using a six-hour Keifer Chu, 12-hour SCS Type II and 24-hour SCS Type II consistent with municipal design standards and GSCA requirements.

The hydrologic parameters and the SWMHYMO model input and output files are found in **Appendix C** and **D**, respectively. The SWMHYMO model schematics for pre- and post-development conditions can be found in **Appendix D**.

To evaluate water quantity and quality control requirements, the hydrologic model was established to produce peak flows at the three outlet locations based on the pre- and post-development drainage plans provided as **Figures 7** and **8**, respectively. The hydrologic model was then extended to facilitate the external drainage corridor analysis, which is described in Section 8.0.

7.3.1 Pre-Development Model Setup

To establish pre-development flows, the contributing drainage areas to each outlet were first subdivided into internal and external drainage areas. Catchments INT-1 – INT-6 and UNC-3 and UNC-4 consist of the Subject Lands and catchment EXT-1 – EXT-5 consist of the external drainage areas. Refer to **Figure 7** for the Pre-Development Drainage Plan and **Appendix C** for hydrologic parameter sheets.

Table 3 summarizes the pre-development peak flows rates obtained from the SWMHYMO model.

Table 3: Summary of Pre-Development Flow Rates

Return Period (Years)	Pre-Development Flow Rates (m ³ /s)		
	Outlet A (13.20 ha)	Outlet B (11.2 ha)	Outlet C (14.0 ha)
6 Hour Keifer Chu			
2	0.26	0.19	0.19
5	0.50	0.37	0.37
10	0.76	0.57	0.58
25	0.98	0.75	0.76
50	1.10	0.85	0.85
100	1.36	1.05	1.07
12 Hour SCS Type II			
2	0.33	0.20	0.20
5	0.70	0.44	0.45
10	1.01	0.64	0.64
25	1.43	0.91	0.91
50	1.75	1.12	1.13
100	2.09	1.34	1.35
24 Hour SCS Type II			
2	0.37	0.24	0.24
5	0.73	0.47	0.47
10	0.97	0.63	0.63
25	1.36	0.88	0.89
50	1.63	1.06	1.07
100	1.99	1.30	1.31
Regional (Timmins)	1.21	1.00	1.05

Pre-development SWMHYMO input and output files have been provided in **Appendix D**.

7.3.2 Post-Development Model Setup

The post-development model was prepared by replacing the pre-development catchments from the pre-development model with the post-development catchments identified in Section 7.2. Refer to **Figure 8** for the Post-Development Drainage Plan and **Appendix C** for hydrologic parameter sheets.

The proposed SWM Facility will be a stormwater management wet pond located on the northeastern side of the development that will provide the required stormwater quantity, quality and erosion controls. The stormwater facility will ultimately convey flows to Outlet B. The drainage area contributing to Outlet B has increased under proposed conditions; therefore, additional analysis was completed to assess regional flows downstream of Outlet B. The watercourse downstream of Outlet B flows between several existing residential dwellings north of Hidden Lake Road before being conveyed to the existing low-lying area to the north. The cross-section of the receiving channel was adopted from the topo performed on September 10, 2021 by Joe Topo. Analysis of the channel cross-section using Bentley FlowMaster (V8i) shows the channel can convey up to 1.13m³/s without overtopping the channel banks. Therefore, the SWM facility will be designed to control the 100-yr and Regional flows below 1.13m³/s to avoid negative impacts to the downstream properties at Outlet B.

A preliminary outlet structure has been designed as a multi-stage outlet to address both quality and quantity control requirements. The outlet structure will consist of a 120 mm diameter extended detention orifice positioned at the permanent pool elevation. A secondary orifice has been included above the extended detention storage elevation to control discharge from the pond for storms exceeding the 25 mm event. Storm events in excess of the 100-year event will be stored in the facility and safely conveyed downstream via an emergency spillway.

The ROUTE RESERVOIR routine was used to determine the volume of detention storage required to attenuate the post-development peak flows discharging to Outlet B to below pre-development levels. To meet quantity control requirements, it was concluded that approximately 7,652 m³ of active storage is required to attenuate the peak flow from the 100-year event to below pre-development levels and approximately 10,360m³ of storage is required to control the regional flows below the maximum capacity of 1.13m³/s provided in the downstream channel.

The results of the post-development model are summarized in **Tables 4** and **5** below.

Table 4: Summary of SWM Facility Storage Volumes

Return Period (Years)	Active Storage Required (m ³)		
	6 Hour Keifer Chu	12 Hour SCS Type II	24 Hour SCS Type II
2	2248	2179	2344
5	3528	3434	3636
10	4850	4425	4451
25	5929	5523	5578
50	6476	6385	6384
100	7652	7279	7421

Table 5: Summary of Pre- and Post-Development Flow Rates

Return Period (Years)	Outlet A		Outlet B		Outlet C	
	Pre-Development (13.2 ha)	Post-Development (4.5 ha)	Pre-Development (11.2 ha)	Post-Development (22.80 ha)	Pre-Development (14.0 ha)	Post-Development (11.0 ha)
6 Hour Keifer Chu						
2	0.26	0.10	0.19	0.10	0.24	0.13
5	0.50	0.18	0.37	0.18	0.47	0.27
10	0.76	0.27	0.57	0.29	0.63	0.42
25	0.98	0.34	0.75	0.39	0.89	0.56
50	1.10	0.38	0.85	0.45	1.07	0.64
100	1.36	0.47	1.05	0.59	1.31	0.81
12 Hour SCS Type II						
2	0.33	0.11	0.20	0.12	0.20	0.14
5	0.70	0.24	0.44	0.25	0.45	0.31
10	1.01	0.34	0.64	0.36	0.64	0.45
25	1.43	0.47	0.91	0.52	0.91	0.65
50	1.75	0.58	1.12	0.63	1.13	0.82
100	2.09	0.69	1.34	0.77	1.35	0.99
24 Hour SCS Type II						
2	0.37	0.13	0.24	0.14	0.24	0.16
5	0.73	0.25	0.47	0.26	0.47	0.33
10	0.97	0.33	0.63	0.34	0.63	0.44
25	1.36	0.45	0.88	0.49	0.89	0.63
50	1.63	0.54	1.06	0.60	1.07	0.77
100	1.99	0.66	1.30	0.75	1.31	0.97
Regional (Timmins)	1.21	0.42	1.00	1.08	1.05	0.81

As evidenced by **Tables 4** and **5**, 'Post-to-Pre' quantity control has been provided for all storm events up to and including the 100-year event for all outlets. Safe conveyance of the Regional event has been provided at Outlet B (SWM Facility).

The post-development Regional peak flows have decreased at both Outlet A and C. As outlined in Section 8.0, the infrastructure downstream of Outlet A and C is deficient under existing conditions. The existing culverts downstream of Outlet B have sufficient capacity for larger storm events, up to and including the 100-year event, except for Culverts 2 and 6, which have capacity for storms up to and including the 50-year event. Therefore, by diverting Regional peak flows in post-development conditions to Outlet B, the overall flood potential is reduced at Outlet A and C. SWMHYMO post-development output files have been provided in **Appendix D**.

7.4 Water Quality & Erosion Control

An end-of-pipe SWM Facility will provide stormwater quality control to an Enhanced Protection Level (Stormwater Management and Design Manual, MECP, 2003) and appropriate erosion control. A comparison between the provided and required volumes for permanent pool and extended detention have been provided in **Table 6**.

Erosion control will be principally achieved by incorporating the erosion control requirements into the extended detention operation of the proposed stormwater management facility. Sizing was based

on providing 24-hour drawdown of the runoff volume produced during a 25 mm design storm event. Based on a contributing drainage area of 19.7 ha, the required water quality volume for a wet pond is 105 m³/ha to provide an enhanced level of treatment (Stormwater Management and Design Manual, MECP, 2003). This water quality volume consists of 65 m³/ha for permanent pool and 40 m³/ha for extended detention, respectively. The required and provided water quality volumes have been summarized in **Table 6** below. Refer to **Appendix E** for relevant water quality and extended detention calculations.

Table 6: SWM Facility Quality Control Characteristics

	Required Volume (m3)	Provided Volume (m3)
Permanent Pool	1281	1350
MECP Extended Detention	788	1290
Erosion Control	1290	1290

7.5 Stormwater Management Facility Operating Characteristics

Taking into account the water quantity and quality storage requirements, a preliminary design for the SWM Facility has been completed to demonstrate that the SWM block is adequately sized. A preliminary operating profile of the SWM Facility is presented in **Table 7** below.

Table 7: SWM Facility Operating Characteristics

Component	Elevation (m)	Storage Required (m ³)	Storage Provided (m ³)
Bottom	215.15	---	---
Permanent Pool	216.05	1281	1350 (dead storage)
Extended Detention	216.25	1290	1290
100-Year High Water Level	217.55	7652	7900
Top of Berm	218.75	---	13600

As evidenced by **Table 7** the pond presented herein is sufficiently sized to provide the required stormwater quantity and quality controls.

The outlet control structure will be located at the north end of the proposed SWM facility and will include 3 culvert crossings on "Street B" prior to being discharged to a proposed engineered conveyance channel. The channel will extend north along the west side of the existing farm laneway and discharge into the existing 900 mm CSP culvert crossing at Hidden Lake Road (Outlet B). Outlet B is the nearest suitable location to discharge stormwater from the Subject Lands, as determined through field reconnaissance and existing topography.

Details with respect to the operation of the SWM facility including specific inverts, detailed grading, inlet locations, sediment forebays, and control structures will be specified during detailed design. Permits and other regulatory instruments such as an Environmental Compliance Approval (MECP) and GSCA approval will be secured prior to construction.

The preliminary design of the SWM Facility has been presented in **Figure 10**. Refer to **Appendix E** for relevant SWM facility calculations.

8.0 EXTERNAL DRAINAGE CORRIDOR ANALYSIS

As indicated in the introduction (Section 1.0), the Town previously requested that the drainage corridor downstream of the Subject Lands be evaluated to determine the conditions of the existing

corridor, identify deficiencies, and recommend upgrades. Given the location of the Alta Phase II lands within Subwatersheds 21A and 22, the external drainage corridor analysis presented herein is limited to these subwatersheds.

The objectives of the external drainage corridor analysis are to evaluate the conditions of existing hydraulic structures within the respective subwatersheds and to determine their hydraulic capacities to:

- Demonstrate that there are no negative impacts to the external conveyance corridor as a result of the proposed development of the Subject Lands;
- Determine if the existing structures have sufficient capacity to meet the requirements stipulated in the Ministry of Transportation's Directive B-100; and,
- Provide recommendations for upgrades and/or maintenance to existing structures.

As discussed in Section 7.0, water quantity control has been incorporated into the overall SWM strategy of Alta Phase II to ensure that post-development peak flow rates are below pre-development levels at the various outlet locations. Therefore, the downstream drainage corridor analysis presented herein is limited to the post-development drainage conditions scenario upon full build-out of Alta Phase II.

The drainage analysis involved a review of background information, field reconnaissance, supplementary topographic and structure survey, an extension of hydrologic modelling, and detailed hydraulic calculations. A detailed description and summary of results for each of the elements of the analysis are described for the respective study subwatersheds below.

8.1 Subwatershed 21A

As explained in Section 7.0, field reconnaissance conducted by Crozier staff identified drainage patterns within Subwatershed 21, which differed from that reported in the CCSS. To address the observed drainage patterns, a new subwatershed was delineated and is referred to as Subwatershed 21A in this report. Drainage from a portion of Subwatershed 21A was described in detail in Section 7.1, however, given the subwatershed-scale scope of this supplementary analysis, additional subcatchments were delineated to account for the entire drainage area contributing to its outlet at Georgian Bay. Refer to **Figure 11** for the post-development subwatershed plan considering the entire Subwatershed 21A drainage area. When compared to **Figure 8** (Post-Development Drainage Plan), it is important to note that additional subcatchments were introduced around the Subject Lands to account for the entire lands contributing to the outlet of Subwatershed 21A at Georgian Bay. These additional subcatchments were appended to the previously described SWMHYMO hydrologic model to provide peak flow estimates at selected points of interest.

Upon development of Alta Phase II and as illustrated in **Figure 11**, the area contributing to the outlet of Subwatershed 21A is approximately 43 ha, which includes the site and external lands. Existing residential homes fronting Hidden Lake Road and the Craigleith Provincial Park are located within the subwatershed.

Drainage from the tablelands of the Escarpment emanates as sheet flow toward Watercourse 21A, which is an incised watercourse as it traverses north across the Escarpment face. Watercourse 21A accepts additional drainage as it passes across the Subject Lands and the Nipissing Ridge. At the base of Nipissing Ridge, the watercourse follows a 90-degree bend at Hidden Lake Road (Outlet C) and flows north along the east side of Hidden Lake Road beneath six (6) driveway culverts (all 1100 mm x 700 mm CSPA) before reaching the Georgian Trail. Watercourse 21A then passes beneath Georgian Trail via a pair of 750 mm dia. CSP culverts and Highway 26 via a 1650 mm by 1020 mm CSPA culvert before discharging to Georgian Bay at the north limit of Craigleith Provincial Park.

As noted in Section 7.1, the possibility of spill flow conditions exists from Watercourse 21A to Watercourse 21 via a broad draw extending from the forested area near the 90-degree bend at Hidden Lake Road to Watercourse 21. It is speculated that prior to the construction of the sewage leaching bed for Craigleith Provincial Park, this may have been the original drainage route of Watercourse 21A. (Watercourse 21 conveys drainage beneath the Georgian Trail via a 1600 mm by 900 mm CSPA culvert and beneath Highway 26 via a 1.25 m by 2.45 m concrete box culvert).

Hydrologic Modeling & Results

The SWMHYMO hydrologic model prepared for the Subject Lands was extended to account for the entire drainage area contributing to the outlet of Subwatershed 21A. Additional sub-catchments were appended to the post-development drainage plan, as reflected in **Figure 11**, resulting in a total subwatershed area of approximately 43 ha.

The hydrologic model produced peak flows at two points of interest: Outlet C and the subwatershed outlet at Georgian Bay. The peak flow established at the subwatershed outlet was utilized to evaluate the hydraulics of the existing culverts beneath Georgian Trail and Highway 26. The culverts within Craigleith Provincial Park were not analyzed as they are located near the outlet of the subwatershed and on lands not owned by the municipality.

The additional hydrologic parameters and the SWMHYMO model input and output files are found in **Appendix C** and **D**, respectively. Results from the hydrologic modelling for the 2-year and 100-year storm events are summarized in **Table 8**, and the results from the remainder of the storm events are contained in the model output files.

Table 8: Summary of Subwatershed 21A Post-Development Peak Flows (m³/s)

Return Period (Years)	KCHU		SCS12		SCS24	
	Outlet C (36.1 ha)	Subwatershed 21A Outlet (43.1 ha)	Outlet C (36.1 ha)	Subwatershed 21A Outlet (43.1 ha)	Outlet C (36.1 ha)	Subwatershed 21A Outlet (43.1 ha)
2	0.48	0.61	0.47	0.59	0.56	0.70
100	2.85	3.51	3.17	3.87	3.09	3.77

The peak flows listed in **Table 8** were used in conjunction with the hydraulic calculations described below to evaluate the hydraulic condition and capacity of the culverts downstream of the Subject Lands to the outlet at Georgian Bay.

Hydraulic Modeling & Results

The major drainage corridors within Subwatershed 21A were described above. The location and size of the main hydraulic structures located along the drainage corridors are identified in **Figure 11**. Each culvert was surveyed to determine its size, extent, and relationship to adjacent ground elevation. Photographs of each of the structures were also taken to document the existing conditions and recommend maintenance or improvements.

The hydraulic capacity of each of the structures was computed using the CulvertMaster computer model and compared to the peak flows generated using SWMHYMO as presented in **Table 8**. Input data into the CulvertMaster model includes the size of the hydraulic structure, type of material, upstream and downstream invert elevation, tailwater elevation and maximum headwater elevation.

To determine the tailwater conditions, a FlowMaster model was used to compute the depth of flow at natural channel sections immediately downstream of each hydraulic structure. The resulting normal depth was then inputted into the CulvertMaster model as the tailwater elevation to establish whether the culvert will operate as inlet or outlet control under a given peak flow condition.

Results from the hydraulic calculations are presented in **Appendix F** and summarized on the culvert data sheets found in **Appendix G**. The summary sheets include culvert identification and location, characteristic hydraulic rating curves, return period capacity, photographs and key dimensions. A summary of the results from the hydraulic analysis of structures within Subwatershed 21A is listed in **Table 9**.

Table 9: Summary of Hydraulic Structure Characteristics Within Subwatershed 21A

Culvert ID	Culvert Location	Culvert Size / Type	Maximum Capacity (m ³ /s)	100-Year Peak Flow ¹ (m ³ /s)	Return Period Capacity
9	All Private Driveways (East side of Hidden Lake Road)	1100 x 700 mm CSPA (typ.)	0.5	3.14	< 2 Year
10	Georgian Trail	2 x 750 mm CSP	1.1	3.84	< 5 Year
11	Highway 26	1650 x 1020 mm CSPA	2.7	3.84	< 50 Year

Note: Return Period Capacity based on conservative peak flows without considering potential spill flow analysis to Watercourse 21.

¹100-year peak flow from 12-hour SCS Type II storm (largest flow).

It is evident from **Table 9** that the hydraulic capacities of all structures located along the drainage corridor of Subwatershed 21A are below the 100-year peak flows at the respective locations. Culvert No. 9 represents a series of six driveway culverts along the east side of the Hidden Lake Road right-of-way which are all similar in shape and hydraulic characteristics. In general, these driveway culverts have capacities less than the 2-year storm event. Although it is preferable that the driveway culverts convey flows of at least the 2-year event, replacement or improvement of these culverts is at the discretion of the Town. Improvements such as the construction of headwalls and annual maintenance should be considered to optimize their hydraulic capacities.

Culvert No. 11 conveys runoff beneath Highway 26 and has greater capacity than the other structures. It can convey the 25-year storm event as required by the MTO Drainage Directive B-100.

Based on the above hydraulic analysis, the entire Watercourse 21A drainage corridor downstream of the Subject Lands, except for Culvert 11, is deficient despite the slightly reduced peak flows within the corridor because of the proposed Alta Phase II development. It should also be noted that the drainage corridor is deficient in a pre-development state. Replacement of the existing culverts may be considered as a remedial measure. However, given the number of culverts and extent of reconstruction to upgrade this drainage corridor, it may be prudent to re-establish the original Subwatershed 21 boundaries by redirecting runoff from Subwatershed 21A to Watercourse 21, via the previously described spill flow route. Based on the 1.25 m by 2.45 m concrete box culvert beneath Highway 26 relative to its existing drainage area of approximately 40 ha, the use of Watercourse 21 to convey drainage from the additional Subwatershed 21A lands may resolve the existing capacity issues along the Watercourse 21A drainage corridor. Furthermore, the feasibility of this remedial strategy would have to be investigated from a technical perspective and the Town would have to enter into negotiations with the Ministry of Natural Resources, who owns the Craigeleith Provincial Park. This drainage investigation should be completed during the detailed design of Hidden Lake Road to potentially reduce the construction costs associated with upgrading this drainage corridor.

Finally, all culverts within the public ROWs along Watercourse 21A were observed to be in fair operating condition with respect to inlet/outlet condition and sediment accumulation. However, annual inspection and maintenance of these structures should be considered to optimize their hydraulic capacities.

8.2 Subwatershed 22

As explained in Section 7.0, field reconnaissance conducted by Crozier staff lead to a revised delineation of Subwatershed 22 across the Subject Lands and further downstream. The external drainage corridor analysis is based on the updated subwatershed delineation and peak flows generated from the current hydrologic modelling. Refer to **Figure 11** for a delineation of Subwatershed 22 and its various subcatchments. Similar to that of Subwatershed 21A, additional sub-catchments were appended to the previously described SWMHYMO hydrologic model to provide peak flow estimates at selected points of interest from the Subject Lands to the outlet at Georgian Bay.

Under post-development conditions, the area contributing to the outlet of Subwatershed 22 is approximately 70 ha, which includes the Subject Lands, the Escarpment face, the Nipissing Ridge, and the Hidden Lake area. Existing single-family residential lots and a condominium development are located below the Nipissing Ridge between Hidden Lake Road and James Street. The Georgian Trail and Highway 26 traverse the north portion of Subwatershed 22 which terminates at the shoreline of Georgian Bay.

Drainage from upstream external and internal lands will be directed to Outlets A and B within Subwatershed 22. A small portion of the Alta Phase II and upstream external lands will contribute to Outlet C which is located within Subwatershed 21A (see Section 7.2).

Outlet A consists of an 825 mm dia. CSP culvert and Outlet B consists of a 900 mm dia. culvert, both of which convey runoff beneath Hidden Lake Road. The runoff is then conveyed across private properties within defined watercourses before dissipating into an existing low-lying area between the base of the Nipissing Ridge and the Georgian Trail. This low area is poorly drained and measures approximately 130 m long by 30 m wide, on average. Immediately east of this low area is Hidden Lake, which accepts overflow from the low area during periods of elevated runoff. The low-lying area ultimately drains north beneath Georgian Trail and Highway 26 via a series of culverts before reaching the outlet of Subwatershed 22 at Georgian Bay.

Hydrologic Modeling & Results

Similar to that of Subwatershed 21A, the SWMHYMO hydrologic model was used to establish peak flows throughout Subwatershed 22. The model produced peak flows at three points of interest: Outlet A, Outlet B and the subwatershed outlet at Georgian Bay. The natural detention storage of the existing low-lying area upstream of the Georgian Trail was accounted for in the hydrologic modelling. A stage-storage-discharge relationship was developed based on available background information and incorporated into the hydrologic modelling as a ROUTE RESERVOIR routine to account for the natural attenuation.

The additional hydrologic parameters and the SWMHYMO model input and output files are found in **Appendix C** and **D**, respectively. Results from the hydrologic modelling for the 2-year and 100-year storm events are summarized in **Table 10** and the results from the remainder of the storm events are contained in the model output files.

Table 10: Summary of Subwatershed (SWS) 22 Post-Development Peak Flows (m³/s)

Return Period (Years)	KCHU			SCS12			SCS24		
	Outlet A (4.5 ha)	Outlet B (22.8 ha)	SWS 22 Outlet (70.0 ha)	Outlet A (4.5 ha)	Outlet B (22.8 ha)	SWS 22 Outlet (70.0 ha)	Outlet A (4.5 ha)	Outlet B (22.8 ha)	SWS 22 Outlet (70.0 ha)
2	0.10	0.10	0.23	0.11	0.12	0.23	0.13	0.14	0.24
100	0.47	0.59	0.68	0.69	0.73	0.73	0.66	0.75	0.72

It is evident from **Table 10** that the natural attenuation provided in the low-lying area adjacent to the Georgian Trail significantly reduces the peak flows within the subwatershed. Although the contributing drainage area to the outlet of Subwatershed 22A is larger than Subwatershed 21A, it produces lower peak flows because there are significant natural storage areas within the watershed to dampen the peak flow, unlike Subwatershed 21A. The peak flows listed above were used in conjunction with the hydraulic calculations described below to evaluate the hydraulic condition and capacity of the culverts downstream of Subject Lands to the outlet at Georgian Bay.

Hydraulic Modeling & Results

The major drainage corridors within Subwatershed 22 were described above. The location and size of the main hydraulic structures located along the aforementioned drainage corridors are identified in **Figure 12**. Similar to the exercise described for Subwatershed 21A, each of the identified culverts were surveyed to determine their size, extent and relationship with adjacent ground elevation.

The hydraulic capacity of each of the structures was computed using the methodology described in Section 8.1 for Subwatershed 21A. Results from the hydraulic calculations are provided in **Appendix F** and are summarized on culvert data sheets found in **Appendix G**. These summary sheets include culvert identification and location, characteristic hydraulic rating curves, return period capacity, photographs and key dimensions. A summary of the results from the hydraulic analysis of structures within Subwatershed 21A is provided in **Table 11**.

Table 11: Summary of Hydraulic Structure Characteristics within Subwatershed 22

Culvert ID	Culvert Location	Culvert Size / Type	Maximum Capacity (m ³ /s)	100-Year Peak Flow ¹ (m ³ /s)	Return Period Capacity
1	Hidden Lake Road	825 mm CSP	1.2	0.69 ¹	> 100 Year
2	Private Driveway (Hidden Lake Road)	3 x 300 Conc.	0.6	0.69 ¹	> 50 Year
3	Private Driveway (Hidden Lake Road)	825 mm CSP	0.9	0.69 ¹	> 100 Year
4	Hidden Lake Road	900 mm CSP	1.9	0.75 ²	> 100 Year
5	Georgian Trail	825 mm CSP	1.3	0.73 ¹	> 100 Year
6	Rear Yard	750 mm CSP	0.7	0.73 ¹	> 50 Year
7	Private Driveway (Highway 26)	825 mm CSP	1.2	0.73 ¹	> 100 Year
8	Highway 26	1500 x 900 mm CSP	2.8	0.73 ¹	> 100 Year

¹Based on post-development conditions and implementation of SWM Facility within Alta Phase II. 100-year peak flow from 12-hour SCS Type II storm (largest flow).

²100-year peak flow from 24-hour SCS Type II storm (largest flow).

It is evident from **Table 11** that the hydraulic capacities of all structures located along the major drainage corridor within Subwatershed 22, except for Culvert 2 and 6, exceed the 100-year peak flows at their respective locations. However, the hydraulic capacities of Culverts 2 and 6 exceeds the 50-year peak flow. This exceeds the recommended culvert capacity requirements of MTO per Directive B-100. Replacement of these culverts with larger sizes is not warranted.

The culverts were also evaluated based on the factors that may influence their hydraulic capacities such as sediment build-up within the structure, blocked inlet and outlet from excessive vegetation or debris/sediment deposits, and damaged structures. Based on field reconnaissance conducted by Crozier staff, all culverts noted above were found to be in fair operating condition with the exception of Culvert No. 1, where significant sediment deposits were observed at the downstream end of the culvert. We recommend the cleanout of this culvert to ensure its hydraulic capacity is not compromised.

9.0 UTILITIES, SERVICES & SNOW STORAGE

The Subject Lands will be serviced with natural gas, telephone, hydro and cable TV. The design of such utilities will be coordinated with the local utility companies servicing the Town. Utilities are proposed to follow the alignment of the internal road network, with individual service connections to each lot.

The Subject Lands will also have solid waste management and mail delivery services. These services will be coordinated with local companies servicing the Town.

Snow storage areas for the Subject Lands will be specified during detailed design.

10.0 EROSION & SEDIMENT CONTROLS

All sediment and erosion controls will be installed prior to the commencement of any earthworks and maintained throughout until the site is stabilized or as directed by the Engineer, GSCA and/or Town. Controls are to be inspected regularly, after each significant rainfall and maintained in proper working condition. Erosion and sediment control measures to be considered include, but are not limited to, the following:

- Silt Fence

Silt fencing will be installed where required to intercept sheet flow. Heavy duty silt fence will be located around the perimeter of the work zone limits. It should be noted that additional silt fencing may be added based on field decisions by the Site Engineer and Owner prior to, during and following construction.

- Mud Mat

A mud mat will be installed at the main access points to the site (Hidden Lake Road and Alta Rad) to reduce the amount of mud tracking onto existing paved roadways during site servicing operations.

- Flow Check Dams

Temporary check dams will be utilized on-site to prevent any silt mitigation off-site during and after construction activities. These dams will promote the settling of suspended solids and will reduce flow velocities. Sediment accumulation will be monitored and removed as necessary.

- Dust Suppression

During earthwork activities, the Contractor will ensure that measures for dust suppression are provided as required, such as the application of water or lime.

11.0 CONCLUSIONS & RECOMMENDATIONS

Based on the foregoing, we conclude that the proposed Alta Phase II development in the Town of The Blue Mountains can be adequately serviced.

1. Access to the site will be provided via two public roadways, Hidden Lake Road and Alta Road. Municipal roads will be designed in accordance with Town of The Blue Mountains Standards.
2. The development will be serviced via a gravity sanitary sewer system that will drain to a new sewage pumping station to be constructed within Block 61. The proposed station will direct flows back to Alta Phase 1 and the Margaret Drive SPS.
3. Watermain will follow the alignment of the internal road network complete with all appurtenances and hydrants to meet Town Standards. The proposed watermain will be a looped system with connections to the existing watermain on the adjacent public streets.
4. A stormwater management facility is proposed to meet the stormwater quantity, quality and erosion control criteria, which uses Outlet B as the outlet.
5. The external drainage will be safely conveyed through the development via drainage channels to either the SWM facility or the pre-development drainage outlets.
6. The development will not aggravate drainage conditions downstream during storm events up to and including the 100-year event as demonstrated through the external drainage corridor analysis.
7. Upgrades to the drainage corridor along Watercourse 21A should be considered by the Town. Development of the Alta site will improve the existing drainage conditions in this area.
8. Utilities are available to service the site.
9. Sediment and erosion controls, as specified, will be effective in preventing and controlling sediment from migrating into nearby swales, ditches, and watercourses.

Therefore, we recommend approval of the relevant planning applications for the Subject Lands from the perspective of engineering servicing requirements.

Respectfully Submitted,

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APPENDIX A

Sanitary Flow Calculations

Alta Phase 2 Sanitary Demand

Developed Site Area	16.60 ha
Number of Residential Units	
Single Residential	60 Units
Person Per Residential Unit	
Single Residential (per TOBM Engineering Standards, 2009)	2.3 persons/unit
Total Residential Population	138 persons
Unit Sewage flows	
Residential (per TOBM Engineering Standards, 2009)	450 L/person-day
Infiltration (per TOBM Engineering Standards, 2009)	0.23 L/s/ha
Total Design Sewage Flows	
Infiltration/Inflow Residential	3.82 L/sec
Average Daily Residential Flow	0.72 L/sec
Residential Peak Factor (Harmon Formula)	4.20
Total Peak Daily Flow	6.84 L/sec

APPENDIX B

Water Demand & Fire Flow Calculations

Alta Phase 2 Water Demand

Developed Site Area	16.60 ha
Number of Residential Units	
Single Residential	60 Units
Person Per Residential Unit	
Single Residential (per TOBM Engineering Standards, 2009)	2.3 persons/unit
Total Residential Population	138 persons
<u>Domestic Water Design Flows</u>	
Residential (Per TOBM Engineering Standards, 2009)	450 L/C-day
<u>Total Domestic Water Design Flows</u>	
Average Residential Daily Flow	0.72 L/sec
Max Day Peak Factor (Per TOBM Engineering Standards, 2009)	2.00
Max Day Demand Flow	1.44 L/sec
Peak Hour Factor (Per TOBM Engineering Standards, 2009)	4.50
Peak Hour Flow	3.23 L/sec

Water Supply for Public Fire Protection - 1999
Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

1. An estimate of fire flow required for a given area may be determined by the formula:

$$F = 220 * C * \sqrt{A}$$

Where

- F = the required fire flow in litres per minute
C = coefficient related to the type of construction
= 1.5 for wood frame construction (structure essentially all combustible)
= 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior)
= 0.8 for non-combustible construction (unprotected metal structural components)
= 0.6 for fire-resistive construction (fully protected frame, floors, roof)
A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building considered.

2 number of floors

Ordinary Construction
1.0 C

500 sq.m. total floor area

Therefore F= 5,000 L/min (rounded to nearest 1000 L/min)

Fire flow determined above shall not exceed:

- 30,000 L/min for wood frame construction
30,000 L/min for ordinary construction
25,000 L/min for non-combustible construction
25,000 L/min for fire-resistive construction

2. Values obtained in No. 1 may be reduced by as much as 25% for occupancies having low contents fire hazard or may be increased by up to 25% surcharge for occupancies having a high fire hazard.

Non-Combustible	-25%	Free Burning	15%
Limited Combustible	-15%	Rapid Burning	25%
Combustible	No Charge		

Low fire Hazard occupancy for dwellings

15% reduction

750 L/min reduction

Note: Flow determined shall not be less than 2,000 L/min

3. Sprinklers - The value obtained in No. 2 above maybe reduce by up to 50% for complete automatic sprinkler protection.

No Automatic Sprinklers

0 L/min surcharge / reduction

0

Water Supply for Public Fire Protection - 1999
Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

4. Exposure - To the value obtained in No. 2, a percentage should be added for structures exposed within 45 metres by the fire area under consideration. The percentage shall depend upon the height, area, and construction of the building(s) being exposed, the separation, openings in the exposed building(s), the length and height of exposure, the provision of automatic sprinklers and/or outside sprinklers in the building(s) exposed, the occupancy of the exposed building(s) and the effect of hillside locations on the possible spread of fire.

Separation	Charge	Separation	Charge
0 to 3 m	25%	20.1 to 30 m	10%
3.1 to 10 m	20%	30.1 to 45 m	5%
10.1 to 20 m	15%		

Exposed buildings

Name	Distance	Charge	Surcharge
Lot 42	35	5%	212.5
Lot 6	15	15%	637.5
Lot 3	4	20%	850
Lot 5	4	20%	850

2,550 L/min Surcharge

Determine Required Fire Flow

No.1	5,000	
No. 2	750 reduction	
No. 3	0 reduction	
No. 4	2,550 surcharge	
Required Flow:	6,800 L/min	
Rounded to nearest 1000 L/min:	7,000 L/min	or 116.7 L/s 1,849 USGPM

Determine Required Fire Storage Volume

Flow from above	7,000 L/min
Required duration	2.00 hours
Therefore:	840,000 Litres or 840 cu.m. is the required fire storage volume.

Required Duration of Fire Flow	
Flow Required L/min	Duration (hours)
2,000 or less	1.0
3,000	1.25
4,000	1.5
5,000	1.75
6,000	2.0
8,000	2.0
10,000	2.0
12,000	2.5
14,000	3.0
16,000	3.5
18,000	4.0
20,000	4.5
22,000	5.0
24,000	5.5
26,000	6.0
28,000	6.5
30,000	7.0
32,000	7.5
34,000	8.0
36,000	8.5
38,000	9.0
40,000 and over	9.5

Calculation Check

Office of the Fire Marshall - Fire Protection Water Supply Guideline for Part 3 in the OBC (October 2006)

$Q = KVS_{TOT}$

- Q = minimum supply of water in litres (L)
- K = water supply coefficient
- V = total building volume in cubic metres
- S_{TOT} = total of spatial coefficient values from property line exposures on all sides

First Floor

- | | | |
|--------------------|------|--|
| K = | 23 | Group C building with combustible construction (Table 3.2.1) |
| V = | 3000 | 500 sqm floor area by 6 m height |
| S _{TOT} = | 2 | S _{TOT} Need Not Exceed 2.0 |

Q= 138000 L

Minimum Flow Rate 4500 L/min = 75 L/s

APPENDIX C

Hydrologic Parameters



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-1
 D.A. AREA (ha) 1.40

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-1

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	1.40
				0
				0
				0
Total Area				1.40

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc	0.08	98		98		98	0.05	98		98	0.13	12.50
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0.08		0		0		0.05		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc	0.92	73	0.00		0.00		0.35	79	0.00		1.27	94.99
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	0.92		0.00		0.00		0.35		0.00			

				Composite Area Calculations		Total Pervious Area		1.27
						Total Impervious Area		0.13
						% Impervious		9.11%
						Composite Curve Number		76.8
						Total Area Check		1.40

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.92	9.22	0.35	0.92		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.35	1.75	0.20	0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.13	0.26	0.95	0.13		0		0		0
Composite		1.40	8.02	Composite Runoff Coefficient							
											0.37

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	190	5	2.63%	0.6	0.10	0.54	0.36	0.36	0.14	0.10	0.40	0.27

Appropriate calculated time to peak:	0.27	Appropriate Method:	Airport
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Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-2
 D.A. AREA (ha) 5.80

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-2

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	5.80
				0
				0
				0
Total Area				5.80

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc		0.12	98		98		98		98		98	0.12	11.32
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0.12		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc		3.41	73	2.27	76	0.00		0.00		0.00		5.68	421.79
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		3.41		2.27		0.00		0.00		0.00			

				Composite Area Calculations		Total Pervious Area		5.68
						Total Impervious Area		0.12
						% Impervious		1.99%
						Composite Curve Number		74.7
						Total Area Check		5.80

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	3.41	34.11	0.35	3.41		0		0		0
Meadow	8	2.27	18.19	0.40	2.27		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.12	0.23	0.95	0.12		0		0		0
Composite		5.80	9.06	Composite Runoff Coefficient							0.38

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)	(m)			(m/s)							
Overland	270	7.5	2.78%	0.6	0.10	0.75	0.50	0.50	0.18	0.12	0.46	0.31

Appropriate calculated time to peak: 0.31 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-3
 D.A. AREA (ha) 4.90

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-3

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	4.90
				0
				0
				0
Total Area				4.90

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Ksc		98		98		98	0.01	98		98	0.01	0.98	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
Subtotal	0		0		0		0.01		0				

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Ksc	1.96	73	2.93	76	0.00		0.00		0.00		4.89	365.77	
	0	0.00		0.00		0.00		0.00		0.00	0.00	0.00	
	0	0.00		0.00		0.00		0.00		0.00	0.00	0.00	
	0	0.00		0.00		0.00		0.00		0.00	0.00	0.00	
Subtotal	1.96		2.93		0.00		0.00		0.00				
				Composite Area Calculations			Total Pervious Area			4.89			
							Total Impervious Area			0.01			
							% Impervious			0.20%			
							Composite Curve Number			74.8			
							Total Area Check			4.90			

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	1.96	19.56	0.35	1.96		0		0		0
Meadow	8	2.93	23.47	0.40	2.93		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.01	0.02	0.95	0.01		0		0		0
Composite		4.90	8.79	Composite Runoff Coefficient							0.38

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	425	11.5	2.71%	0.6	0.10	1.20	0.80	0.80	0.28	0.19	0.58	0.39

Appropriate calculated time to peak: 0.39 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-4
 D.A. AREA (ha) 2.00

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	2.00
				0
				0
				0
Total Area				2.00

Impervious Landuses Present:															
Roadway			Sidewalk			Driveway			Building			SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN			
Dc		98		98		98		98		98		0	0		
0		98		98		98		98		98		0	0		
0		98		98		98		98		98		0	0		
0		98		98		98		98		98		0	0		
Subtotal	0		0		0		0		0		0				

Pervious Landuses Present:															
Woodland			Meadow			Wetland			Lawn			Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN			
Dc	2.00	73	0.00		0.00		0.00		0.00		0.00	2.00	146.00		
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	0.00		
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	0.00		
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	0.00		
Subtotal	2.00		0.00		0.00		0.00		0.00		0.00				
				Composite Area Calculations				Total Pervious Area				2.00			
								Total Impervious Area				0			
								% Impervious				0%			
								Composite Curve Number				73.0			
								Total Area Check				2.00			

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.00	20.00	0.52	2.00		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		2.00	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	109	12.5	11.47%	0.6	0.20	0.15	0.10	0.10	0.06	0.04	0.15	0.10

Appropriate calculated time to peak: 0.04 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alfa Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-5
 D.A. AREA (ha) 0.90

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-5

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	0.90
				0
				0
				0
Total Area				0.90

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	0.90	73	0.00		0.00		0.00		0.00		0.90	65.70
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	0.90		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			0.90		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			0.90		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.90	9.00	0.52	0.90		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		0.90	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	111	12.5	11.26%	0.6	0.20	0.15	0.10	0.10	0.07	0.04	0.15	0.10

Appropriate calculated time to peak: 0.04 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre INT-6
 D.A. AREA (ha) 0.70

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre INT-6

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	0.70
				0
				0
				0
Total Area				0.70

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			
Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	0.70	73	0.00		0.00		0.00		0.00		0.70	51.10
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	0.70		0.00		0.00		0.00		0.00			
Composite Area Calculations											Total Pervious Area	
											0.70	
											Total Impervious Area	
											0	
											% Impervious	
											0.00%	
											Composite Curve Number	
											73.0	
											Total Area Check	
											0.70	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.70	7.00	0.52	0.70		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		0.70	10.00	Composite Runoff Coefficient							
											0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)	(m)			(m/s)							
Overland	110	12.5	11.36%	0.6	0.20	0.15	0.10	0.10	0.07	0.04	0.15	0.10

Appropriate calculated time to peak: 0.04 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre UNC-4
 D.A. AREA (ha) 3.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre UNC-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Waterloo Sandy Loam	Wsl	A	100.0	3.20
				0
				0
				0
Total Area				3.20

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Wsl	0.12	98		98		98		98		98	0.116	11.368
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0.12		0		0		0		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Wsl	3.08	32	0.00		0.00		0.00		0.00		3.08	98.69
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	3.08		0.00		0.00		0.00		0.00			

				Composite Area Calculations		Total Pervious Area		3.08	
						Total Impervious Area		0.116	
						% Impervious		3.63%	
						Composite Curve Number		34.4	
						Total Area Check		3.20	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Waterloo Sandy		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	3.08	30.84	0.18	3.08		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.12	0.23	0.95	0		0		0		0
Composite		3.20	9.71	Composite Runoff Coefficient							
											0.21

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	350	25	7.14%	0.6	0.16	0.61	0.41	0.41	0.20	0.13	0.47	0.32

Appropriate calculated time to peak: 0.32 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME
 D.A. AREA (ha) **3.50**

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre EXT-1

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	3.50
				0
				0
				0
Total Area				3.50

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc			98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		3.50	73	0.00		0.00		0.00		0.00		3.50	255.50
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		3.50		0.00		0.00		0.00		0.00			

					Composite Area Calculations		Total Pervious Area		3.50	
							Total Impervious Area		0	
							% Impervious		0.00%	
							Composite Curve Number		73.0	
							Total Area Check		3.50	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				0		0		0			
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	3.50	35.00	0.52	3.50		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		3.50	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	460	160	34.78%	0.6	0.35	0.36	0.24	0.24	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: **0.13** Appropriate Method: **Bransby Williams**



Project Name: Alfa Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre EXT-2
 D.A. AREA (ha) 4.10

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre EXT-2

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	4.10
				0
				0
				0
Total Area				4.10

Impervious Landuses Present:															
Roadway			Sidewalk			Driveway			Building			SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	CN	Area	A*CN	
Dc		98		98		98		98		98		98	0	0	
	0	98		98		98		98		98		98	0	0	
	0	98		98		98		98		98		98	0	0	
	0	98		98		98		98		98		98	0	0	
Subtotal	0		0		0		0		0		0				

Pervious Landuses Present:																
Woodland			Meadow			Wetland			Lawn			Cultivated			Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	CN	Area	A*CN		
Dc	4.10	73	0.00		0.00		0.00		0.00		0.00		4.10	299.30		
	0	0.00	0.00		0.00		0.00		0.00		0.00		0.00	0.00		
	0	0.00	0.00		0.00		0.00		0.00		0.00		0.00	0.00		
	0	0.00	0.00		0.00		0.00		0.00		0.00		0.00	0.00		
Subtotal	4.10		0.00		0.00		0.00		0.00		0.00					
							Composite Area Calculations			Total Pervious Area			4.10			
										Total Impervious Area			0			
										% Impervious			0.00%			
										Composite Curve Number			73.0			
										Total Area Check			4.10			

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0		
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	4.10	41.00	0.52	4.10		0		0		0	2.13
Meadow	8	0.00	0.00		0		0		0		0	0.00
Wetland	16	0.00	0.00		0		0		0		0	0.00
Lawn	5	0.00	0.00		0		0		0		0	0.00
Cultivated	7	0.00	0.00		0		0		0		0	0.00
Impervious	2	0.00	0.00		0		0		0		0	0.00
Composite		4.10	10.00	Composite Runoff Coefficient								0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			TP (hr)				
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.18	0.12	0.21	0.14

Appropriate calculated time to peak: 0.12 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre EXT-3
 D.A. AREA (ha) 2.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre EXT-3

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	2.20
				0
				0
				0
Total Area				2.20

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc			98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		2.20	73	0.00		0.00		0.00		0.00		2.20	160.60
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		2.20		0.00		0.00		0.00		0.00			

					Composite Area Calculations		Total Pervious Area			2.20	
							Total Impervious Area			0	
							% Impervious			0.00%	
							Composite Curve Number			73.0	
							Total Area Check			2.20	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.20	22.00	0.52	2.20		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		2.20	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: 0.13 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre EXT-4
 D.A. AREA (ha) 2.60

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre EXT-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	2.60
				0
				0
				0
Total Area				2.60

Impervious Landuses Present:													
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals		
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc		98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
Subtotal	0		0		0		0		0				

Pervious Landuses Present:													
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals		
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc	2.60	73	0.00		0.00		0.00		0.00		2.60	189.80	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
Subtotal	2.60		0.00		0.00		0.00		0.00				
				Composite Area Calculations			Total Pervious Area			2.60			
							Total Impervious Area			0			
							% Impervious			0.00%			
							Composite Curve Number			73.0			
							Total Area Check			2.60			

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.60	26.00	0.52	2.60		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		2.60	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: 0.13 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-04-21
 By: Z. Holland

D.A. NAME Pre EXT-5
 D.A. AREA (ha) 5.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Pre EXT-5

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	5.20
				0
				0
				0
Total Area				5.20

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	5.20	73	0.00		0.00		0.00		0.00		5.20	379.60
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	5.20		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			5.20		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			5.20		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	5.20	52.00	0.52	5.20		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		5.20	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)							
Overland	415	140	33.73%	0.6	0.35	0.33	0.22	0.22	0.17	0.11	0.20	0.13

Appropriate calculated time to peak: 0.11 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2022-02-11
 By: J. Kerschbaumer

D.A. NAME Post INT-1
 D.A. AREA (ha) 8.60

Hydrologic Parameters: CALIB STANDHYD Command
Post Development Drainage Area: Catchment Post INT-1

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area
Kemble Silty Clay	Ksc	C	100.0	8.6
				0
				0
				0
Total Area Check				8.6

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN
Ksc	1.05	98		98	0.26	98	2.40	98		98	3.71	363.43
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal Area	1.05		0		0.26		2.40		0		3.71	

Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN
Ksc	0		0		0		4.89	79	0		4.89	386.43
0	0		0		0		0		0		0	0
0	0		0		0		0		0		0	0
0	0		0		0		0		0		0	0
Subtotal Area	0		0		0		4.89		0			

	Pervious Area Calculations	Total Pervious Area	4.89
		Composite Pervious Curve Number	79
	Impervious Area Calculations	Total Directly Connected Area	1.44
		Total Indirectly Connected Area	2.27
		Total Impervious Area	3.71
		% X imp	16.8
		% T imp	43.1
Total Area Check			8.60

Initial Abstraction and Tp Calculations

Landuse	IA (mm)	Area (ha)	A * IA
Woodland	10	0	0
Meadow	8	0	0
Wetland	16	0	0
Lawn	5	4.89	24.46
Cultivated	7	0	0

Land Use	IA (mm)	Slope (%)	Travel Length (m)	Manning's n
Pervious	5.0	2	65	0.25
Impervious	2.0	0.5	239	0.013



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-22
 By: Z. Holland

D.A. NAME
 D.A. AREA (ha) **Post INT-2**
3.00

Hydrologic Parameters: CALIB STANDHYD Command
Post Development Drainage Area: Catchment Post INT-2

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area
Dunedin Clay	Dc	C	100.0	3
				0
				0
				0
Total Area Check				3

Impervious Landuses Present:													
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals		
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN	
Dc	0.39	98		98	0.07	98	0.48	98		98	0.93	91.23	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
Subtotal Area	0.39		0		0.07		0.48		0		0.93		

Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals		
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN	
Dc	0		0		0		2.07	79	0		2.07	163.46	
0	0		0		0		0		0		0	0	
0	0		0		0		0		0		0	0	
0	0		0		0		0		0		0	0	
Subtotal Area	0		0		0		2.07		0				

	Pervious Area Calculations		Total Pervious Area		2.07	
			Composite Pervious Curve Number		79	
			Total Directly Connected Area		0.45	
			Total Indirectly Connected Area		0.48	
			Total Impervious Area		0.93	
			% X imp		15.0	
				% T imp		31.0
				Total Area Check		3.00

Initial Abstraction and Tp Calculations

Landuse	IA (mm)	Area (ha)	A * IA
Woodland	10	0	0
Meadow	8	0	0
Wetland	16	0	0
Lawn	5	2.07	10.35
Cultivated	7	0	0

Land Use	IA (mm)	Slope (%)	Travel Length (m)	Manning's n
Pervious	5.0	2	65	0.25
Impervious	2.0	0.5	141	0.013



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-22
 By: Z. Holland

D.A. NAME Post INT-3
 D.A. AREA (ha) 0.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post INT-3

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	0.20
				0
				0
				0
Total Area				0.20

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc		98		98		98		98		98	0	0.00	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
Subtotal	0		0		0		0.00		0				

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc	0.20	73	0.00		0.00		0.00		0.00		0.20	14.60	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
Subtotal	0.20		0.00		0.00		0.00		0.00				

				Composite Area Calculations		Total Pervious Area		0.20	
						Total Impervious Area		0	
						% Impervious		0.00%	
						Composite Curve Number		73.0	
						Total Area Check		0.20	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.20	2.00	0.52	0.20		0		0		0
Meadow	8	0.00	0.00		0.00		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0.00		0		0		0
Composite		0.20	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)							
Overland	37	5	13.51%	0.6	0.22	0.05	0.03	0.03	0.02	0.02	0.08	0.05

Appropriate calculated time to peak: 0.02 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-22
 By: Z. Holland

D.A. NAME Post INT-4
 D.A. AREA (ha) 0.60

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post INT-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	0.60
				0
				0
				0
Total Area				0.60

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0.00
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0		0		0		0.00		0			

Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	0.60	73	0.00		0.00		0.00		0.00		0.60	43.80
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	0.60		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			0.60		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			0.60		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.60	6.00	0.52	0.60		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		0.60	10.00	Composite Runoff Coefficient							
											0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	30	5	16.67%	0.6	0.24	0.03	0.02	0.02	0.02	0.01	0.07	0.05

Appropriate calculated time to peak: 0.01 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post INT-5
 D.A. AREA (ha) 0.10

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post INT-5

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	0.10
				0
				0
				0
Total Area				0.10

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0.00
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0		0		0		0.00		0			

Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	0.10	73	0.00		0.00		0.00		0.00		0.10	7.30
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	0.10		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			0.10		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			0.10		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	0.10	1.00	0.52	0.10		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		0.10	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	17	2.5	14.71%	0.6	0.23	0.02	0.01	0.01	0.01	0.01	0.05	0.04

Appropriate calculated time to peak: 0.01 Appropriate Method: Bransby Williams

Note: Minimum time to peak set to 0.05 hr for SWMHYMO model stability.



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post UNC-1
 D.A. AREA (ha) 0.80

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post UNC-1

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	0.80
				0
				0
				0
Total Area				0.80

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc		0.08	98		98		98	0.05	98		98	0	12.50
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0.08		0		0		0.05		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc		0.00	73	0.00		0.00		0.67	79	0.00		0.67	53.13
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		0.00		0.00		0.00		0.67		0.00			

Composite Area Calculations										Total Pervious Area		0.67	
										Total Impervious Area		0.1275	
										% Impervious		15.94%	
										Composite Curve Number		82.0	
										Total Area Check		0.80	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay		0		0		0		
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	0.00	0.00	0.20	0		0		0		0	0.00
Meadow	8	0.00	0.00		0		0		0		0.00	
Wetland	16	0.00	0.00		0		0		0		0.00	
Lawn	5	0.67	3.36		1		0		0		0.13	
Cultivated	7	0.00	0.00		0		0		0		0.00	
Impervious	2	0.13	0.26	0.95	0		0		0	0	0.12	
Composite		0.80	4.52	Composite Runoff Coefficient								0.32



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post UNC-2
 D.A. AREA (ha) 1.50

Hydrologic Parameters: CALIB STANDHYD Command
Post Development Drainage Area: Catchment Post UNC-2

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area
Kemble Silty Clay	Ksc	C	100.0	1.5
				0
				0
				0
Total Area Check				1.5

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN
Ksc	0.09	98		98	0.02	98	0.22	98		98	0.33	32.53
	0	98		98		98		98		98	0	0
		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal Area	0.09		0		0.02		0.22		0		0.33	

Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals		
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN	
Ksc	0		0		0		1.17	79	0		1.17	92.28	
0	0		0		0		0		0		0	0	
0	0		0		0		0		0		0	0	
0	0		0		0		0		0		0	0	
Subtotal Area	0		0		0		1.17		0				

	Pervious Area Calculations	Total Pervious Area	1.17
		Composite Pervious Curve Number	79
	Impervious Area Calculations	Total Directly Connected Area	0.11
		Total Indirectly Connected Area	0.22
		Total Impervious Area	0.33
		% X imp	7.5
		% T imp	22.1
Total Area Check		1.50	

Initial Abstraction and Tp Calculations

Landuse	IA (mm)	Area (ha)	A * IA
Woodland	10	0	0
Meadow	8	0	0
Wetland	16	0	0
Lawn	5	1.17	5.84
Cultivated	7	0	0

Land Use	IA (mm)	Slope (%)	Travel Length (m)	Manning's n
Pervious	5.0	2	65	0.25
Impervious	2.0	0.5	100	0.013



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2022-02-11
 By: J. Kerschbaumer

D.A. NAME Post UNC-3
 D.A. AREA (ha) 2.00

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post UNC-3

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	2.00
				0
				0
				0
Total Area				2.00

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc			98		98		98	0.08	98		98	0.08	7.99
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0.00		0		0		0.08		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Ksc		1.48	73	0.00		0.00		0.44	79	0.00		1.92	142.71
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		1.48		0.00		0.00		0.44		0.00			

Composite Area Calculations								Total Pervious Area		1.92
								Total Impervious Area		0.0815
								% Impervious		4.08%
								Composite Curve Number		75.3
								Total Area Check		2.00

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	1.48	14.76	0.52	1.48		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.44	2.21	0.20	0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.08	0.16	0.95	0		0		0		0
Composite		2.00	8.57	Composite Runoff Coefficient							
											0.47

Time to Peak Inputs						Uplands			Bransby Williams		Airport		
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)	
Overland	142	25	17.61%	0.6	0.25	0.16	0.10	0.10	0.07	0.05	0.16	0.11	

Appropriate calculated time to peak: 0.05 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post UNC-4
 D.A. AREA (ha) 2.70

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post UNC-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Waterloo Sandy Loam	Wsl	C	100.0	2.70
				0.00
				0
				0
Total Area				2.70

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Wsl		0.10	98		98		98		98		98	0.10	10.19
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0.10		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Wsl		2.21	32	0.00		0.00		0.39	49	0.00		2.60	89.69
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		2.21		0.00		0.00		0.39		0.00			

Composite Area Calculations								Total Pervious Area		2.60	
								Total Impervious Area		0.10	
								% Impervious		3.85%	
								Composite Curve Number		37.0	
								Total Area Check		2.70	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Waterloo Sandy							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.21	22.07	0.18	2.21		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.39	1.95	0.20	0.39		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.10	0.21	0.95	0.10		0		0		0
Composite		2.70	8.97	Composite Runoff Coefficient							0.21

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			TP (hr)				
Overland	324	25	7.72%	0.6	0.17	0.54	0.36	0.36	0.19	0.12	0.44	0.30

Appropriate calculated time to peak: 0.30 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post EXT-1
 D.A. AREA (ha) 3.50

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post EXT-1

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	3.50
				0
				0
				0
Total Area				3.50

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		3.50	73	0.00		0.00		0.00		0.00		3.50	255.50
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		3.50		0.00		0.00		0.00		0.00			
					Composite Area Calculations			Total Pervious Area			3.50		
								Total Impervious Area			0		
								% Impervious			0.00%		
								Composite Curve Number			73.0		
								Total Area Check			3.50		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	3.50	35.00	0.52	3.50		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		3.50	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	460	160	34.78%	0.6	0.35	0.36	0.24	0.24	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: 0.13 Appropriate Method: Bransby Williams



Project Name: Alfa Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post EXT-2
 D.A. AREA (ha) 4.10

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post EXT-2

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	4.10
				0
				0
				0
Total Area				4.10

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	4.10	73	0.00		0.00		0.00		0.00		4.10	299.30
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	4.10		0.00		0.00		0.00		0.00			

					Composite Area Calculations					Total Pervious Area		
										Total Impervious Area		
										% Impervious		
										Composite Curve Number		
										Total Area Check		
										4.10		
										0		
										0.00%		
										73.0		
										4.10		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	4.10	41.00	0.52	4.10		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		4.10	10.00	Composite Runoff Coefficient							
				0.52							

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.18	0.12	0.21	0.14

Appropriate calculated time to peak: 0.12 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post EXT-3
 D.A. AREA (ha) 2.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post EXT-3

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	2.20
				0
				0
				0
Total Area				2.20

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc			98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		2.20	73	0.00		0.00		0.00		0.00		2.20	160.60
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		2.20		0.00		0.00		0.00		0.00			

					Composite Area Calculations		Total Pervious Area		2.20	
							Total Impervious Area		0	
							% Impervious		0.00%	
							Composite Curve Number		73.0	
							Total Area Check		2.20	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				0		0		0			
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.20	22.00	0.52	2.20		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		2.20	10.00	Composite Runoff Coefficient							

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: 0.13 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post EXT-4
 D.A. AREA (ha) 2.60

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post EXT-4

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	2.60
				0
				0
				0
Total Area				2.60

Impervious Landuses Present:													
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals		
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc		98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
	0	98		98		98		98		98	0	0	
Subtotal	0		0		0		0		0				

Pervious Landuses Present:													
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals		
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc	2.60	73	0.00		0.00		0.00		0.00		2.60	189.80	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00	
Subtotal	2.60		0.00		0.00		0.00		0.00				
				Composite Area Calculations			Total Pervious Area			2.60			
							Total Impervious Area			0			
							% Impervious			0.00%			
							Composite Curve Number			73.0			
							Total Area Check			2.60			

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.60	26.00	0.52	2.60		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		2.60	10.00	Composite Runoff Coefficient							
											0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	445	155	34.83%	0.6	0.35	0.35	0.23	0.23	0.19	0.13	0.21	0.14

Appropriate calculated time to peak: 0.13 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-23
 By: Z. Holland

D.A. NAME Post EXT-5
 D.A. AREA (ha) 5.20

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment Post EXT-5

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	5.20
				0
				0
				0
Total Area				5.20

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	5.20	73	0.00		0.00		0.00		0.00		5.20	379.60
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	5.20		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			5.20		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			5.20		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	5.20	52.00	0.52	5.20		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		5.20	10.00	Composite Runoff Coefficient							0.52

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	415	140	33.73%	0.6	0.35	0.33	0.22	0.22	0.17	0.11	0.20	0.13

Appropriate calculated time to peak: 0.11 Appropriate Method: Bransby Williams



Project Name: Flato UMW - Phase 2 (WS)
 Project No.: 1060-5609
 Date: 2021-06-22
 By: Z. Holland

D.A. NAME
 D.A. AREA (ha)

SWMF
 0.90

Hydrologic Parameters: CALIB STANDHYD Command
Post Development Drainage Area: Catchment SWMF

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Kemble Silty Clay	Ksc	C	100	0.90
				0
				0
				0
Total Area Check				0.90

Impervious Landuses Present:												Subtotals	
Soils	Roadway		Sidewalk		Driveway		Building		SWMF			Area	A*CN
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN			
Ksc		98		98		98		98	0.45	98		0.45	44.10
0		98		98		98		98		98		0	0
0		98		98		98		98		98		0	0
0		98		98		98		98		98		0	0
Subtotal Area	0		0		0		0		0.45				
Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated			Area	A*CN
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN			
Ksc	0		0		0		0.45	79	0			0.45	35.55
0	0		0		0		0		0			0	0
0	0		0		0		0		0			0	0
0	0		0		0		0		0			0	0
Subtotal Area	0		0		0		0.45		0				
												Pervious Area Calculations	
												Total Pervious Area	
												Composite Pervious Curve Number	
												Total Directly Connected Area	
												Total Indirectly Connected Area	
												Total Impervious Area	
												% X imp	
												% T imp	
												Total Area Check	

Initial Abstraction and Tp Calculations

Landuse	IA (mm)	Area (ha)	A * IA
Woodland	10	0	0
Meadow	8	0	0
Wetland	16	0	0
Lawn	5	0.45	2.25
Cultivated	7	0	0

Land Use	IA (mm)	Slope (%)	Travel Length (m)	Manning's n
Pervious	5.0	2	20	0.25
Impervious	2.0	2	77	0.013



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-13
 By: E. Horner

D.A. NAME
 D.A. AREA (ha) **EXT-6**
6.00

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-6

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	6.00
				0
				0
				0
Total Area				6.00

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc			98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0		0		0		0		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		6.00	73	0.00		0.00		0.00		0.00		6.00	438.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		6.00		0.00		0.00		0.00		0.00			

					Composite Area Calculations		Total Pervious Area		6.00	
							Total Impervious Area		0	
							% Impervious		0.00%	
							Composite Curve Number		73.0	
							Total Area Check		6.00	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay							
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	6.00	60.00	0.30	6.00		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00		0		0		0		0
Composite		6.00	10.00	Composite Runoff Coefficient							0.30

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	550	30	5.45%	0.6	0.14	1.09	0.73	0.73	0.31	0.21	0.58	0.39

Appropriate calculated time to peak: **0.39** Appropriate Method: **Airport**



Project Name: Alfa Phase II
 Project No.: 119-2528
 Date: 2021-06-13
 By: E. Horner

D.A. NAME EXT-7
 D.A. AREA (ha) 6.00

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-7

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	6.00
				0
				0
				0
Total Area				6.00

Impervious Landuses Present:													
Roadway			Sidewalk			Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
Subtotal	0		0		0		0		0				
Pervious Landuses Present:													
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals		
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Dc	6.00	73	0.00		0.00		0.00		0.00		6.00	438.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
Subtotal	6.00		0.00		0.00		0.00		0.00				
					Composite Area Calculations			Total Pervious Area			6.00		
								Total Impervious Area			0		
								% Impervious			0.00%		
								Composite Curve Number			73.0		
								Total Area Check			6.00		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0		
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	6.00	60.00	0.35	6.00		0		0		0	2.10
Meadow	8	0.00	0.00		0		0		0		0	0.00
Wetland	16	0.00	0.00		0		0		0		0	0.00
Lawn	5	0.00	0.00		0		0		0		0	0.00
Cultivated	7	0.00	0.00		0		0		0		0	0.00
Impervious	2	0.00	0.00		0		0		0		0	0.00
Composite		6.00	10.00	Composite Runoff Coefficient								0.35

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			TP (hr)				
Overland	450	135	30.00%	0.6	0.33	0.38	0.25	0.25	0.18	0.12	0.28	0.19

Appropriate calculated time to peak: 0.19 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2022-02-11
 By: J. Kerschbaumer

D.A. NAME EXT-8
 D.A. AREA (ha) 13.10

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-8

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay	Ksc	C	100.0	13.10
				0
				0
				0
Total Area				13.10

Impervious Landuses Present:													
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals		
Soils	Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Ksc	0.21	98		98	0.12	98	0.24	98		98	0.5725	56.105	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
0		98		98		98		98		98	0	0	
Subtotal	0.21		0		0.12		0.24		0				

Pervious Landuses Present:													
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals		
Soils	Area	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	CN	Area	A*CN	
Ksc	10.17	73	0.00		0.00		2.36	79	0.00		12.53	928.64	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00	
Subtotal	10.17		0.00		0.00		2.36		0.00				

				Composite Area Calculations		Total Pervious Area		12.53	
						Total Impervious Area		0.5725	
						% Impervious		4.37%	
						Composite Curve Number		75.2	
						Total Area Check		13.10	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty Clay		0		0		0		
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	10.17	101.72	0.30	10.17		0		0		0	3.05
Meadow	8	0.00	0.00		0		0		0		0	0.00
Wetland	16	0.00	0.00		0		0		0		0	0.00
Lawn	5	2.36	11.78	0.20	2		0		0		0	0.47
Cultivated	7	0.00	0.00		0		0		0		0	0.00
Impervious	2	0.57	1.15	0.95	1		0		0		0	0.54
Composite		13.10	8.75	Composite Runoff Coefficient								0.31

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	800	70	8.75%	0.6	0.18	1.25	0.84	0.84	0.38	0.26	0.59	0.40

Appropriate calculated time to peak: 0.40 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-16
 By: E. Horner

D.A. NAME EXT-9
 D.A. AREA (ha) 7.00

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-9

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Granby Sand	Gs	C	100.0	7.00
				0
				0
				0
Total Area				7.00

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Gs	0.44	98		98	0.08	98	0.16	98		98	0.682	66.836
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0.44		0		0.08		0.16		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Gs	4.69	73	0.00		0.00		1.62	79	0.00		6.32	470.96
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	4.69		0.00		0.00		1.62		0.00			

				Composite Area Calculations		Total Pervious Area		6.32	
						Total Impervious Area		0.682	
						% Impervious		9.74%	
						Composite Curve Number		76.8	
						Total Area Check		7.00	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Granby Sand		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	4.69	46.94	0.25	4.69		0		0		0	1.17
Meadow	8	0.00	0.00		0		0		0		0	0.00
Wetland	16	0.00	0.00		0		0		0		0	0.00
Lawn	5	1.62	8.12	0.15	2		0		0		0	0.24
Cultivated	7	0.00	0.00		0		0		0		0	0.00
Impervious	2	0.68	1.36	0.95	1		0		0		0	0.65
Composite		7.00	8.06	Composite Runoff Coefficient								0.30



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-22
 By: E. Horner

D.A. NAME EXT-10A
 D.A. AREA (ha) 27.90

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-10A

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Brighton Sand	Brs	A	66.7	18.61
Granby Sand	Gs	C	33.3	9
				0
				0
Total Area				27.90

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Brs	0.41	98		98	0.37	98	0.75	98		98	1.53	150.24
Gs	0.21	98		98	0.19	98	0.37	98		98	0.77	75.29
0		98		98		98		98		98	0	0
0		98		98		98		98		98	0	0
Subtotal	0.62		0		0.56		1.12		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Brs	8.49	32	0.00		3.69	50	4.90	49	0.00		17.08	696.14
Gs	5.41	73	0.00		0.00	50	3.12	79	0.00		8.52	640.83
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	13.89		0.00		3.69		8.01		0.00			
				Composite Area Calculations			Total Pervious Area			25.60		
							Total Impervious Area			2.3014		
							% Impervious			8.25%		
							Composite Curve Number			56.0		
							Total Area Check			27.90		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Brighton Sand		Granby Sand		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	13.89	138.95	0.18	8.49	0.35	5		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	3.69	59.04	0.05	4		0		0		0
Lawn	5	8.01	40.07	0.15	5	0.15	3		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	2.30	4.60	0.95	2	0.95	1		0		0
Composite		27.90	8.70	Composite Runoff Coefficient							0.25

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	415	140	33.73%	0.6	0.35	0.33	0.22	0.22	0.14	0.09	0.29	0.20

Appropriate calculated time to peak: 0.20 Appropriate Method: Airport



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-13
 By: E. Horner

D.A. NAME EXT-10B
 D.A. AREA (ha) 4.90

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-10B

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Brighton Sand	Brs	A	100.0	4.90
				0
				0
				0
Total Area				4.90

Impervious Landuses Present:													
		Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils		Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Brs		0.7	98		98	0.1	98	0.4	98		98	1.2	117.6
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
	0		98		98		98		98		98	0	0
Subtotal		0.7		0		0.1		0.4		0			

Pervious Landuses Present:													
		Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils		Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Brs		1.85	32	0.00		0.00		1.85	49	0.00		3.70	149.85
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00		0.00		0.00		0.00		0.00		0.00	0.00
Subtotal		1.85		0.00		0.00		1.85		0.00			

		Composite Area Calculations		Total Pervious Area		3.70	
				Total Impervious Area		1.2	
				% Impervious		24.49%	
				Composite Curve Number		54.6	
				Total Area Check		4.90	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Brighton Sand		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	1.85	18.50	0.12	1.85		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	1.85	9.25	0.15	2		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	1.20	2.40	0.95	1		0		0		0
Composite		4.90	6.15	Composite Runoff Coefficient							0.33

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	75	5	6.67%	0.6	0.15	0.13	0.09	0.09	0.04	0.03	0.25	0.17

Appropriate calculated time to peak: 0.17 Appropriate Method: Airport

Time of concentration set to 15 min per Town standards



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-16
 By: E. Horner

D.A. NAME EXT-11
 D.A. AREA (ha) 3.90

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-11

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Kemble Silty Clay/Dunedin Clay	Ksc/Dc	C	90.0	3.51
Waterloo Sandy Loam	Wsl	A	10.0	0
				0
				0
Total Area				3.90

Impervious Landuses Present:											
Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area A*CN
Ksc/Dc	0.12	98		98	0.06	98	0.12	98		98	0.299 29.302
Wsl		98		98		98		98		98	0 0
0		98		98		98		98		98	0 0
0		98		98		98		98		98	0 0
Subtotal	0.12		0		0.06		0.12		0		
Pervious Landuses Present:											
Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area A*CN
Ksc/Dc	2.22	73	0.00		0.00		1.00	79	0.00		3.21 240.38
Wsl	0.27	32	0.00		0.00		0.12	49	0.00		0.39 14.47
0	0.00		0.00		0.00		0.00		0.00		0.00 0.00
0	0.00		0.00		0.00		0.00		0.00		0.00 0.00
Subtotal	2.49		0.00		0.00		1.11		0.00		
Composite Area Calculations										Total Pervious Area	
										Total Impervious Area	
										% Impervious	
										Composite Curve Number	
										Total Area Check	
										3.60	
										0.299	
										7.67%	
										72.9	
										3.90	

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Kemble Silty		Waterloo Sandy Loam		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	2.49	24.89	0.52	2.22	0.35	0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	1.11	5.56	0.20	1	0.20	0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.30	0.60	0.95	0	0.95	0		0		0
Composite		3.90	7.96	Composite Runoff Coefficient							
											0.45

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path	Length	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity	Tc (hr)	Tp (hr)	TOTAL	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Description	(m)				(m/s)			Tp (hr)				
Overland	230	30	13.04%	0.6	0.22	0.29	0.20	0.20	0.11	0.08	0.23	0.15

Appropriate calculated time to peak: 0.08 Appropriate Method: Bransby Williams



Project Name: Alta Phase II
 Project No.: 119-2528
 Date: 2021-06-08
 By: E. Horner

D.A. NAME EXT-12
 D.A. AREA (ha) 5.20

Hydrologic Parameters: CALIB NASHYD Command
Post Development Drainage Area: Catchment EXT-12

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic Group	% Area	Area (ha)
Dunedin Clay	Dc	C	100.0	5.20
				0
				0
				0
Total Area				5.20

Impervious Landuses Present:												
Roadway			Sidewalk		Driveway		Building		SWMF		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc		98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
	0	98		98		98		98		98	0	0
Subtotal	0		0		0		0		0			

Pervious Landuses Present:												
Woodland			Meadow		Wetland		Lawn		Cultivated		Subtotals	
Soils	Area (ha)	CN	Area (ha)	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
Dc	5.20	73	0.00		0.00		0.00		0.00		5.20	379.60
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
	0	0.00	0.00		0.00		0.00		0.00		0.00	0.00
Subtotal	5.20		0.00		0.00		0.00		0.00			
				Composite Area Calculations			Total Pervious Area			5.20		
							Total Impervious Area			0		
							% Impervious			0.00%		
							Composite Curve Number			73.0		
							Total Area Check			5.20		

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient							
Landuse	IA (mm)	Area (ha)	A * IA	Dunedin Clay		0		0		0	
				RC	Area	RC	Area	RC	Area	RC	Area
Woodland	10	5.20	52.00	0.35	5.20		0		0		0
Meadow	8	0.00	0.00		0		0		0		0
Wetland	16	0.00	0.00		0		0		0		0
Lawn	5	0.00	0.00		0		0		0		0
Cultivated	7	0.00	0.00		0		0		0		0
Impervious	2	0.00	0.00	0.95	0		0		0		0
Composite		5.20	10.00	Composite Runoff Coefficient							0.35

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp (hr)	TOTAL Tp (hr)	Tc (hr)	Tp (hr)	Tc (hr)	Tp (hr)
Overland	470	165	35.11%	0.6	0.36	0.37	0.25	0.25	0.19	0.12	0.27	0.18

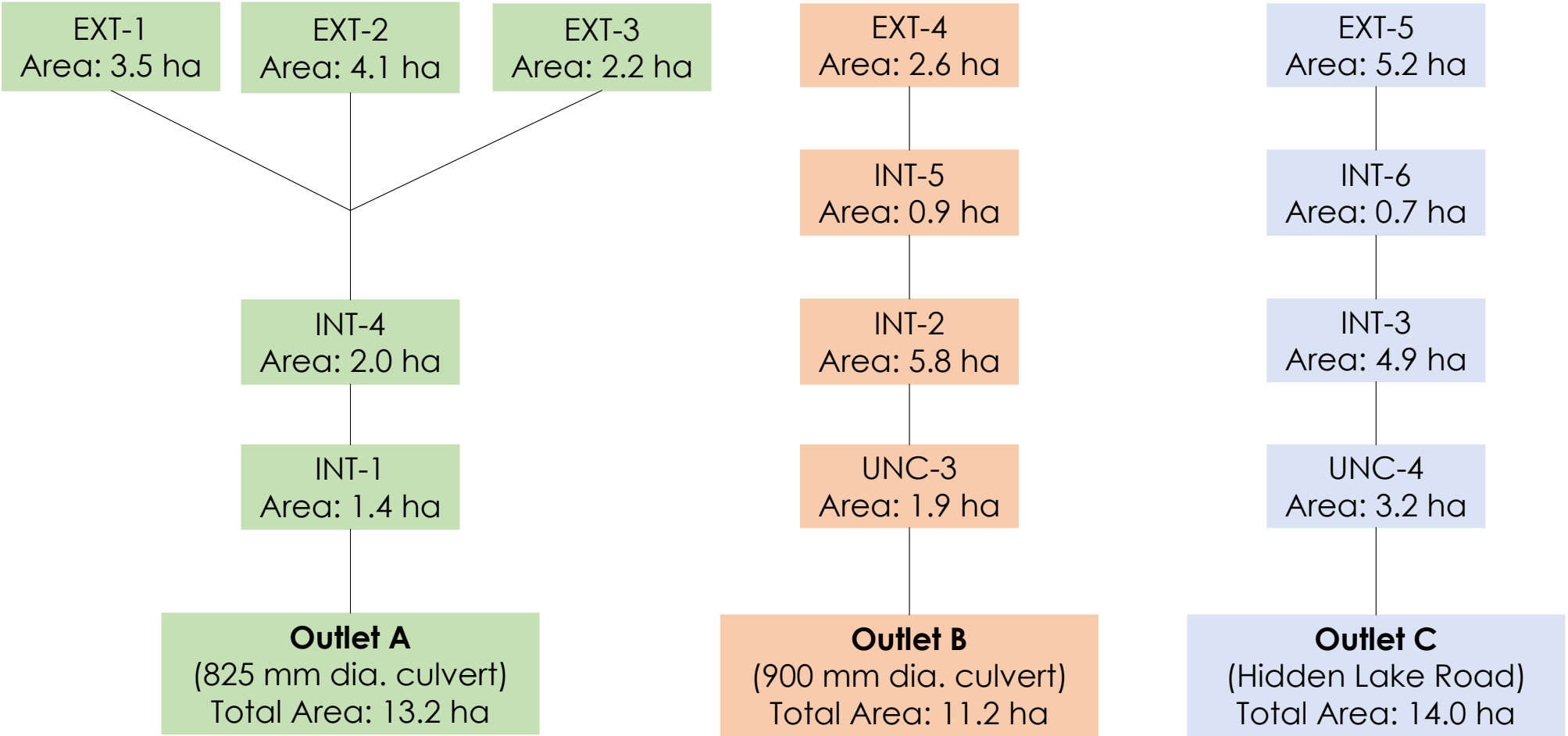
Appropriate calculated time to peak: 0.18 Appropriate Method: Airport

APPENDIX D

SWMHYMO Input and Output Files

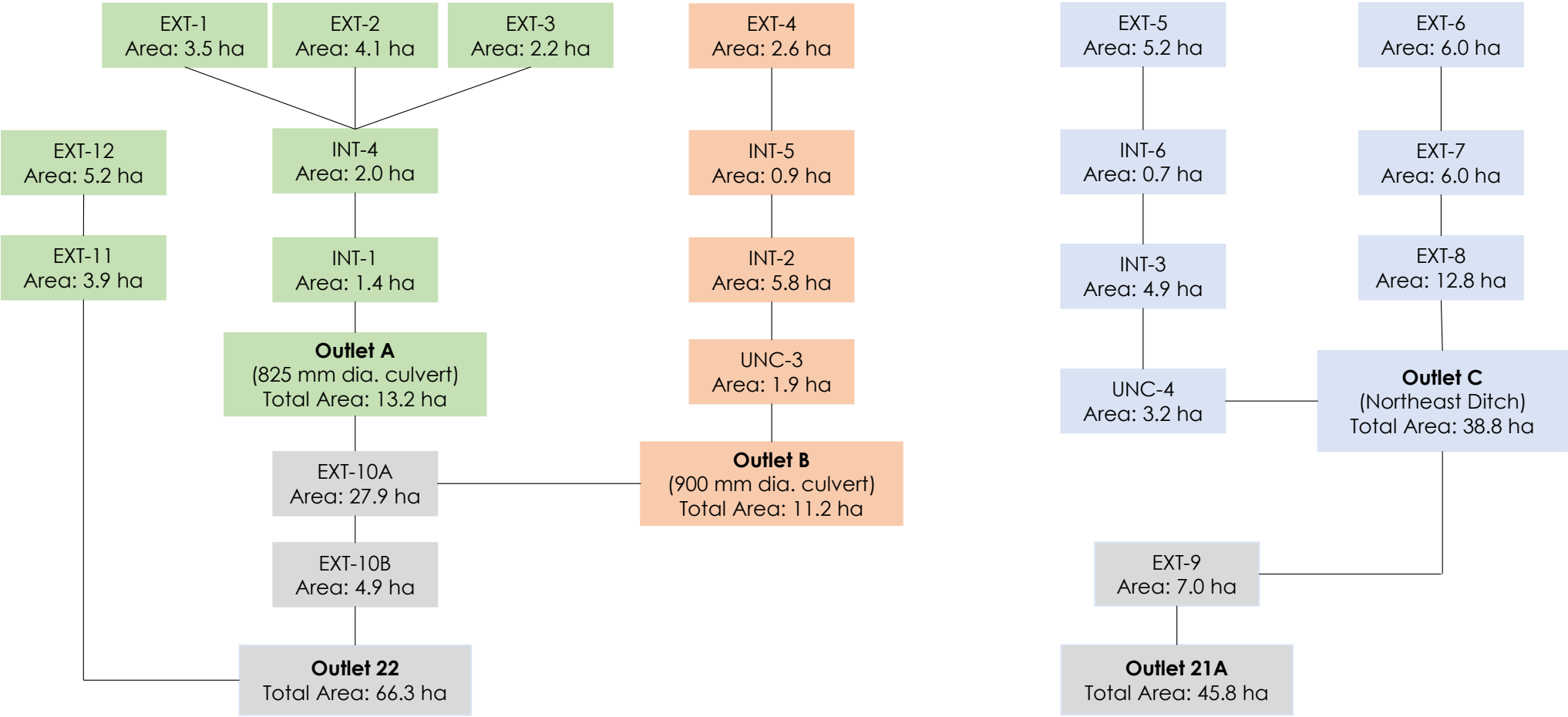
Alta Phase II Pre-Development SWMHYMO Model

Project Name: Alta Phase II
Project Number: 119-2528
Date: 2022/02/11



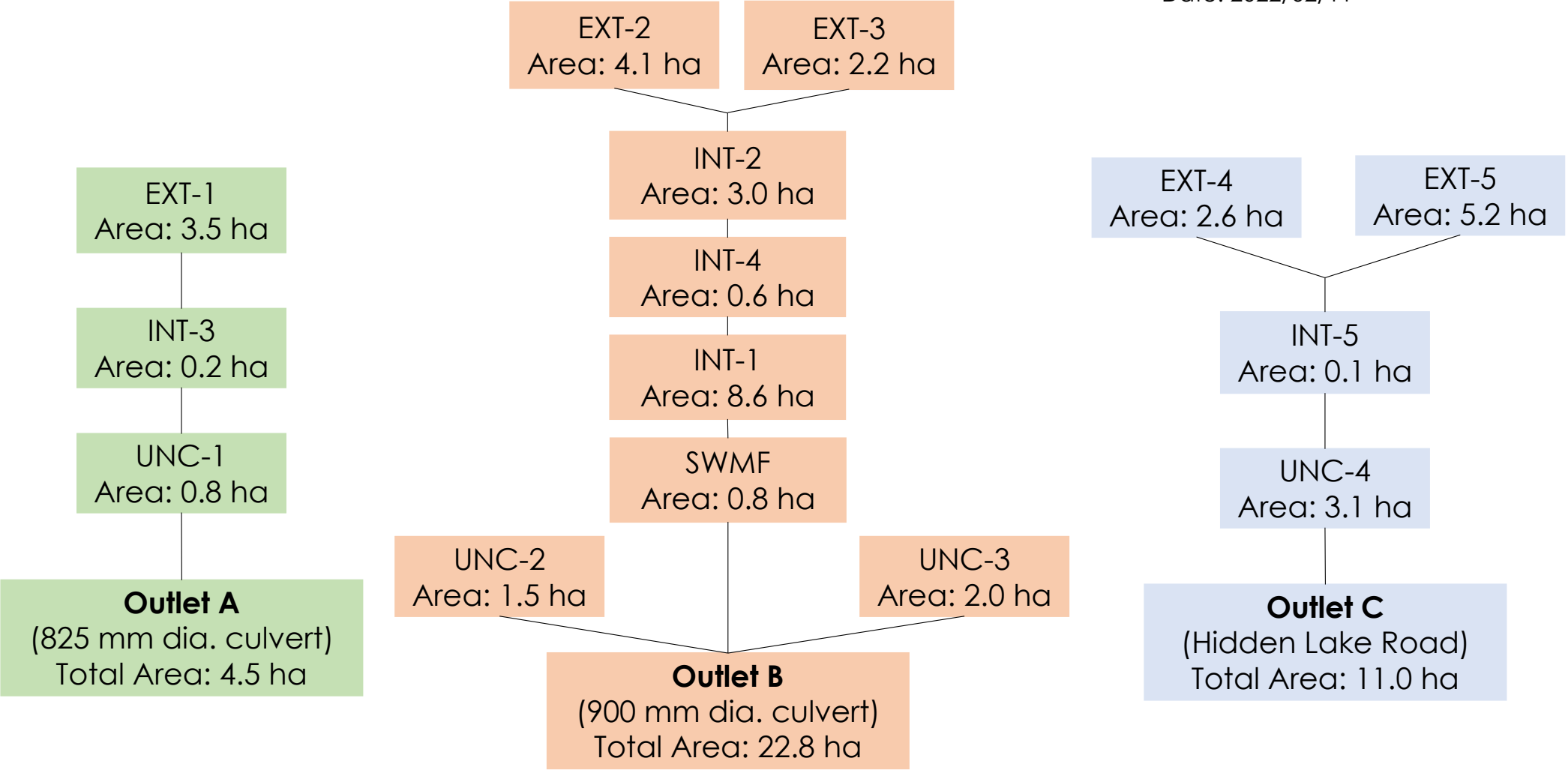
Alta Phase II Pre-Development SWMHYMO Model (Including External Drainage Corridor)

Project Name: Alta Phase II
Project Number: 119-2528
Date: 2022/02/11



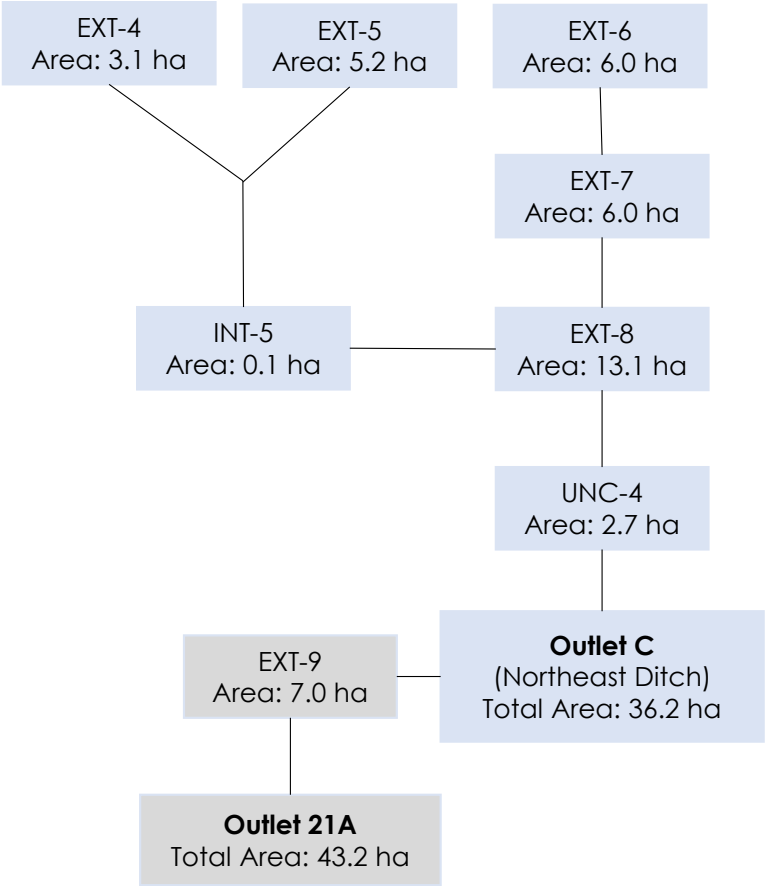
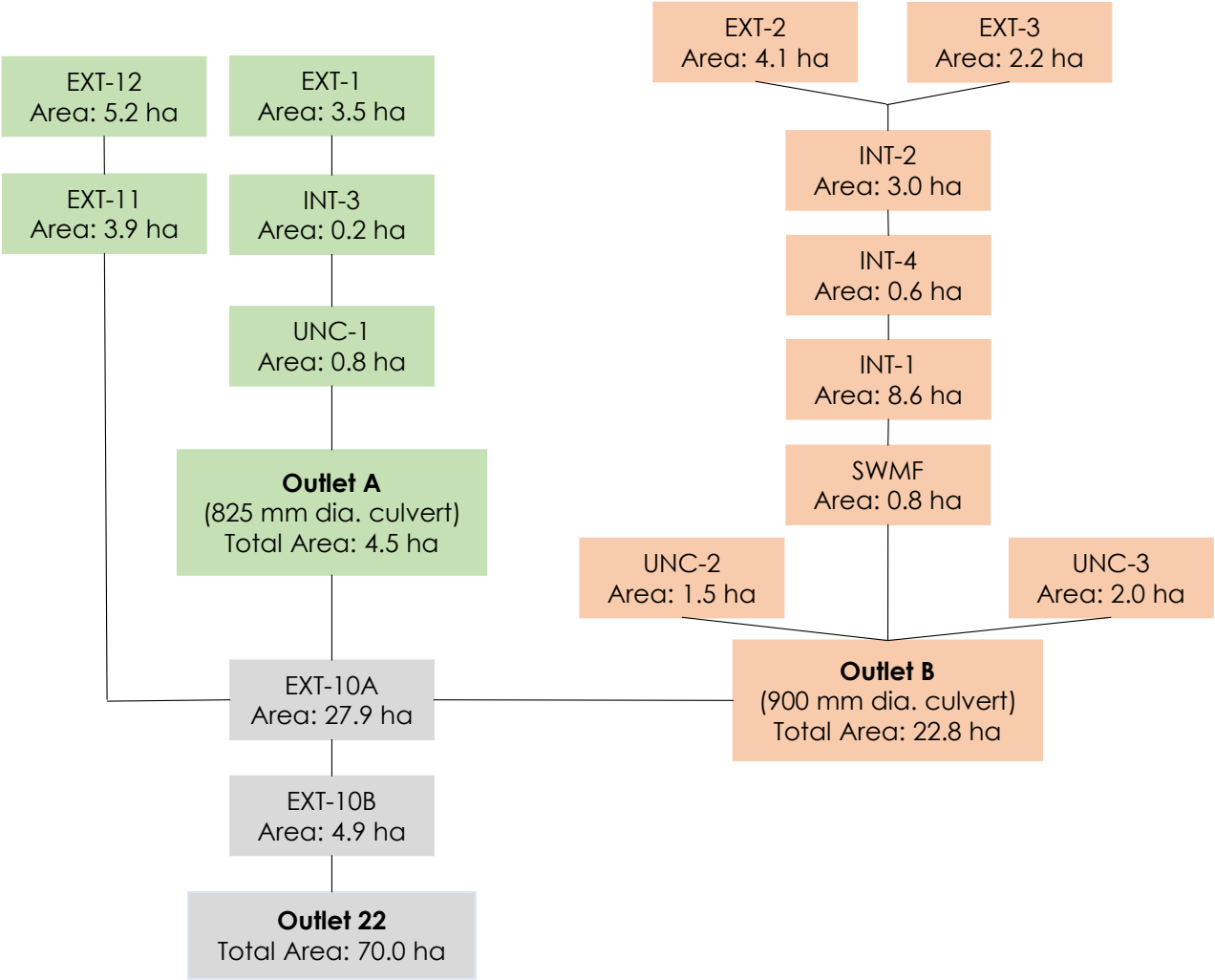
Alta Phase II Post-Development SWMHYMO Model

Project Name: Alta Phase II
Project Number: 119-2528
Date: 2022/02/11



Alta Phase II Post-Development SWMHYMO Model (Including External Drainage Corridor)

Project Name: Alta Phase II
Project Number: 119-2528
Date: 2022/02/11



PRE_25mm

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SSSSS W W M M H H Y Y M M 000 222 000 11
77777 =====
S W W W MM MM H H Y Y MM MM O O 2 0 0 11
7 7
SSSSS W W M M M HHHH Y M M M O O 2 0 0 11
7 Ver4.05.0
S W W M M H H Y M M M O O 222 0 0 11
7 APR 2017
SSSSS W W M M H H Y M M 000 2 0 0 11
7 =====
2 0 0 11
7 # 3737016
StormWater Management HYdrologic Model 222 000 11
7 =====

***** SWMHYMO Ver4.05.0

***** A single event and continuous hydrologic simulation model

***** based on the principles of HYMO and its successors

***** OTTHYMO-83 and OTTHYMO-89.

***** Distributed by: J.F. Sabourin and Associates Inc.

***** Ottawa, Ontario: (613) 836-3884

***** Gatineau, Quebec: (819) 243-6858

***** E-Mail: swmhymo@jfsa.com

+++++

Alta Phase 2 (119-2528)

1

PRE_25mm

+++++ Licensed user: C.F. Crozier & Associates Inc.

+++++

Collingwood

SERIAL#:3737016

+++++

+++++

***** +++++ PROGRAM ARRAY DIMENSIONS +++++

***** Maximum value for ID numbers : 11

***** Max. number of rainfall points: 105408

***** Max. number of flow points : 105408

***** S U M M A R Y O U T P U T

***** RUN DATE: 2021-06-30 TIME: 12:08:14 RUN COUNTER: 000002

***** Input file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\25mm\PRE_25mm.Dat *
***** Output file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\25mm\PRE_25mm.out *
***** Summary file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\25mm\PRE_25mm.sum *
***** User comments:

*
1: _____
*
*
2: _____
*

Alta Phase 2 (119-2528)

2

```
PRE_25mm
*
3:_____
      *

*****
*****

#*****

# Project Name: [ALTA PHASE II]   Project Number: [119-2528]

# Date      : 2021.06.30

# Modified   : 2021.06.30

# Modeller   : [Z. Holland]

# Company    : C.F. Crozier & Associates Inc.

# License #   : 3737016

#*****

RUN#:COMMAND#
R0001:C00001-----
-----
START
[TZERO = .00 hrs on      0]
[METOUT= 2   (1=imperial, 2=metric output)]
[NSTORM= 0 ]
[NRUN  = 0001 ]

Alta Phase 2 (119-2528)
```

```
PRE_25mm
#-----|-----25mm-----|

#-----|-----|

R0001:C00002-----
-----
READ STORM
Filename = 25mm.stm

Comment = 25 mm Event

[SDT= 4.80:SDUR= 3.04:PTOT= 25.05]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00003-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD      1.2 05:EXT-1      3.50      .020 No_date      1:14
2.08 .083      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00004-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD      1.2 02:EXT-2      4.10      .024 No_date      1:13
2.08 .083      .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00005-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)
```



```

PRE_25mm
  CALIB NASHYD      1.2 03:EXT-3      2.20      .012 No_date      1:14
2.08 .083      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 04:INT-4      2.00      .015 No_date      1:04
2.08 .083      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 06:INT-1      1.40      .010 No_date      1:25
3.09 .123      .000
  [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----

#-----|-----

R0001:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  ADD HYD      1.2 05:EXT-1      3.50      .020 No_date      1:14
2.08 n/a      .000
  +      1.2 02:EXT-2      4.10      .024 No_date      1:13
2.08 n/a      .000
  +      1.2 03:EXT-3      2.20      .012 No_date      1:14
2.08 n/a      .000
  +      1.2 04:INT-4      2.00      .015 No_date      1:04
2.08 n/a      .000
  +      1.2 06:INT-1      1.40      .010 No_date      1:25
3.09 n/a      .000
  SUM=      1.2 01:825mm      13.20      .075 No_date      1:13
2.19 n/a      .000
#-----|-----

#-----|-----OUTLET B-----|

Alta Phase 2 (119-2528)

```

```

PRE_25mm

R0001:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 04:EXT-4      2.60      .015 No_date      1:14
2.08 .083      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 05:INT-5      .90      .007 No_date      1:04
2.08 .083      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 06:INT-2      5.80      .029 No_date      1:31
2.51 .100      .000
  [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 07:UNC-3      1.90      .013 No_date      1:06
1.92 .077      .000
  [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----

#-----|-----

R0001:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
  ADD HYD      1.2 04:EXT-4      2.60      .015 No_date      1:14
2.08 n/a      .000
  +      1.2 05:INT-5      .90      .007 No_date      1:04
2.08 n/a      .000
  +      1.2 06:INT-2      5.80      .029 No_date      1:31
2.51 n/a      .000
  +      1.2 07:UNC-3      1.90      .013 No_date      1:06

Alta Phase 2 (119-2528)

```

PRE_25mm
1.92 n/a .000
SUM= 1.2 02:900mm 11.20 .050 No_date 1:21
2.27 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 05:EXT-5 5.20 .031 No_date 1:12
2.08 .083 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 06:INT-6 .70 .005 No_date 1:04
2.08 .083 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 07:INT-3 4.90 .023 No_date 1:38
2.60 .104 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 08:UNC-4 3.20 .003 No_date 1:34
.47 .019 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.2 05:EXT-5 5.20 .031 No_date 1:12
2.08 n/a .000
+ 1.2 06:INT-6 .70 .005 No_date 1:04

Alta Phase 2 (119-2528)

7

PRE_25mm
2.08 n/a .000
+ 1.2 07:INT-3 4.90 .023 No_date 1:38
2.60 n/a .000
+ 1.2 08:UNC-4 3.20 .003 No_date 1:34
.47 n/a .000
SUM= 1.2 03:OUTLET C 14.00 .048 No_date 1:18
1.89 n/a .000
R0001:C00019-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 04:Ext-6 6.00 .021 No_date 1:42
2.08 .083 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00020-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 09:Ext-7 6.00 .029 No_date 1:20
2.08 .083 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00021-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.2 10:Ext-8 12.80 .060 No_date 1:39
2.66 .106 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

8

PRE_25mm

```
R0001:C00022-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.2 03:OUTLET C      14.00      .048 No_date    1:18
1.89 n/a          .000
  +          1.2 04:Ext-6              6.00      .021 No_date    1:42
2.08 n/a          .000
  +          1.2 09:Ext-7              6.00      .029 No_date    1:20
2.08 n/a          .000
  +          1.2 10:Ext-8             12.80      .060 No_date    1:39
2.66 n/a          .000
  SUM=          1.2 06:NE_DITCH       38.80      .150 No_date    1:32
2.20 n/a          .000
R0001:C00023-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 04:Ext-9        7.00      .043 No_date    1:32
3.08 .123          .000
  [CN= 76.8: N= 3.00: Tp= .34]
#-----|-----
```

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

```
R0001:C00024-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.2 06:NE_DITCH       38.80      .150 No_date    1:32
2.20 n/a          .000
  +          1.2 04:Ext-9              7.00      .043 No_date    1:32
3.08 n/a          .000
  SUM=          1.2 05:21A           45.80      .192 No_date    1:32
2.34 n/a          .000
R0001:C00025-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 04:Ext-10A     27.90      .083 No_date    1:20
1.24 .049          .000
  [CN= 56.0: N= 3.00: Tp= .20]
```

Alta Phase 2 (119-2528)

9

PRE_25mm

#-----|-----

```
R0001:C00026-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 03:Ext-11       3.90      .038 No_date    1:07
2.62 .105          .000
  [CN= 72.9: N= 3.00: Tp= .08]
#-----|-----
```

```
R0001:C00027-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 06:Ext-12       5.20      .026 No_date    1:20
2.08 .083          .000
  [CN= 73.0: N= 3.00: Tp= .18]
#-----|-----
```

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

```
R0001:C00028-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.2 01:825mm        13.20      .075 No_date    1:13
2.19 n/a          .000
  +          1.2 02:900mm           11.20      .050 No_date    1:21
2.27 n/a          .000
  +          1.2 04:Ext-10A         27.90      .083 No_date    1:20
1.24 n/a          .000
  +          1.2 03:Ext-11          3.90      .038 No_date    1:07
2.62 n/a          .000
  +          1.2 06:Ext-12          5.20      .026 No_date    1:20
2.08 n/a          .000
  SUM=          1.2 05:WET-STO       61.40      .255 No_date    1:16
1.79 n/a          .000
```

Alta Phase 2 (119-2528)

10

```

PRE_25mm
R0001:C00029-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ROUTE RESERVOIR ->   1.2 05:WET-ST0      61.40      .255 No_date   1:16
1.79 n/a      .000
      out <=   1.2 04:22      61.40      .144 No_date   1:51
1.79 n/a      .000
      overflow <=   1.2 06:OVF      .00      .000 No_date   0:00
.00 n/a      .000
      {MxStoUsed=.2487E-01 m3, TotOvfVol=.0000E+00 m3, N-Ovf=    0, TotDurOvf=
0.hrs}
R0001:C00030-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.2 03:Ext-10B      4.90      .022 No_date   1:14
1.55 .062      .000
      [CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00031-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD      1.2 03:Ext-10B      4.90      .022 No_date   1:14
1.55 n/a      .000
      +      1.2 04:22      61.40      .144 No_date   1:51
1.79 n/a      .000
      +      1.2 06:OVF      .00      .000 No_date   0:00
.00 n/a      .000
      SUM=      1.2 05:22      66.30      .156 No_date   1:26
1.77 n/a      .000
R0001:C00032-----
-----
FINISH
-----
*****
*****

```

Alta Phase 2 (119-2528)

```

PRE_25mm
WARNINGS / ERRORS / NOTES
-----
Simulation ended on 2021-06-30 at 12:08:14
=====
=====

```

PRE_KCHU

=====

SSSSS W W M M H H Y Y M M 000 222 000 11
77777 =====
S W W W MM MM H H Y Y MM MM O O 2 0 0 11
7 7
SSSSS W W M M M HHHH Y M M M O O 2 0 0 11
7 Ver4.05.0
S W W M M H H Y M M O O 222 0 0 11
7 APR 2017
SSSSS W W M M H H Y M M 000 2 0 0 11
7 =====
2 0 0 11
7 # 3737016
StormWater Management HYdrologic Model 222 000 11
7 =====

***** SWMHYMO Ver4.05.0

***** A single event and continuous hydrologic simulation model

***** based on the principles of HYMO and its successors

***** OTTHYMO-83 and OTTHYMO-89.

***** Distributed by: J.F. Sabourin and Associates Inc.

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+++++

Alta Phase 2 (119-2528)

1

PRE_KCHU

+++++ Licensed user: C.F. Crozier & Associates Inc.

+++++

+++++

+++++

Collingwood

SERIAL#:3737016

+++++

***** +++++ PROGRAM ARRAY DIMENSIONS +++++

***** Maximum value for ID numbers : 11

***** Max. number of rainfall points: 105408

***** Max. number of flow points : 105408

***** S U M M A R Y O U T P U T

***** RUN DATE: 2021-06-30 TIME: 12:16:42 RUN COUNTER: 000003

***** Input file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_KCHU\PRE_KCHU.Da*
***** t

***** Output file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_KCHU\PRE_KCHU.ou*
***** t

***** Summary file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_KCHU\PRE_KCHU.su*
***** m

***** User comments:

Alta Phase 2 (119-2528)

2

```
PRE_KCHU
*
1: _____
  *
2: _____
  *
3: _____
  *

*****
*****

#*****

# Project Name: [ALTA PHASE II]   Project Number: [119-2528]

# Date      : 2021.06.30

# Modified   : 2021.06.30

# Modeller   : [Z. Holland]

# Company    : C.F. Crozier & Associates Inc.

# License #   : 3737016

#*****

RUN#:COMMAND#
R0001:C00001-----
Alta Phase 2 (119-2528)
```

```
PRE_KCHU
-----
START
[TZERO =   .00 hrs on      0]
[METOUT=   2   (1=imperial, 2=metric output)]
[NSTORM=   0 ]
[NRUN  = 0001 ]
#-----|-----|

#-----|-----2 YEAR KCHU-----|

#-----|-----|

R0001:C00002-----
-----
READ STORM
Filename = 2yr.stm

Comment = 2-Year 6 hr Kefer Chu Chicago Storm Event

[SDT=60.00:SDUR=   6.00:PTOT=  37.90]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00003-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)
```

PRE_KCHU
CALIB NASHYD 1.0 05:EXT-1 3.50 .068 No_date 3:01
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .081 No_date 3:01
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .043 No_date 3:01
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:INT-4 2.00 .044 No_date 3:00
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-1 1.40 .028 No_date 3:06
8.37 .221 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-1 3.50 .068 No_date 3:01
6.39 n/a .000
+ 1.0 02:EXT-2 4.10 .081 No_date 3:01
6.39 n/a .000
+ 1.0 03:EXT-3 2.20 .043 No_date 3:01
6.39 n/a .000
+ 1.0 04:INT-4 2.00 .044 No_date 3:00
Alta Phase 2 (119-2528)

PRE_KCHU
6.39 n/a .000 + 1.0 06:INT-1 1.40 .028 No_date 3:06
8.37 n/a .000
SUM= 1.0 01:825mm 13.20 .261 No_date 3:01
6.60 n/a .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:EXT-4 2.60 .051 No_date 3:01
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:INT-5 .90 .020 No_date 3:00
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-2 5.80 .094 No_date 3:08
7.24 .191 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:UNC-3 1.90 .037 No_date 3:00
5.81 .153 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

Alta Phase 2 (119-2528)

PRE_KCHU

```
R0001:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 04:EXT-4          2.60      .051 No_date    3:01
6.39 n/a      .000
  +          1.0 05:INT-5          .90      .020 No_date    3:00
6.39 n/a      .000
  +          1.0 06:INT-2          5.80      .094 No_date    3:08
7.24 n/a      .000
  +          1.0 07:UNC-3          1.90      .037 No_date    3:00
5.81 n/a      .000
  SUM=          1.0 02:900mm          11.20      .191 No_date    3:01
6.73 n/a      .000
#-----|-----
```

#-----|-----OUTLET C-----|

```
R0001:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 05:EXT-5          5.20      .105 No_date    3:01
6.39 .169      .000
  [CN= 73.0: N= 3.00: Tp= .11]
R0001:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-6          .70      .015 No_date    3:00
6.39 .169      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 07:INT-3          4.90      .071 No_date    3:12
7.39 .195      .000
  [CN= 74.8: N= 3.00: Tp= .39]
R0001:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 08:UNC-4          3.20      .011 No_date    3:09
1.55 .041      .000
  [CN= 34.4: N= 3.00: Tp= .32]
#-----|-----
```

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

Alta Phase 2 (119-2528)

7

PRE_KCHU

```
#-----|-----|
R0001:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 05:EXT-5          5.20      .105 No_date    3:01
6.39 n/a      .000
  +          1.0 06:INT-6          .70      .015 No_date    3:00
6.39 n/a      .000
  +          1.0 07:INT-3          4.90      .071 No_date    3:12
7.39 n/a      .000
  +          1.0 08:UNC-4          3.20      .011 No_date    3:09
1.55 n/a      .000
  SUM=          1.0 03:OUTLET C          14.00      .188 No_date    3:01
5.63 n/a      .000
R0001:C00019-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:Ext-6          6.00      .075 No_date    3:13
6.39 .169      .000
  [CN= 73.0: N= 3.00: Tp= .39]
#-----|-----|
```

```
R0001:C00020-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 09:Ext-7          6.00      .106 No_date    3:03
6.39 .169      .000
  [CN= 73.0: N= 3.00: Tp= .19]
#-----|-----|
```

```
R0001:C00021-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 10:Ext-8          12.80      .187 No_date    3:13
7.53 .199      .000
  [CN= 75.2: N= 3.00: Tp= .40]
#-----|-----|
```

#-----|-----|

Alta Phase 2 (119-2528)

8

PRE_KCHU
#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----|

#-----|-----|

R0001:C00022-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 .188 No_date 3:01
5.63 n/a .000 + 1.0 04:Ext-6 6.00 .075 No_date 3:13
6.39 n/a .000 + 1.0 09:Ext-7 6.00 .106 No_date 3:03
6.39 n/a .000 + 1.0 10:Ext-8 12.80 .187 No_date 3:13
7.53 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 .520 No_date 3:04
6.49 n/a .000
R0001:C00023-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .125 No_date 3:09
8.36 .220 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00024-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 .520 No_date 3:04
Alta Phase 2 (119-2528) 9

PRE_KCHU
6.49 n/a .000 + 1.0 04:Ext-9 7.00 .125 No_date 3:09
8.36 n/a .000 SUM= 1.0 05:21A 45.80 .639 No_date 3:05
6.78 n/a .000
R0001:C00025-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 .276 No_date 3:04
3.73 .098 .000
[CN= 56.0: N= 3.00: Tp= .20]
#-----|-----|

R0001:C00026-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .089 No_date 3:00
7.21 .190 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----|

R0001:C00027-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .093 No_date 3:03
6.39 .169 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00028-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 .261 No_date 3:01
6.60 n/a .000
Alta Phase 2 (119-2528) 10

```

PRE_KCHU
6.73 n/a .000 + 1.0 02:900mm 11.20 .191 No_date 3:01
3.73 n/a .000 + 1.0 04:Ext-10A 27.90 .276 No_date 3:04
7.21 n/a .000 + 1.0 03:Ext-11 3.90 .089 No_date 3:00
6.39 n/a .000 + 1.0 06:Ext-12 5.20 .093 No_date 3:03
SUM= 1.0 05:WET-STO 61.40 .900 No_date 3:01
5.34 n/a .000
R0001:C00029-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 .900 No_date 3:01
5.34 n/a .000
out <= 1.0 04:22 61.40 .203 No_date 3:46
5.34 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1458E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00030-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .055 No_date 3:02
4.15 .109 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

R0001:C00031-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .055 No_date 3:02
4.15 n/a .000
+ 1.0 04:22 61.40 .203 No_date 3:46
5.34 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00

Alta Phase 2 (119-2528)

```

11

```

PRE_KCHU
.00 n/a .000
SUM= 1.0 05:22 66.30 .239 No_date 3:05
5.25 n/a .000
#-----|-----

#-----|-----5 YEAR KCHU-----|

#-----|-----

R0001:C00032-----
-----
READ STORM
Filename = 5yr.stm

Comment = 5-Year 6 hr Kifer Chu Chicago Storm Event

[SDT=60.00:SDUR= 6.00:PTOT= 52.70]
#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

R0001:C00033-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .131 No_date 3:01
13.34 .253 .000
[CN= 73.0: N= 3.00: Tp= .13]

Alta Phase 2 (119-2528)

```

12

```

PRE_KCHU
R0001:C00034-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 02:EXT-2          4.10      .155 No_date    3:01
13.34 .253      .000
    [CN= 73.0: N= 3.00: Tp= .12]
R0001:C00035-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 03:EXT-3          2.20      .082 No_date    3:01
13.34 .253      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00036-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:INT-4          2.00      .082 No_date    3:00
13.34 .253      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00037-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-1          1.40      .053 No_date    3:05
16.44 .312      .000
    [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00038-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    ADD HYD              1.0 05:EXT-1          3.50      .131 No_date    3:01
13.34 n/a        .000
    +                    1.0 02:EXT-2          4.10      .155 No_date    3:01
13.34 n/a        .000
    +                    1.0 03:EXT-3          2.20      .082 No_date    3:01
13.34 n/a        .000
    +                    1.0 04:INT-4          2.00      .082 No_date    3:00
13.34 n/a        .000
    +                    1.0 06:INT-1          1.40      .053 No_date    3:05
16.44 n/a        .000
Alta Phase 2 (119-2528)

```

```

PRE_KCHU
SUM=      1.0 01:825mm      13.20      .497 No_date    3:00
13.67 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00039-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:EXT-4          2.60      .097 No_date    3:01
13.34 .253      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00040-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 05:INT-5          .90      .037 No_date    3:00
13.34 .253      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00041-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-2          5.80      .184 No_date    3:07
14.69 .279      .000
    [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00042-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 07:UNC-3          1.90      .070 No_date    3:00
12.14 .230      .000
    [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00043-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

```

PRE_KCHU
ADD HYD          1.0 04:EXT-4          2.60      .097 No_date    3:01
13.34 n/a      .000
13.34 n/a      .000 +          1.0 05:INT-5          .90      .037 No_date    3:00
13.34 n/a      .000 +          1.0 06:INT-2          5.80     .184 No_date    3:07
14.69 n/a      .000 +          1.0 07:UNC-3          1.90     .070 No_date    3:00
12.14 n/a      .000
13.84 n/a      .000 SUM=          1.0 02:900mm        11.20     .372 No_date    3:01
#-----|-----

```

```

#-----|-----OUTLET C-----|

```

```

R0001:C00044-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 05:EXT-5          5.20     .199 No_date    3:01
13.34 .253      .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00045-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-6          .70      .029 No_date    3:00
13.34 .253      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00046-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 07:INT-3          4.90     .141 No_date    3:11
14.89 .283      .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00047-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 08:UNC-4          3.20     .023 No_date    3:09
3.50 .066      .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

```

```

#-----|-----

```

Alta Phase 2 (119-2528)

15

PRE_KCHU

```

R0001:C00048-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD          1.0 05:EXT-5          5.20     .199 No_date    3:01
13.34 n/a      .000
13.34 n/a      .000 +          1.0 06:INT-6          .70      .029 No_date    3:00
13.34 n/a      .000 +          1.0 07:INT-3          4.90     .141 No_date    3:11
14.89 n/a      .000 +          1.0 08:UNC-4          3.20     .023 No_date    3:09
3.50 n/a      .000
SUM=          1.0 03:OUTLET C        14.00     .370 No_date    3:01
11.64 n/a      .000
R0001:C00049-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 04:Ext-6          6.00     .154 No_date    3:11
13.34 .253      .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

```

```

R0001:C00050-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 09:Ext-7          6.00     .207 No_date    3:03
13.34 .253      .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

```

```

R0001:C00051-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 10:Ext-8          12.80     .368 No_date    3:11
15.13 .287      .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

```

```

#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

```

Alta Phase 2 (119-2528)

16

PRE_KCHU

#-----|-----|

#-----|-----|

R0001:C00052-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.370	No_date	3:01
11.64 n/a .000						
+	1.0	04:Ext-6	6.00	.154	No_date	3:11
13.34 n/a .000						
+	1.0	09:Ext-7	6.00	.207	No_date	3:03
13.34 n/a .000						
+	1.0	10:Ext-8	12.80	.368	No_date	3:11
15.13 n/a .000						
SUM=	1.0	06:NE_DITCH	38.80	1.043	No_date	3:03
13.32 n/a .000						

R0001:C00053-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.238	No_date	3:08
16.42 .312 .000						
[CN= 76.8: N= 3.00: Tp= .34]						

#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00054-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.043	No_date	3:03
13.32 n/a .000						
+	1.0	04:Ext-9	7.00	.238	No_date	3:08
16.42 n/a .000						

Alta Phase 2 (119-2528)

17

PRE_KCHU

SUM= 1.0 05:21A 45.80 1.273 No_date 3:04

13.79 n/a .000
R0001:C00055-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.554	No_date	3:03
7.95 .151 .000						
[CN= 56.0: N= 3.00: Tp= .20]						

#-----|-----|

R0001:C00056-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.161	No_date	3:00
14.38 .273 .000						
[CN= 72.9: N= 3.00: Tp= .08]						

#-----|-----|

R0001:C00057-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.182	No_date	3:02
13.34 .253 .000						
[CN= 73.0: N= 3.00: Tp= .18]						

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00058-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	.497	No_date	3:00
13.67 n/a .000						
+	1.0	02:900mm	11.20	.372	No_date	3:01
13.84 n/a .000						
+	1.0	04:Ext-10A	27.90	.554	No_date	3:03

Alta Phase 2 (119-2528)

18

```

PRE_KCHU
7.95 n/a .000 + 1.0 03:Ext-11 3.90 .161 No_date 3:00
14.38 n/a .000 + 1.0 06:Ext-12 5.20 .182 No_date 3:02
13.34 n/a .000 SUM= 1.0 05:WET-STO 61.40 1.752 No_date 3:01
11.12 n/a .000
R0001:C00059-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 1.752 No_date 3:01
11.12 n/a .000 out <= 1.0 04:22 61.40 .282 No_date 4:13
11.12 n/a .000 overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 {MxStoUsed=.3829E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00060-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .105 No_date 3:02
8.41 .160 .000 [CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00061-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .105 No_date 3:02
8.41 n/a .000 + 1.0 04:22 61.40 .282 No_date 4:13
11.12 n/a .000 + 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 SUM= 1.0 05:22 66.30 .349 No_date 3:05
10.92 n/a .000
Alta Phase 2 (119-2528)

```

19

```

PRE_KCHU
#-----|-----|

#-----|-----10 YEAR KCHU-----|

#-----|-----|

R0001:C00062-----
-----
READ STORM
Filename = 10yr.stm

Comment = 10yr 6 hr Kifer Chu Chicago Storm Event

[SDT=60.00:SDUR= 6.00:PTOT= 66.00]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00063-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .199 No_date 3:01
20.91 .317 .000 [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00064-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .236 No_date 3:01
Alta Phase 2 (119-2528)

```

20

```

PRE_KCHU
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00065-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .125 No_date 3:01
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00066-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:INT-4 2.00 .123 No_date 3:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00067-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-1 1.40 .079 No_date 3:05
24.96 .378 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----|

#-----|-----|

#-----|-----|

R0001:C00068-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-1 3.50 .199 No_date 3:01
20.91 n/a .000 + 1.0 02:EXT-2 4.10 .236 No_date 3:01
20.91 n/a .000 + 1.0 03:EXT-3 2.20 .125 No_date 3:01
20.91 n/a .000 + 1.0 04:INT-4 2.00 .123 No_date 3:00
20.91 n/a .000 + 1.0 06:INT-1 1.40 .079 No_date 3:05
24.96 n/a .000 SUM= 1.0 01:825mm 13.20 .756 No_date 3:00
21.34 n/a .000
#-----|-----|

Alta Phase 2 (119-2528)

```

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```

PRE_KCHU

#-----|-----OUTLET B-----|

R0001:C00069-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:EXT-4 2.60 .148 No_date 3:01
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00070-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:INT-5 .90 .055 No_date 3:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00071-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-2 5.80 .285 No_date 3:06
22.68 .344 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00072-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:UNC-3 1.90 .106 No_date 3:00
19.12 .290 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00073-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 04:EXT-4 2.60 .148 No_date 3:01
20.91 n/a .000 + 1.0 05:INT-5 .90 .055 No_date 3:00

Alta Phase 2 (119-2528)

```

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PRE_KCHU
20.91 n/a .000
+ 1.0 06:INT-2 5.80 .285 No_date 3:06
22.68 n/a .000
+ 1.0 07:UNC-3 1.90 .106 No_date 3:00
19.12 n/a .000
SUM= 1.0 02:900mm 11.20 .574 No_date 3:00
21.52 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00074-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .302 No_date 3:01
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00075-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .043 No_date 3:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00076-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .218 No_date 3:10
22.92 .347 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00077-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .039 No_date 3:08
5.86 .089 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00078-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
Alta Phase 2 (119-2528) 23

PRE_KCHU
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .302 No_date 3:01
20.91 n/a .000
+ 1.0 06:INT-6 .70 .043 No_date 3:00
20.91 n/a .000
+ 1.0 07:INT-3 4.90 .218 No_date 3:10
22.92 n/a .000
+ 1.0 08:UNC-4 3.20 .039 No_date 3:08
5.86 n/a .000
SUM= 1.0 03:OUTLET C 14.00 .575 No_date 3:01
18.18 n/a .000
R0001:C00079-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .244 No_date 3:10
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00080-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .319 No_date 3:02
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00081-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .571 No_date 3:11
23.25 .352 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

Alta Phase 2 (119-2528) 24

PRE_KCHU

#-----|-----

R0001:C00082-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.575	No_date	3:01
18.18	n/a	.000				
		+	1.0	04:Ext-6	6.00	.244 No_date 3:10
20.91	n/a	.000				
		+	1.0	09:Ext-7	6.00	.319 No_date 3:02
20.91	n/a	.000				
		+	1.0	10:Ext-8	12.80	.571 No_date 3:11
23.25	n/a	.000				
		SUM=	1.0	06:NE_DITCH	38.80	1.635 No_date 3:03
20.70	n/a	.000				

R0001:C00083-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.362	No_date	3:07
24.93	.378	.000				
		[CN=	76.8: N=	3.00: Tp=	.34]	

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00084-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.635	No_date	3:03
20.70	n/a	.000				
		+	1.0	04:Ext-9	7.00	.362 No_date 3:07
24.93	n/a	.000				
		SUM=	1.0	05:21A	45.80	1.986 No_date 3:03
21.34	n/a	.000				

R0001:C00085-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

Alta Phase 2 (119-2528)

25

PRE_KCHU

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.884	No_date	3:03
12.78	.194	.000				
		[CN=	56.0: N=	3.00: Tp=	.20]	

#-----|-----

R0001:C00086-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.240	No_date	3:00
22.09	.335	.000				
		[CN=	72.9: N=	3.00: Tp=	.08]	

#-----|-----

R0001:C00087-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.280	No_date	3:02
20.91	.317	.000				
		[CN=	73.0: N=	3.00: Tp=	.18]	

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00088-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	.756	No_date	3:00
21.34	n/a	.000				
		+	1.0	02:900mm	11.20	.574 No_date 3:00
21.52	n/a	.000				
		+	1.0	04:Ext-10A	27.90	.884 No_date 3:03
12.78	n/a	.000				
		+	1.0	03:Ext-11	3.90	.240 No_date 3:00
22.09	n/a	.000				

Alta Phase 2 (119-2528)

26

```

PRE_KCHU
+      1.0 06:Ext-12      5.20      .280 No_date      3:02
20.91 n/a      .000
SUM=    1.0 05:WET-STO      61.40      2.714 No_date      3:01
17.50 n/a      .000
R0001:C00089-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR ->    1.0 05:WET-STO      61.40      2.714 No_date      3:01
17.50 n/a      .000
out <=    1.0 04:22      61.40      .361 No_date      4:19
17.50 n/a      .000
overflow <=    1.0 06:OVF      .00      .000 No_date      0:00
.00 n/a      .000
{MxStoUsed=.6720E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf=    0, TotDurOvf=
0.hrs}
R0001:C00090-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 03:Ext-10B      4.90      .163 No_date      3:02
13.22 .200      .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00091-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 03:Ext-10B      4.90      .163 No_date      3:02
13.22 n/a      .000
+      1.0 04:22      61.40      .361 No_date      4:19
17.50 n/a      .000
+      1.0 06:OVF      .00      .000 No_date      0:00
.00 n/a      .000
SUM=    1.0 05:22      66.30      .460 No_date      3:04
17.18 n/a      .000
#-----|-----|

Alta Phase 2 (119-2528)

```

27

```

PRE_KCHU
#-----|-----25 YEAR KCHU-----|

#-----|-----|

R0001:C00092-----
-----
READ STORM
Filename = 25yr.stm

Comment = 25-Year 6 hr Kifer Chu Chicago Storm Event

[SDT=60.00:SDUR= 6.00:PTOT= 77.90]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00093-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:EXT-1      3.50      .258 No_date      3:01
28.49 .366      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00094-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 02:EXT-2      4.10      .305 No_date      3:01
28.49 .366      .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00095-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528)

```

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Alta Phase 2 (119-2528)

Alta Phase 2 (119-2528)

```
PRE_KCHU
+ 1.0 07:UNC-3 1.90 .137 No_date 3:00
26.16 n/a .000
SUM= 1.0 02:900mm 11.20 .751 No_date 3:00
29.19 n/a .000
#-----|-----
```

```
#-----|-----OUTLET C-----|
```

```
R0001:C00104-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .390 No_date 3:01
28.49 .366 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00105-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .055 No_date 3:00
28.49 .366 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00106-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .287 No_date 3:10
30.88 .396 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00107-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .054 No_date 3:08
8.42 .108 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----
```

```
#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|
```

```
#-----|-----
```

```
R0001:C00108-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .390 No_date 3:01
28.49 n/a .000
Alta Phase 2 (119-2528)
```

31

```
PRE_KCHU
+ 1.0 06:INT-6 .70 .055 No_date 3:00
28.49 n/a .000
+ 1.0 07:INT-3 4.90 .287 No_date 3:10
30.88 n/a .000
+ 1.0 08:UNC-4 3.20 .054 No_date 3:08
8.42 n/a .000
SUM= 1.0 03:OUTLET C 14.00 .755 No_date 3:01
24.74 n/a .000
R0001:C00109-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .325 No_date 3:10
28.49 .366 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----
```

```
R0001:C00110-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .416 No_date 3:02
28.49 .366 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----
```

```
R0001:C00111-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .751 No_date 3:10
31.28 .402 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----
```

```
#-----|-----
```

```
#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |
```

```
#-----|-----
```

```
#-----|-----
```

Alta Phase 2 (119-2528)

32

PRE_KCHU

R0001:C00112-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 .755 No_date 3:01
24.74 n/a .000 + 1.0 04:Ext-6 6.00 .325 No_date 3:10
28.49 n/a .000 + 1.0 09:Ext-7 6.00 .416 No_date 3:02
28.49 n/a .000 + 1.0 10:Ext-8 12.80 .751 No_date 3:10
31.28 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 2.160 No_date 3:03
28.05 n/a .000

R0001:C00113-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .471 No_date 3:07
33.28 .427 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00114-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 2.160 No_date 3:03
28.05 n/a .000 + 1.0 04:Ext-9 7.00 .471 No_date 3:07
33.28 n/a .000 SUM= 1.0 05:21A 45.80 2.619 No_date 3:03
28.85 n/a .000

R0001:C00115-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.186 No_date 3:03
17.82 .229 .000

Alta Phase 2 (119-2528)

33

PRE_KCHU

[CN= 56.0: N= 3.00: Tp= .20]

#-----|-----

R0001:C00116-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .307 No_date 3:00
29.76 .382 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

R0001:C00117-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .365 No_date 3:02
28.49 .366 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00118-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 .980 No_date 3:00
29.00 n/a .000 + 1.0 02:900mm 11.20 .751 No_date 3:00
29.19 n/a .000 + 1.0 04:Ext-10A 27.90 1.186 No_date 3:03
17.82 n/a .000 + 1.0 03:Ext-11 3.90 .307 No_date 3:00
29.76 n/a .000 + 1.0 06:Ext-12 5.20 .365 No_date 3:02
28.49 n/a .000 SUM= 1.0 05:WET-ST0 61.40 3.563 No_date 3:01

Alta Phase 2 (119-2528)

34

```
PRE_KCHU
23.96 n/a .000
R0001:C00119-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 3.563 No_date 3:01
23.96 n/a .000
out <= 1.0 04:22 61.40 .430 No_date 4:35
23.96 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.9622E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00120-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .216 No_date 3:02
18.19 .234 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----
```

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

```
R0001:C00121-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .216 No_date 3:02
18.19 n/a .000
+ 1.0 04:22 61.40 .430 No_date 4:35
23.96 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .563 No_date 3:04
23.53 n/a .000
#-----|-----
```

#-----|-----50YEAR KCHU-----|

Alta Phase 2 (119-2528) 35

PRE_KCHU

#-----|-----

R0001:C00122-----

READ STORM
Filename = 50yr.stm

Comment = 50-Year 6 hr Kifer Chu Chicago Storm Event

[SDT=60.00:SDUR= 6.00:PTOT= 83.90]

#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

```
R0001:C00123-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .290 No_date 3:01
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00124-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .343 No_date 3:01
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00125-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .182 No_date 3:01
32.54 .388 .000
```

Alta Phase 2 (119-2528) 36

PRE_KCHU
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00126-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:INT-4 2.00 .177 No_date 3:00
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00127-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-1 1.40 .115 No_date 3:04
37.73 .450 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00128-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-1 3.50 .290 No_date 3:01
32.54 n/a .000
+ 1.0 02:EXT-2 4.10 .343 No_date 3:01
32.54 n/a .000
+ 1.0 03:EXT-3 2.20 .182 No_date 3:01
32.54 n/a .000
+ 1.0 04:INT-4 2.00 .177 No_date 3:00
32.54 n/a .000
+ 1.0 06:INT-1 1.40 .115 No_date 3:04
37.73 n/a .000
SUM= 1.0 01:825mm 13.20 1.100 No_date 3:00
33.09 n/a .000
#-----|-----|

#-----|-----OUTLET B-----|

Alta Phase 2 (119-2528)

37

PRE_KCHU
R0001:C00129-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:EXT-4 2.60 .215 No_date 3:01
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00130-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:INT-5 .90 .080 No_date 3:00
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00131-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-2 5.80 .421 No_date 3:06
34.82 .415 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00132-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:UNC-3 1.90 .154 No_date 3:00
29.94 .357 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00133-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 04:EXT-4 2.60 .215 No_date 3:01
32.54 n/a .000
+ 1.0 05:INT-5 .90 .080 No_date 3:00
32.54 n/a .000
+ 1.0 06:INT-2 5.80 .421 No_date 3:06
34.82 n/a .000
+ 1.0 07:UNC-3 1.90 .154 No_date 3:00
29.94 n/a .000
SUM= 1.0 02:900mm 11.20 .847 No_date 3:00

Alta Phase 2 (119-2528)

38

PRE_KCHU
33.28 n/a .000
#-----|-----

#-----|-----OUTLET C-----

R0001:C00134-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .438 No_date 3:01
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00135-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .062 No_date 3:00
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00136-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .325 No_date 3:09
35.11 .418 .000
[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00137-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .063 No_date 3:08
9.85 .117 .000
[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----

#-----|-----

R0001:C00138-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .438 No_date 3:01
32.54 n/a .000
+ 1.0 06:INT-6 .70 .062 No_date 3:00
32.54 n/a .000
+ 1.0 07:INT-3 4.90 .325 No_date 3:09

Alta Phase 2 (119-2528)

39

PRE_KCHU
35.11 n/a .000
+ 1.0 08:UNC-4 3.20 .063 No_date 3:08
9.85 n/a .000
SUM= 1.0 03:OUTLET C 14.00 .853 No_date 3:01
28.25 n/a .000
R0001:C00139-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .369 No_date 3:10
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00140-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .469 No_date 3:02
32.54 .388 .000
[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00141-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .848 No_date 3:10
35.55 .424 .000
[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

40


```

PRE_KCHU
R0001:C00142-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 03:OUTLET C      14.00      .853 No_date    3:01
28.25 n/a      .000
      +          1.0 04:Ext-6          6.00      .369 No_date    3:10
32.54 n/a      .000
      +          1.0 09:Ext-7          6.00      .469 No_date    3:02
32.54 n/a      .000
      +          1.0 10:Ext-8          12.80     .848 No_date    3:10
35.55 n/a      .000
      SUM=        1.0 06:NE_DITCH      38.80     2.446 No_date    3:02
31.98 n/a      .000
R0001:C00143-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 04:Ext-9          7.00      .529 No_date    3:07
37.70 .449      .000
      [CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

```

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

```

R0001:C00144-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 06:NE_DITCH      38.80     2.446 No_date    3:02
31.98 n/a      .000
      +          1.0 04:Ext-9          7.00      .529 No_date    3:07
37.70 n/a      .000
      SUM=        1.0 05:21A          45.80     2.963 No_date    3:03
32.86 n/a      .000
R0001:C00145-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 04:Ext-10A      27.90     1.355 No_date    3:03
20.58 .245      .000
      [CN= 56.0: N= 3.00: Tp= .20]
#-----|-----

```

Alta Phase 2 (119-2528)

41

PRE_KCHU

```

R0001:C00146-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 03:Ext-11        3.90      .343 No_date    3:00
33.85 .403      .000
      [CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

```

```

R0001:C00147-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 06:Ext-12        5.20      .411 No_date    3:02
32.54 .388      .000
      [CN= 73.0: N= 3.00: Tp= .18]
#-----|-----

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

```

R0001:C00148-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 01:825mm        13.20     1.100 No_date    3:00
33.09 n/a      .000
      +          1.0 02:900mm        11.20      .847 No_date    3:00
33.28 n/a      .000
      +          1.0 04:Ext-10A       27.90     1.355 No_date    3:03
20.58 n/a      .000
      +          1.0 03:Ext-11        3.90      .343 No_date    3:00
33.85 n/a      .000
      +          1.0 06:Ext-12        5.20      .411 No_date    3:02
32.54 n/a      .000
      SUM=        1.0 05:WET-STO       61.40     4.028 No_date    3:01
27.44 n/a      .000
R0001:C00149-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

```

Alta Phase 2 (119-2528)

42

```

PRE_KCHU
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 4.028 No_date 3:01
27.44 n/a .000
out <= 1.0 04:22 61.40 .464 No_date 5:03
27.44 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1121E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00150-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .246 No_date 3:02
20.92 .249 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

#-----|-----

R0001:C00151-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .246 No_date 3:02
20.92 n/a .000
+ 1.0 04:22 61.40 .464 No_date 5:03
27.44 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .617 No_date 3:04
26.96 n/a .000
#-----|-----

#-----|-----100 YEAR KCHU-----|

#-----|-----

Alta Phase 2 (119-2528)

```

43

```

PRE_KCHU

R0001:C00152-----
-----
READ STORM
Filename = 100yr.stm

Comment = 100-Year 6 hr Kifer Chu Chicago Storm Event

[SDT=60.00:SDUR= 6.00:PTOT= 96.00]
#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

#-----|-----

R0001:C00153-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .359 No_date 3:01
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00154-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .423 No_date 3:01
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00155-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .225 No_date 3:01
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00156-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

```

44

```

PRE_KCHU
CALIB NASHYD          1.0 04:INT-4          2.00      .218 No_date    3:00
41.10 .428      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00157-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-1          1.40      .142 No_date    3:04
46.99 .490      .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----|

#-----|-----|

#-----|-----|

R0001:C00158-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
41.10 n/a      .000      1.0 05:EXT-1          3.50      .359 No_date    3:01
+
41.10 n/a      .000      1.0 02:EXT-2          4.10      .423 No_date    3:01
+
41.10 n/a      .000      1.0 03:EXT-3          2.20      .225 No_date    3:01
+
41.10 n/a      .000      1.0 04:INT-4          2.00      .218 No_date    3:00
+
41.10 n/a      .000      1.0 06:INT-1          1.40      .142 No_date    3:04
46.99 n/a      .000
SUM= 1.0 01:825mm      13.20      1.360 No_date    3:00
41.73 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00159-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

45

```

PRE_KCHU
CALIB NASHYD          1.0 04:EXT-4          2.60      .266 No_date    3:01
41.10 .428      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00160-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 05:INT-5          .90      .098 No_date    3:00
41.10 .428      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00161-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-2          5.80      .524 No_date    3:06
43.70 .455      .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00162-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 07:UNC-3          1.90      .191 No_date    3:00
37.99 .396      .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00163-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
41.10 n/a      .000      1.0 04:EXT-4          2.60      .266 No_date    3:01
+
41.10 n/a      .000      1.0 05:INT-5          .90      .098 No_date    3:00
+
41.10 n/a      .000      1.0 06:INT-2          5.80      .524 No_date    3:06
+
43.70 n/a      .000      1.0 07:UNC-3          1.90      .191 No_date    3:00
37.99 n/a      .000
SUM= 1.0 02:900mm      11.20      1.054 No_date    3:00
41.92 n/a      .000
#-----|-----|

Alta Phase 2 (119-2528)

```

46

PRE_KCHU

#-----|-----OUTLET C-----|

R0001:C00164-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .540 No_date 3:00
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00165-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .076 No_date 3:00
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00166-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .406 No_date 3:09
44.02 .459 .000
[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00167-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .083 No_date 3:08
13.05 .136 .000
[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00168-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .540 No_date 3:00
41.10 n/a .000
+ 1.0 06:INT-6 .70 .076 No_date 3:00
41.10 n/a .000
+ 1.0 07:INT-3 4.90 .406 No_date 3:09
44.02 n/a .000
+ 1.0 08:UNC-4 3.20 .083 No_date 3:08
13.05 n/a .000

Alta Phase 2 (119-2528)

47

PRE_KCHU

SUM= 1.0 03:OUTLET C 14.00 1.066 No_date 3:01
35.71 n/a .000
R0001:C00169-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .464 No_date 3:09
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----

R0001:C00170-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .583 No_date 3:02
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00171-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 1.059 No_date 3:09
44.52 .464 .000
[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

R0001:C00172-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 1.066 No_date 3:01

Alta Phase 2 (119-2528)

48

```
PRE_KCHU
35.71 n/a .000
+ 1.0 04:Ext-6 6.00 .464 No_date 3:09
41.10 n/a .000
+ 1.0 09:Ext-7 6.00 .583 No_date 3:02
41.10 n/a .000
+ 1.0 10:Ext-8 12.80 1.059 No_date 3:09
44.52 n/a .000
SUM= 1.0 06:NE_DITCH 38.80 3.069 No_date 3:02
40.28 n/a .000
R0001:C00173-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .655 No_date 3:07
46.96 .489 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----|
```

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

```
R0001:C00174-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 3.069 No_date 3:02
40.28 n/a .000
+ 1.0 04:Ext-9 7.00 .655 No_date 3:07
46.96 n/a .000
SUM= 1.0 05:21A 45.80 3.709 No_date 3:03
41.31 n/a .000
R0001:C00175-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.730 No_date 3:03
26.57 .277 .000
[CN= 56.0: N= 3.00: Tp= .20]
#-----|-----|
```

R0001:C00176-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528) 49

```
PRE_KCHU
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .421 No_date 3:00
42.48 .443 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----|
```

```
R0001:C00177-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .510 No_date 3:02
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----|
```

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

```
R0001:C00178-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.360 No_date 3:00
41.73 n/a .000
+ 1.0 02:900mm 11.20 1.054 No_date 3:00
41.92 n/a .000
+ 1.0 04:Ext-10A 27.90 1.730 No_date 3:03
26.57 n/a .000
+ 1.0 03:Ext-11 3.90 .421 No_date 3:00
42.48 n/a .000
+ 1.0 06:Ext-12 5.20 .510 No_date 3:02
41.10 n/a .000
SUM= 1.0 05:WET-STO 61.40 5.040 No_date 3:01
34.87 n/a .000
R0001:C00179-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 5.040 No_date 3:01
34.87 n/a .000
out <= 1.0 04:22 61.40 .506 No_date 5:11
Alta Phase 2 (119-2528) 50
```

PRE_KCHU
34.87 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1501E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00180-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .312 No_date 3:02
26.82 .279 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00181-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .312 No_date 3:02
26.82 n/a .000
+ 1.0 04:22 61.40 .506 No_date 5:11
34.87 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .738 No_date 3:04
34.27 n/a .000
R0001:C00182-----

FINISH

WARNINGS / ERRORS / NOTES

Simulation ended on 2021-06-30 at 12:16:42
=====

Alta Phase 2 (119-2528)

PRE_KCHU

PRE_Craigleith_SCS12

=====

SSSSS W W M M H H Y Y M M 000 222 000 11
77777 =====
S W W W MM MM H H Y Y MM MM O O 2 0 0 11
7 7
SSSSS W W W M M M H H H H Y M M M O O 2 0 0 11
7 Ver4.05.0
S W W M M H H Y M M O O 222 0 0 11
7 APR 2017
SSSSS W W M M H H Y M M 000 2 0 0 11
7 =====
2 0 0 11
7 # 3737016
StormWater Management HYdrologic Model 222 000 11
7 =====

***** SWMHYMO Ver4.05.0

***** A single event and continuous hydrologic simulation model

***** based on the principles of HYMO and its successors

***** OTTHYMO-83 and OTTHYMO-89.

***** Distributed by: J.F. Sabourin and Associates Inc.

***** Ottawa, Ontario: (613) 836-3884

***** Gatineau, Quebec: (819) 243-6858

***** E-Mail: swmhymo@jfsa.com

+++++

Alta Phase 2 (119-2528)

1

PRE_Craigleith_SCS12

++++++ Licensed user: C.F. Crozier & Associates Inc.

+++++

+++++

+++++

Collingwood

SERIAL#:3737016

+++++

***** +++++ PROGRAM ARRAY DIMENSIONS +++++

***** Maximum value for ID numbers : 11

***** Max. number of rainfall points: 105408

***** Max. number of flow points : 105408

***** S U M M A R Y O U T P U T

***** * RUN DATE: 2021-06-30 TIME: 12:17:49 RUN COUNTER: 000004

* Input file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS12\PRE_Craigl*
* eith_SCS12.Dat

* Output file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS12\PRE_Craigl*
* eith_SCS12.out

* Summary file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS12\PRE_Craigl*
* eith_SCS12.sum

* User comments:

Alta Phase 2 (119-2528)

2

PRE_Craigleith_SCS12

*

1:_____

*_____

2:_____

*_____

3:_____

*_____

#*****

Project Name: [ALTA PHASE II] Project Number: [119-2528]

Date : 2021.06.30

Modified : 2021.06.30

Modeller : [Z. Holland]

Company : C.F. Crozier & Associates Inc.

License # : 3737016

#*****

RUN#:COMMAND#

R0001:C00001-----

Alta Phase 2 (119-2528)

3

PRE_Craigleith_SCS12

START

[TZERO = .00 hrs on 0]

[METOUT= 2 (1=imperial, 2=metric output)]

[NSTORM= 0]

[NRUN = 0001]

#-----|-----

#-----|-----2YR SCS (12HR)-----|

#-----|-----

R0001:C00002-----

MASS STORM

Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase

II\2021.06.30\Craigleith_SC

Comment = 12 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 12.00:PTOT= 39.60]

#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

R0001:C00003-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

4


```

PRE_Craigleith_SCS12
CALIB NASHYD      1.0 05:EXT-1      3.50      .087 No_date      6:03
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 02:EXT-2      4.10      .107 No_date      6:03
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 03:EXT-3      2.20      .055 No_date      6:03
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:INT-4      2.00      .071 No_date      6:00
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-1      1.40      .029 No_date      6:11
9.21 .233 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
7.09 n/a .000      1.0 05:EXT-1      3.50      .087 No_date      6:03
7.09 n/a .000      +      1.0 02:EXT-2      4.10      .107 No_date      6:03
7.09 n/a .000      +      1.0 03:EXT-3      2.20      .055 No_date      6:03
7.09 n/a .000      +      1.0 04:INT-4      2.00      .071 No_date      6:00

Alta Phase 2 (119-2528)

```

```

PRE_Craigleith_SCS12
7.09 n/a .000      +      1.0 06:INT-1      1.40      .029 No_date      6:11
9.21 n/a .000      SUM=      1.0 01:825mm      13.20      .327 No_date      6:02
7.32 n/a .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:EXT-4      2.60      .065 No_date      6:03
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:INT-5      .90      .032 No_date      6:00
7.09 .179 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-2      5.80      .093 No_date      6:15
8.00 .202 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 07:UNC-3      1.90      .058 No_date      6:00
6.44 .163 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

Alta Phase 2 (119-2528)

```

PRE_Craigleith_SCS12

```
R0001:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 04:EXT-4          2.60      .065 No_date    6:03
7.09 n/a          .000
  +          1.0 05:INT-5              .90      .032 No_date    6:00
7.09 n/a          .000
  +          1.0 06:INT-2              5.80      .093 No_date    6:15
8.00 n/a          .000
  +          1.0 07:UNC-3              1.90      .058 No_date    6:00
6.44 n/a          .000
  SUM=          1.0 02:900mm          11.20      .203 No_date    6:02
7.45 n/a          .000
#-----|-----
```

```
#-----|-----OUTLET C-----|
```

```
R0001:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 05:EXT-5          5.20      .142 No_date    6:02
7.09 .179          .000
  [CN= 73.0: N= 3.00: Tp= .11]
R0001:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-6              .70      .025 No_date    6:00
7.09 .179          .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 07:INT-3              4.90      .068 No_date    6:21
8.16 .206          .000
  [CN= 74.8: N= 3.00: Tp= .39]
R0001:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 08:UNC-4              3.20      .010 No_date    6:16
1.74 .044          .000
  [CN= 34.4: N= 3.00: Tp= .32]
#-----|-----
```

```
#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|
```

Alta Phase 2 (119-2528)

7

PRE_Craigleith_SCS12

```
#-----|-----|
R0001:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 05:EXT-5          5.20      .142 No_date    6:02
7.09 n/a          .000
  +          1.0 06:INT-6              .70      .025 No_date    6:00
7.09 n/a          .000
  +          1.0 07:INT-3              4.90      .068 No_date    6:21
8.16 n/a          .000
  +          1.0 08:UNC-4              3.20      .010 No_date    6:16
1.74 n/a          .000
  SUM=          1.0 03:OUTLET C          14.00      .203 No_date    6:02
6.24 n/a          .000
R0001:C00019-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:Ext-6          6.00      .071 No_date    6:22
7.09 .179          .000
  [CN= 73.0: N= 3.00: Tp= .39]
#-----|-----|
```

```
R0001:C00020-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 09:Ext-7          6.00      .118 No_date    6:07
7.09 .179          .000
  [CN= 73.0: N= 3.00: Tp= .19]
#-----|-----|
```

```
R0001:C00021-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 10:Ext-8          12.80      .179 No_date    6:22
8.31 .210          .000
  [CN= 75.2: N= 3.00: Tp= .40]
#-----|-----|
```

```
#-----|-----|
```

Alta Phase 2 (119-2528)

8

PRE_Craigleith_SCS12

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----|

#-----|-----|

R0001:C00022-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 03:OUTLET C 14.00 .203 No_date 6:02

6.24 n/a .000 + 1.0 04:Ext-6 6.00 .071 No_date 6:22

7.09 n/a .000 + 1.0 09:Ext-7 6.00 .118 No_date 6:07

7.09 n/a .000 + 1.0 10:Ext-8 12.80 .179 No_date 6:22

8.31 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 .480 No_date 6:09

7.19 n/a .000

R0001:C00023-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-9 7.00 .124 No_date 6:16

9.19 .232 .000

[CN= 76.8: N= 3.00: Tp= .34]

#-----|-----|

#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00024-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 06:NE_DITCH 38.80 .480 No_date 6:09

Alta Phase 2 (119-2528)

9

PRE_Craigleith_SCS12

7.19 n/a .000 + 1.0 04:Ext-9 7.00 .124 No_date 6:16

9.19 n/a .000 SUM= 1.0 05:21A 45.80 .596 No_date 6:11

7.49 n/a .000

R0001:C00025-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-10A 27.90 .306 No_date 6:07

4.14 .105 .000

[CN= 56.0: N= 3.00: Tp= .20]

#-----|-----|

R0001:C00026-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 03:Ext-11 3.90 .137 No_date 6:01

7.94 .201 .000

[CN= 72.9: N= 3.00: Tp= .08]

#-----|-----|

R0001:C00027-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:Ext-12 5.20 .106 No_date 6:06

7.09 .179 .000

[CN= 73.0: N= 3.00: Tp= .18]

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00028-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 01:825mm 13.20 .327 No_date 6:02

7.32 n/a .000

Alta Phase 2 (119-2528)

10

```

PRE_Craigleith_SCS12
+ 1.0 02:900mm 11.20 .203 No_date 6:02
7.45 n/a .000
+ 1.0 04:Ext-10A 27.90 .306 No_date 6:07
4.14 n/a .000
+ 1.0 03:Ext-11 3.90 .137 No_date 6:01
7.94 n/a .000
+ 1.0 06:Ext-12 5.20 .106 No_date 6:06
7.09 n/a .000
SUM= 1.0 05:WET-STO 61.40 1.020 No_date 6:03
5.92 n/a .000
R0001:C00029-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 1.020 No_date 6:03
5.92 n/a .000
out <= 1.0 04:22 61.40 .200 No_date 6:53
5.92 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1379E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00030-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .068 No_date 6:05
4.57 .115 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00031-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .068 No_date 6:05
4.57 n/a .000
+ 1.0 04:22 61.40 .200 No_date 6:53
5.92 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00

Alta Phase 2 (119-2528)

```

11

```

PRE_Craigleith_SCS12
.00 n/a .000
SUM= 1.0 05:22 66.30 .238 No_date 6:08
5.82 n/a .000
#-----|-----|

#-----|-----5YR SCS (12HR)-----|

#-----|-----|

R0001:C00032-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 12 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 12.00:PTOT= 55.20]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00033-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .189 No_date 6:03
14.68 .266 .000
[CN= 73.0: N= 3.00: Tp= .13]

Alta Phase 2 (119-2528)

```

12

```

PRE_Craigleith_SCS12
R0001:C00034-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 02:EXT-2          4.10      .230 No_date    6:03
14.68 .266      .000
    [CN= 73.0: N= 3.00: Tp= .12]
R0001:C00035-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 03:EXT-3          2.20      .119 No_date    6:03
14.68 .266      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00036-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:INT-4          2.00      .146 No_date    6:00
14.68 .266      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00037-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-1          1.40      .060 No_date    6:11
17.96 .325      .000
    [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00038-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    ADD HYD              1.0 05:EXT-1          3.50      .189 No_date    6:03
14.68 n/a        .000
    +                    1.0 02:EXT-2          4.10      .230 No_date    6:03
14.68 n/a        .000
    +                    1.0 03:EXT-3          2.20      .119 No_date    6:03
14.68 n/a        .000
    +                    1.0 04:INT-4          2.00      .146 No_date    6:00
14.68 n/a        .000
    +                    1.0 06:INT-1          1.40      .060 No_date    6:11
17.96 n/a        .000
Alta Phase 2 (119-2528)

```

13

```

PRE_Craigleith_SCS12
SUM=      1.0 01:825mm      13.20      .704 No_date    6:02
15.03 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00039-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:EXT-4          2.60      .141 No_date    6:03
14.68 .266      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00040-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 05:INT-5          .90      .066 No_date    6:00
14.68 .266      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00041-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-2          5.80      .200 No_date    6:14
16.11 .292      .000
    [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00042-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 07:UNC-3          1.90      .121 No_date    6:00
13.37 .242      .000
    [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00043-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

14

```

PRE_Craigleith_SCS12
ADD HYD          1.0 04:EXT-4          2.60      .141 No_date    6:03
14.68 n/a      .000
14.68 n/a      .000 +          1.0 05:INT-5          .90      .066 No_date    6:00
14.68 n/a      .000 +          1.0 06:INT-2          5.80      .200 No_date    6:14
16.11 n/a      .000 +          1.0 07:UNC-3          1.90      .121 No_date    6:00
13.37 n/a      .000
SUM=          1.0 02:900mm          11.20      .444 No_date    6:01
15.20 n/a      .000
#-----|-----

```

```

#-----|-----OUTLET C-----|

```

```

R0001:C00044-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 05:EXT-5          5.20      .304 No_date    6:02
14.68 .266      .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00045-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-6          .70      .051 No_date    6:00
14.68 .266      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00046-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 07:INT-3          4.90      .145 No_date    6:19
16.32 .296      .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00047-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 08:UNC-4          3.20      .024 No_date    6:15
3.91 .071      .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

```

```

#-----|-----

```

Alta Phase 2 (119-2528)

15

PRE_Craigleith_SCS12

```

R0001:C00048-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD          1.0 05:EXT-5          5.20      .304 No_date    6:02
14.68 n/a      .000
14.68 n/a      .000 +          1.0 06:INT-6          .70      .051 No_date    6:00
14.68 n/a      .000 +          1.0 07:INT-3          4.90      .145 No_date    6:19
16.32 n/a      .000 +          1.0 08:UNC-4          3.20      .024 No_date    6:15
3.91 n/a      .000
SUM=          1.0 03:OUTLET C          14.00      .445 No_date    6:02
12.79 n/a      .000
R0001:C00049-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 04:Ext-6          6.00      .158 No_date    6:20
14.68 .266      .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

```

```

R0001:C00050-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 09:Ext-7          6.00      .261 No_date    6:06
14.68 .266      .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

```

```

R0001:C00051-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 10:Ext-8          12.80      .379 No_date    6:20
16.58 .300      .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

```

```

#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

```

Alta Phase 2 (119-2528)

16

PRE_Craigleith_SCS12

#-----|-----|

#-----|-----|

R0001:C00052-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.445	No_date	6:02
12.79 n/a .000						
+	1.0	04:Ext-6	6.00	.158	No_date	6:20
14.68 n/a .000						
+	1.0	09:Ext-7	6.00	.261	No_date	6:06
14.68 n/a .000						
+	1.0	10:Ext-8	12.80	.379	No_date	6:20
16.58 n/a .000						
SUM=	1.0	06:NE_DITCH	38.80	1.059	No_date	6:07
14.62 n/a .000						

R0001:C00053-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.255	No_date	6:15
17.94 .325 .000						
[CN= 76.8: N= 3.00: Tp= .34]						

#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00054-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.059	No_date	6:07
14.62 n/a .000						
+	1.0	04:Ext-9	7.00	.255	No_date	6:15
17.94 n/a .000						

Alta Phase 2 (119-2528)

17

PRE_Craigleith_SCS12

SUM= 1.0 05:21A 45.80 1.292 No_date 6:09

15.13 n/a .000
R0001:C00055-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.677	No_date	6:07
8.79 .159 .000						
[CN= 56.0: N= 3.00: Tp= .20]						

#-----|-----|

R0001:C00056-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.273	No_date	6:01
15.75 .285 .000						
[CN= 72.9: N= 3.00: Tp= .08]						

#-----|-----|

R0001:C00057-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.233	No_date	6:06
14.68 .266 .000						
[CN= 73.0: N= 3.00: Tp= .18]						

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00058-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	.704	No_date	6:02
15.03 n/a .000						
+	1.0	02:900mm	11.20	.444	No_date	6:01
15.20 n/a .000						
+	1.0	04:Ext-10A	27.90	.677	No_date	6:07

Alta Phase 2 (119-2528)

18

```

PRE_Craigleith_SCS12
8.79 n/a .000 + 1.0 03:Ext-11 3.90 .273 No_date 6:01
15.75 n/a .000 + 1.0 06:Ext-12 5.20 .233 No_date 6:06
14.68 n/a .000 SUM= 1.0 05:WET-STO 61.40 2.218 No_date 6:02
12.24 n/a .000
R0001:C00059-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 2.218 No_date 6:02
12.24 n/a .000 out <= 1.0 04:22 61.40 .277 No_date 7:12
12.24 n/a .000 overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 {MxStoUsed=.3638E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00060-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .139 No_date 6:05
9.24 .167 .000 [CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00061-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .139 No_date 6:05
9.24 n/a .000 + 1.0 04:22 61.40 .277 No_date 7:12
12.24 n/a .000 + 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 SUM= 1.0 05:22 66.30 .351 No_date 6:08
12.02 n/a .000
Alta Phase 2 (119-2528)

```

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```

PRE_Craigleith_SCS12
#-----|-----|

#-----|-----10YR SCS (12HR)-----|

#-----|-----|

R0001:C00062-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 12 hour SCS II storm mass curve
[SDT= 1.00:SDUR= 12.00:PTOT= 66.00]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00063-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .272 No_date 6:03
20.91 .317 .000 [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00064-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .331 No_date 6:02
Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00065-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .171 No_date 6:03
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00066-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:INT-4 2.00 .207 No_date 6:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00067-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-1 1.40 .085 No_date 6:10
24.96 .378 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----|

#-----|-----|

#-----|-----|

R0001:C00068-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-1 3.50 .272 No_date 6:03
20.91 n/a .000 + 1.0 02:EXT-2 4.10 .331 No_date 6:02
20.91 n/a .000 + 1.0 03:EXT-3 2.20 .171 No_date 6:03
20.91 n/a .000 + 1.0 04:INT-4 2.00 .207 No_date 6:00
20.91 n/a .000 + 1.0 06:INT-1 1.40 .085 No_date 6:10
24.96 n/a .000 SUM= 1.0 01:825mm 13.20 1.012 No_date 6:01
21.34 n/a .000
#-----|-----|

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS12

#-----|-----OUTLET B-----|

R0001:C00069-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:EXT-4 2.60 .202 No_date 6:03
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00070-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:INT-5 .90 .093 No_date 6:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00071-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-2 5.80 .287 No_date 6:13
22.68 .344 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00072-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:UNC-3 1.90 .172 No_date 6:00
19.12 .290 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00073-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 04:EXT-4 2.60 .202 No_date 6:03
20.91 n/a .000 + 1.0 05:INT-5 .90 .093 No_date 6:00

Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS12
20.91 n/a .000 + 1.0 06:INT-2 5.80 .287 No_date 6:13
22.68 n/a .000 + 1.0 07:UNC-3 1.90 .172 No_date 6:00
19.12 n/a .000 SUM= 1.0 02:900mm 11.20 .642 No_date 6:01
21.52 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00074-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .437 No_date 6:02
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00075-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .072 No_date 6:00
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00076-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .208 No_date 6:19
22.92 .347 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00077-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .037 No_date 6:15
5.86 .089 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00078-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
Alta Phase 2 (119-2528) 23

PRE_Craigleith_SCS12
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .437 No_date 6:02
20.91 n/a .000 + 1.0 06:INT-6 .70 .072 No_date 6:00
20.91 n/a .000 + 1.0 07:INT-3 4.90 .208 No_date 6:19
22.92 n/a .000 + 1.0 08:UNC-4 3.20 .037 No_date 6:15
5.86 n/a .000 SUM= 1.0 03:OUTLET C 14.00 .644 No_date 6:02
18.18 n/a .000
R0001:C00079-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .230 No_date 6:19
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00080-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .378 No_date 6:06
20.91 .317 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00081-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .542 No_date 6:19
23.25 .352 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

Alta Phase 2 (119-2528) 24

PRE_Craigleith_SCS12

#-----|-----

R0001:C00082-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.644	No_date	6:02
18.18 n/a .000						
+	1.0	04:Ext-6	6.00	.230	No_date	6:19
20.91 n/a .000						
+	1.0	09:Ext-7	6.00	.378	No_date	6:06
20.91 n/a .000						
+	1.0	10:Ext-8	12.80	.542	No_date	6:19
23.25 n/a .000						
SUM=	1.0	06:NE_DITCH	38.80	1.540	No_date	6:07
20.70 n/a .000						

R0001:C00083-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.360	No_date	6:15
24.93 .378 .000						
[CN= 76.8: N= 3.00: Tp= .34]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00084-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.540	No_date	6:07
20.70 n/a .000						
+	1.0	04:Ext-9	7.00	.360	No_date	6:15
24.93 n/a .000						
SUM=	1.0	05:21A	45.80	1.866	No_date	6:09
21.34 n/a .000						

R0001:C00085-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.998	No_date	6:07
12.78 .194 .000						
[CN= 56.0: N= 3.00: Tp= .20]						

#-----|-----

R0001:C00086-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.382	No_date	6:01
22.10 .335 .000						
[CN= 72.9: N= 3.00: Tp= .08]						

#-----|-----

R0001:C00087-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.338	No_date	6:05
20.91 .317 .000						
[CN= 73.0: N= 3.00: Tp= .18]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00088-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	1.012	No_date	6:01
21.34 n/a .000						
+	1.0	02:900mm	11.20	.642	No_date	6:01
21.52 n/a .000						
+	1.0	04:Ext-10A	27.90	.998	No_date	6:07
12.78 n/a .000						
+	1.0	03:Ext-11	3.90	.382	No_date	6:01
22.10 n/a .000						

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12
+      1.0 06:Ext-12      5.20      .338 No_date      6:05
20.91 n/a      .000
SUM=      1.0 05:WET-STO      61.40      3.218 No_date      6:02
17.50 n/a      .000
R0001:C00089-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR ->      1.0 05:WET-STO      61.40      3.218 No_date      6:02
17.50 n/a      .000
out <=      1.0 04:22      61.40      .333 No_date      7:25
17.50 n/a      .000
overflow <=      1.0 06:OVF      .00      .000 No_date      0:00
.00 n/a      .000
{MxStoUsed=.5644E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf=      0, TotDurOvf=
0.hrs}
R0001:C00090-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 03:Ext-10B      4.90      .200 No_date      6:05
13.22 .200      .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

R0001:C00091-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 03:Ext-10B      4.90      .200 No_date      6:05
13.22 n/a      .000
+      1.0 04:22      61.40      .333 No_date      7:25
17.50 n/a      .000
+      1.0 06:OVF      .00      .000 No_date      0:00
.00 n/a      .000
SUM=      1.0 05:22      66.30      .447 No_date      6:07
17.18 n/a      .000
#-----|-----

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS12
#-----|-----25YR SCS (12HR)-----|

#-----|-----|

R0001:C00092-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 12 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 12.00:PTOT= 79.20]
#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

R0001:C00093-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:EXT-1      3.50      .385 No_date      6:03
29.35 .371      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00094-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 02:EXT-2      4.10      .467 No_date      6:02
29.35 .371      .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00095-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS12
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 03:EXT-3          2.20      .242 No_date    6:03
29.35 .371      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00096-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:INT-4          2.00      .287 No_date    6:00
29.35 .371      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00097-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-1          1.40      .117 No_date    6:10
34.25 .433      .000
  [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----|

#-----|-----|

#-----|-----|

R0001:C00098-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD              1.0 05:EXT-1          3.50      .385 No_date    6:03
29.35 n/a      .000
  + 1.0 02:EXT-2          4.10      .467 No_date    6:02
29.35 n/a      .000
  + 1.0 03:EXT-3          2.20      .242 No_date    6:03
29.35 n/a      .000
  + 1.0 04:INT-4          2.00      .287 No_date    6:00
29.35 n/a      .000
  + 1.0 06:INT-1          1.40      .117 No_date    6:10
34.25 n/a      .000
  SUM= 1.0 01:825mm      13.20      1.429 No_date    6:01
29.87 n/a      .000
#-----|-----|

```

```

PRE_Craigleith_SCS12
#-----|-----OUTLET B-----|

R0001:C00099-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:EXT-4          2.60      .286 No_date    6:03
29.35 .371      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00100-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 05:INT-5          .90      .129 No_date    6:00
29.35 .371      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00101-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-2          5.80      .404 No_date    6:13
31.50 .398      .000
  [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00102-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 07:UNC-3          1.90      .242 No_date    6:00
26.97 .340      .000
  [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00103-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD              1.0 04:EXT-4          2.60      .286 No_date    6:03
29.35 n/a      .000
  + 1.0 05:INT-5          .90      .129 No_date    6:00
29.35 n/a      .000
  + 1.0 06:INT-2          5.80      .404 No_date    6:13
31.50 n/a      .000
Alta Phase 2 (119-2528)

```

PRE_Craigleith_SCS12
+ 1.0 07:UNC-3 1.90 .242 No_date 6:00
26.97 n/a .000
SUM= 1.0 02:900mm 11.20 .910 No_date 6:01
30.06 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00104-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .615 No_date 6:02
29.35 .371 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00105-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .100 No_date 6:00
29.35 .371 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00106-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .293 No_date 6:18
31.78 .401 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00107-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .055 No_date 6:14
8.72 .110 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00108-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .615 No_date 6:02
29.35 n/a .000
Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12
+ 1.0 06:INT-6 .70 .100 No_date 6:00
29.35 n/a .000
+ 1.0 07:INT-3 4.90 .293 No_date 6:18
31.78 n/a .000
+ 1.0 08:UNC-4 3.20 .055 No_date 6:14
8.72 n/a .000
SUM= 1.0 03:OUTLET C 14.00 .914 No_date 6:02
25.49 n/a .000
R0001:C00109-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .328 No_date 6:18
29.35 .371 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00110-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .536 No_date 6:06
29.35 .371 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00111-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .761 No_date 6:19
32.19 .406 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12

R0001:C00112-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 .914 No_date 6:02
25.49 n/a .000 + 1.0 04:Ext-6 6.00 .328 No_date 6:18
29.35 n/a .000 + 1.0 09:Ext-7 6.00 .536 No_date 6:06
29.35 n/a .000 + 1.0 10:Ext-8 12.80 .761 No_date 6:19
32.19 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 2.193 No_date 6:06
28.89 n/a .000

R0001:C00113-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .500 No_date 6:15
34.23 .432 .000
[CN= 76.8: N= 3.00: Tp= .34]

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00114-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 2.193 No_date 6:06
28.89 n/a .000 + 1.0 04:Ext-9 7.00 .500 No_date 6:15
34.23 n/a .000 SUM= 1.0 05:21A 45.80 2.645 No_date 6:08
29.71 n/a .000

R0001:C00115-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.452 No_date 6:06
18.40 .232 .000

Alta Phase 2 (119-2528)

33

PRE_Craigleith_SCS12

[CN= 56.0: N= 3.00: Tp= .20]

#-----|-----

R0001:C00116-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .528 No_date 6:01
30.64 .387 .000
[CN= 72.9: N= 3.00: Tp= .08]

#-----|-----

R0001:C00117-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .480 No_date 6:05
29.35 .371 .000
[CN= 73.0: N= 3.00: Tp= .18]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00118-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.429 No_date 6:01
29.87 n/a .000 + 1.0 02:900mm 11.20 .910 No_date 6:01
30.06 n/a .000 + 1.0 04:Ext-10A 27.90 1.452 No_date 6:06
18.40 n/a .000 + 1.0 03:Ext-11 3.90 .528 No_date 6:01
30.64 n/a .000 + 1.0 06:Ext-12 5.20 .480 No_date 6:05
29.35 n/a .000 SUM= 1.0 05:WET-ST0 61.40 4.586 No_date 6:02

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS12
24.70 n/a .000
R0001:C00119-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 4.586 No_date 6:02
24.70 n/a .000
out <= 1.0 04:22 61.40 .404 No_date 8:05
24.70 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.8547E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00120-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .286 No_date 6:05
18.77 .237 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00121-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .286 No_date 6:05
18.77 n/a .000
+ 1.0 04:22 61.40 .404 No_date 8:05
24.70 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .569 No_date 6:07
24.26 n/a .000
#-----|-----|

#-----|-----50YR SCS (12HR)-----|

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS12

#-----|-----|

R0001:C00122-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
-----|-----|
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 12 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 12.00:PTOT= 88.80]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00123-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .472 No_date 6:03
35.95 .405 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00124-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .573 No_date 6:02
35.95 .405 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00125-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .296 No_date 6:03
35.95 .405 .000

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00126-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 04:INT-4          2.00      .349 No_date    6:00
35.95 .405      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00127-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-1          1.40      .143 No_date    6:10
41.43 .467      .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00128-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD              1.0 05:EXT-1          3.50      .472 No_date    6:03
35.95 n/a      .000
+ 1.0 02:EXT-2          4.10      .573 No_date    6:02
35.95 n/a      .000
+ 1.0 03:EXT-3          2.20      .296 No_date    6:03
35.95 n/a      .000
+ 1.0 04:INT-4          2.00      .349 No_date    6:00
35.95 n/a      .000
+ 1.0 06:INT-1          1.40      .143 No_date    6:10
41.43 n/a      .000
SUM= 1.0 01:825mm      13.20      1.753 No_date    6:01
36.53 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

Alta Phase 2 (119-2528)

```

```

PRE_Craigleith_SCS12
R0001:C00129-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 04:EXT-4          2.60      .350 No_date    6:03
35.95 .405      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00130-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 05:INT-5          .90      .157 No_date    6:00
35.95 .405      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00131-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 06:INT-2          5.80      .495 No_date    6:13
38.36 .432      .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00132-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD          1.0 07:UNC-3          1.90      .296 No_date    6:00
33.14 .373      .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00133-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD              1.0 04:EXT-4          2.60      .350 No_date    6:03
35.95 n/a      .000
+ 1.0 05:INT-5          .90      .157 No_date    6:00
35.95 n/a      .000
+ 1.0 06:INT-2          5.80      .495 No_date    6:13
38.36 n/a      .000
+ 1.0 07:UNC-3          1.90      .296 No_date    6:00
33.14 n/a      .000
SUM= 1.0 02:900mm      11.20      1.120 No_date    6:01

Alta Phase 2 (119-2528)

```

PRE_Craigleith_SCS12

36.72 n/a .000

#-----|-----

#-----|-----OUTLET C-----|

R0001:C00134-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 05:EXT-5 5.20 .753 No_date 6:02

35.95 .405 .000

[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00135-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:INT-6 .70 .122 No_date 6:00

35.95 .405 .000

[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00136-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 07:INT-3 4.90 .358 No_date 6:18

38.66 .435 .000

[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00137-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 08:UNC-4 3.20 .071 No_date 6:14

11.10 .125 .000

[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00138-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 05:EXT-5 5.20 .753 No_date 6:02

35.95 n/a .000

+ 1.0 06:INT-6 .70 .122 No_date 6:00

35.95 n/a .000

+ 1.0 07:INT-3 4.90 .358 No_date 6:18

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS12

38.66 n/a .000

+ 1.0 08:UNC-4 3.20 .071 No_date 6:14

11.10 n/a .000

SUM= 1.0 03:OUTLET C 14.00 1.126 No_date 6:02

31.22 n/a .000

R0001:C00139-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-6 6.00 .406 No_date 6:18

35.95 .405 .000

[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----

R0001:C00140-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 09:Ext-7 6.00 .660 No_date 6:06

35.95 .405 .000

[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00141-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 10:Ext-8 12.80 .932 No_date 6:19

39.12 .441 .000

[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

40

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PRE_Craigleith_SCS12
R0001:C00142-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 03:OUTLET C      14.00    1.126 No_date    6:02
31.22  n/a      .000
      +          1.0 04:Ext-6          6.00    .406 No_date    6:18
35.95  n/a      .000
      +          1.0 09:Ext-7          6.00    .660 No_date    6:06
35.95  n/a      .000
      +          1.0 10:Ext-8          12.80    .932 No_date    6:19
39.12  n/a      .000
      SUM=        1.0 06:NE_DITCH      38.80    2.706 No_date    6:06
35.29  n/a      .000
R0001:C00143-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 04:Ext-9        7.00    .608 No_date    6:14
41.40  .466      .000
      [CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

```

```

#-----|-----

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#-----|-----

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```

R0001:C00144-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 06:NE_DITCH      38.80    2.706 No_date    6:06
35.29  n/a      .000
      +          1.0 04:Ext-9          7.00    .608 No_date    6:14
41.40  n/a      .000
      SUM=        1.0 05:21A          45.80    3.255 No_date    6:08
36.22  n/a      .000
R0001:C00145-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 04:Ext-10A      27.90    1.821 No_date    6:06
22.94  .258      .000
      [CN= 56.0: N= 3.00: Tp= .20]
#-----|-----

```

Alta Phase 2 (119-2528)

41

PRE_Craigleith_SCS12

```

R0001:C00146-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 03:Ext-11       3.90    .641 No_date    6:01
37.29  .420      .000
      [CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

```

```

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

```

```

#-----|-----

```

```

#-----|-----

```

```

R0001:C00148-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 01:825mm        13.20    1.753 No_date    6:01
36.53  n/a      .000
      +          1.0 02:900mm        11.20    1.120 No_date    6:01
36.72  n/a      .000
      +          1.0 04:Ext-10A       27.90    1.821 No_date    6:06
22.94  n/a      .000
      +          1.0 03:Ext-11        3.90    .641 No_date    6:01
37.29  n/a      .000
      +          1.0 06:Ext-12        5.20    .591 No_date    6:05
35.95  n/a      .000
      SUM=        1.0 05:WET-STO      61.40    5.666 No_date    6:02
30.39  n/a      .000
R0001:C00149-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

```

Alta Phase 2 (119-2528)

42

```

PRE_Craigleith_SCS12
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 5.666 No_date 6:02
30.39 n/a .000
out <= 1.0 04:22 61.40 .460 No_date 8:07
30.39 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1091E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00150-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .356 No_date 6:05
23.25 .262 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00151-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .356 No_date 6:05
23.25 n/a .000
+ 1.0 04:22 61.40 .460 No_date 8:07
30.39 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .669 No_date 6:07
29.86 n/a .000
#-----|-----|

#-----|-----100YR SCS (12HR)-----|

#-----|-----|

Alta Phase 2 (119-2528)

```

43

```

PRE_Craigleith_SCS12

R0001:C00152-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 12 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 12.00:PTOT= 98.40]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00153-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .563 No_date 6:03
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00154-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .684 No_date 6:02
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00155-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .354 No_date 6:03
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00156-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

```

44

```

PRE_Craigleith_SCS12
CALIB NASHYD      1.0 04:INT-4      2.00      .413 No_date      6:00
42.86 .436      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00157-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-1      1.40      .169 No_date      6:10
48.88 .497      .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00158-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 05:EXT-1      3.50      .563 No_date      6:03
42.86 n/a      .000
+      1.0 02:EXT-2      4.10      .684 No_date      6:02
42.86 n/a      .000
+      1.0 03:EXT-3      2.20      .354 No_date      6:03
42.86 n/a      .000
+      1.0 04:INT-4      2.00      .413 No_date      6:00
42.86 n/a      .000
+      1.0 06:INT-1      1.40      .169 No_date      6:10
48.88 n/a      .000
SUM=      1.0 01:825mm      13.20      2.092 No_date      6:01
43.49 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00159-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

45

```

PRE_Craigleith_SCS12
CALIB NASHYD      1.0 04:EXT-4      2.60      .418 No_date      6:03
42.86 .436      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00160-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:INT-5      .90      .186 No_date      6:00
42.86 .436      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00161-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-2      5.80      .591 No_date      6:12
45.51 .463      .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00162-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 07:UNC-3      1.90      .353 No_date      6:00
39.64 .403      .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00163-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 04:EXT-4      2.60      .418 No_date      6:03
42.86 n/a      .000
+      1.0 05:INT-5      .90      .186 No_date      6:00
42.86 n/a      .000
+      1.0 06:INT-2      5.80      .591 No_date      6:12
45.51 n/a      .000
+      1.0 07:UNC-3      1.90      .353 No_date      6:00
39.64 n/a      .000
SUM=      1.0 02:900mm      11.20      1.340 No_date      6:01
43.69 n/a      .000
#-----|-----|

Alta Phase 2 (119-2528)

```

46

PRE_Craigleith_SCS12

#-----|-----OUTLET C-----|

R0001:C00164-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .898 No_date 6:02
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00165-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .145 No_date 6:00
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00166-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .427 No_date 6:18
45.84 .466 .000
[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00167-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .088 No_date 6:14
13.73 .139 .000
[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00168-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .898 No_date 6:02
42.86 n/a .000
+ 1.0 06:INT-6 .70 .145 No_date 6:00
42.86 n/a .000
+ 1.0 07:INT-3 4.90 .427 No_date 6:18
45.84 n/a .000
+ 1.0 08:UNC-4 3.20 .088 No_date 6:14
13.73 n/a .000

Alta Phase 2 (119-2528)

47

PRE_Craigleith_SCS12

SUM= 1.0 03:OUTLET C 14.00 1.347 No_date 6:02
37.24 n/a .000
R0001:C00169-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .487 No_date 6:18
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----

R0001:C00170-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .789 No_date 6:05
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00171-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 1.110 No_date 6:18
46.35 .471 .000
[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

R0001:C00172-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 1.347 No_date 6:02

Alta Phase 2 (119-2528)

48

PRE_Craigleith_SCS12
37.24 n/a .000
+ 1.0 04:Ext-6 6.00 .487 No_date 6:18
42.86 n/a .000
+ 1.0 09:Ext-7 6.00 .789 No_date 6:05
42.86 n/a .000
+ 1.0 10:Ext-8 12.80 1.110 No_date 6:18
46.35 n/a .000
SUM= 1.0 06:NE_DITCH 38.80 3.244 No_date 6:06
41.98 n/a .000
R0001:C00173-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .721 No_date 6:14
48.85 .496 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00174-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 3.244 No_date 6:06
41.98 n/a .000
+ 1.0 04:Ext-9 7.00 .721 No_date 6:14
48.85 n/a .000
SUM= 1.0 05:21A 45.80 3.894 No_date 6:08
43.03 n/a .000
R0001:C00175-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 2.219 No_date 6:06
27.81 .283 .000
[CN= 56.0: N= 3.00: Tp= .20]
#-----|-----

R0001:C00176-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528) 49

PRE_Craigleith_SCS12
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .758 No_date 6:01
44.25 .450 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

R0001:C00177-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .707 No_date 6:05
42.86 .436 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00178-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 2.092 No_date 6:01
43.49 n/a .000
+ 1.0 02:900mm 11.20 1.340 No_date 6:01
43.69 n/a .000
+ 1.0 04:Ext-10A 27.90 2.219 No_date 6:06
27.81 n/a .000
+ 1.0 03:Ext-11 3.90 .758 No_date 6:01
44.25 n/a .000
+ 1.0 06:Ext-12 5.20 .707 No_date 6:05
42.86 n/a .000
SUM= 1.0 05:WET-STO 61.40 6.807 No_date 6:02
36.40 n/a .000
R0001:C00179-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 6.807 No_date 6:02
36.40 n/a .000
out <= 1.0 04:22 61.40 .490 No_date 8:11
Alta Phase 2 (119-2528) 50

PRE_Craigleith_SCS12
36.40 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1358E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00180-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .430 No_date 6:05
28.04 .285 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00181-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .430 No_date 6:05
28.04 n/a .000 + 1.0 04:22 61.40 .490 No_date 8:11
36.40 n/a .000 + 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .776 No_date 6:06
35.78 n/a .000
R0001:C00182-----

FINISH

WARNINGS / ERRORS / NOTES

Simulation ended on 2021-06-30 at 12:17:50
=====

Alta Phase 2 (119-2528)

PRE_Craigleith_SCS12

PRE_Craigleith_SCS24

=====

```
SSSSS W W M M H H Y Y M M 000      222    000    11
77777 =====
S      W W W MM MM H H Y Y MM MM O O      2    0    0    11
7 7
SSSSS W W W M M M HHHH Y M M M O O      2    0    0    11
7 Ver4.05.0
S      W W M M H H Y M M M O O      222    0    0    11
7 APR 2017
SSSSS W W M M H H Y M M 000      2    0    0    11
7 =====

7 # 3737016
StormWater Management HYdrologic Model      222    000    11
7 =====
```

```
***** SWMHYMO Ver4.05.0
*****
***** A single event and continuous hydrologic simulation model
*****
***** based on the principles of HYMO and its successors
*****
***** OTTHYMO-83 and OTTHYMO-89.
*****
```

```
***** Distributed by: J.F. Sabourin and Associates Inc.
*****
***** Ottawa, Ontario: (613) 836-3884
*****
***** Gatineau, Quebec: (819) 243-6858
*****
***** E-Mail: swmhymo@jfsa.com
*****
```

+++++

Alta Phase 2 (119-2528)

1

PRE_Craigleith_SCS24

++++++ Licensed user: C.F. Crozier & Associates Inc.

++++++

Collingwood

SERIAL#:3737016

++++++

+++++

++++++ PROGRAM ARRAY DIMENSIONS ++++++

Maximum value for ID numbers : 11

Max. number of rainfall points: 105408

Max. number of flow points : 105408

***** S U M M A R Y O U T P U T *****

* RUN DATE: 2021-06-30 TIME: 12:19:11 RUN COUNTER: 000005

*

* Input file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS24\PRE_Craigl*

* eith_SCS24.Dat

*

* Output file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS24\PRE_Craigl*

* eith_SCS24.out

*

* Summary file: C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SCS24\PRE_Craigl*

* eith_SCS24.sum

*

* User comments:

*

Alta Phase 2 (119-2528)

2

PRE_Craigleith_SCS24

*

1: _____

_____*

2: _____

_____*

3: _____

_____*

#*****

Project Name: [ALTA PHASE II] Project Number: [119-2528]

Date : 2021.06.30

Modified : 2021.06.30

Modeller : [Z. Holland]

Company : C.F. Crozier & Associates Inc.

License # : 3737016

#*****

RUN#:COMMAND#

R0001:C00001-----

Alta Phase 2 (119-2528)

3

PRE_Craigleith_SCS24

START

[TZERO = .00 hrs on 0]

[METOUT= 2 (1=imperial, 2=metric output)]

[NSTORM= 0]

[NRUN = 0001]

#-----|-----

#-----|-----2YR SCS-----

#-----|-----

R0001:C00002-----

MASS STORM

Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase

II\2021.06.30\Craigleith_SC

Comment = 24 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 24.00:PTOT= 45.60]

#-----|-----

#-----|-----PRE-DEVELOPMENT-----

#-----|-----

#-----|-----OUTLET A-----

#-----|-----

R0001:C00003-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

4

```

PRE_Craigleith_SCS24
CALIB NASHYD      1.0 05:EXT-1      3.50      .099 No_date  12:15
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 02:EXT-2      4.10      .121 No_date  12:15
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 03:EXT-3      2.20      .063 No_date  12:15
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:INT-4      2.00      .079 No_date  12:12
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-1      1.40      .034 No_date  12:23
12.35 .271 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
9.78 n/a .000      1.0 05:EXT-1      3.50      .099 No_date  12:15
9.78 n/a .000      +      1.0 02:EXT-2      4.10      .121 No_date  12:15
9.78 n/a .000      +      1.0 03:EXT-3      2.20      .063 No_date  12:15
9.78 n/a .000      +      1.0 04:INT-4      2.00      .079 No_date  12:12

Alta Phase 2 (119-2528)

```

```

PRE_Craigleith_SCS24
9.78 n/a .000      +      1.0 06:INT-1      1.40      .034 No_date  12:23
12.35 n/a .000      SUM=      1.0 01:825mm      13.20      .372 No_date  12:14
10.06 n/a .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:EXT-4      2.60      .074 No_date  12:15
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:INT-5      .90      .036 No_date  12:12
9.78 .215 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-2      5.80      .110 No_date  12:27
10.89 .239 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 07:UNC-3      1.90      .065 No_date  12:12
8.89 .195 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

Alta Phase 2 (119-2528)

```

PRE_Craigleith_SCS24

```
R0001:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 04:EXT-4          2.60      .074 No_date  12:15
9.78  n/a      .000
      +          1.0 05:INT-5          .90      .036 No_date  12:12
9.78  n/a      .000
      +          1.0 06:INT-2          5.80      .110 No_date  12:27
10.89 n/a      .000
      +          1.0 07:UNC-3          1.90      .065 No_date  12:12
8.89  n/a      .000
      SUM=        1.0 02:900mm          11.20      .236 No_date  12:14
10.21 n/a      .000
#-----|-----
```

```
#-----|-----OUTLET C-----|
```

```
R0001:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 05:EXT-5          5.20      .160 No_date  12:14
9.78 .215      .000
      [CN= 73.0: N= 3.00: Tp= .11]
R0001:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 06:INT-6          .70      .028 No_date  12:12
9.78 .215      .000
      [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 07:INT-3          4.90      .081 No_date  12:32
11.07 .243      .000
      [CN= 74.8: N= 3.00: Tp= .39]
R0001:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 08:UNC-4          3.20      .012 No_date  12:28
2.48 .054      .000
      [CN= 34.4: N= 3.00: Tp= .32]
#-----|-----
```

```
#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|
```

Alta Phase 2 (119-2528)

7

PRE_Craigleith_SCS24

```
#-----|-----|
R0001:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD          1.0 05:EXT-5          5.20      .160 No_date  12:14
9.78  n/a      .000
      +          1.0 06:INT-6          .70      .028 No_date  12:12
9.78  n/a      .000
      +          1.0 07:INT-3          4.90      .081 No_date  12:32
11.07 n/a      .000
      +          1.0 08:UNC-4          3.20      .012 No_date  12:28
2.48  n/a      .000
      SUM=        1.0 03:OUTLET C          14.00      .236 No_date  12:14
8.56  n/a      .000
R0001:C00019-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 04:Ext-6          6.00      .085 No_date  12:32
9.78 .215      .000
      [CN= 73.0: N= 3.00: Tp= .39]
#-----|-----|
```

```
R0001:C00020-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 09:Ext-7          6.00      .138 No_date  12:19
9.78 .215      .000
      [CN= 73.0: N= 3.00: Tp= .19]
#-----|-----|
```

```
R0001:C00021-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 10:Ext-8          12.80      .212 No_date  12:32
11.26 .247      .000
      [CN= 75.2: N= 3.00: Tp= .40]
#-----|-----|
```

```
#-----|-----|
```

Alta Phase 2 (119-2528)

8

PRE_Craigleith_SCS24

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----|

#-----|-----|

R0001:C00022-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 03:OUTLET C 14.00 .236 No_date 12:14

8.56 n/a .000 + 1.0 04:Ext-6 6.00 .085 No_date 12:32

9.78 n/a .000 + 1.0 09:Ext-7 6.00 .138 No_date 12:19

9.78 n/a .000 + 1.0 10:Ext-8 12.80 .212 No_date 12:32

11.26 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 .576 No_date 12:21

9.83 n/a .000

R0001:C00023-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-9 7.00 .144 No_date 12:28

12.33 .270 .000

[CN= 76.8: N= 3.00: Tp= .34]

#-----|-----|

#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00024-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 06:NE_DITCH 38.80 .576 No_date 12:21

Alta Phase 2 (119-2528)

9

PRE_Craigleith_SCS24

9.83 n/a .000 + 1.0 04:Ext-9 7.00 .144 No_date 12:28

12.33 n/a .000 SUM= 1.0 05:21A 45.80 .712 No_date 12:24

10.21 n/a .000

R0001:C00025-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-10A 27.90 .354 No_date 12:19

5.76 .126 .000

[CN= 56.0: N= 3.00: Tp= .20]

#-----|-----|

R0001:C00026-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 03:Ext-11 3.90 .150 No_date 12:13

10.73 .235 .000

[CN= 72.9: N= 3.00: Tp= .08]

#-----|-----|

R0001:C00027-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:Ext-12 5.20 .123 No_date 12:18

9.78 .215 .000

[CN= 73.0: N= 3.00: Tp= .18]

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00028-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 01:825mm 13.20 .372 No_date 12:14

10.06 n/a .000

Alta Phase 2 (119-2528)

10

```

PRE_Craigleith_SCS24
+ 1.0 02:900mm 11.20 .236 No_date 12:14
10.21 n/a .000
+ 1.0 04:Ext-10A 27.90 .354 No_date 12:19
5.76 n/a .000
+ 1.0 03:Ext-11 3.90 .150 No_date 12:13
10.73 n/a .000
+ 1.0 06:Ext-12 5.20 .123 No_date 12:18
9.78 n/a .000
SUM= 1.0 05:WET-STO 61.40 1.173 No_date 12:15
8.15 n/a .000
R0001:C00029-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 1.173 No_date 12:15
8.15 n/a .000
out <= 1.0 04:22 61.40 .212 No_date 13:07
8.15 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1675E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00030-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .075 No_date 12:17
6.21 .136 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

R0001:C00031-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .075 No_date 12:17
6.21 n/a .000
+ 1.0 04:22 61.40 .212 No_date 13:07
8.15 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00

Alta Phase 2 (119-2528)

```

11

```

PRE_Craigleith_SCS24
.00 n/a .000
SUM= 1.0 05:22 66.30 .254 No_date 12:20
8.01 n/a .000
#-----|-----

#-----|-----5YR SCS-----|

#-----|-----

R0001:C00032-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 24 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 24.00:PTOT= 62.40]
#-----|-----

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----

#-----|-----OUTLET A-----|

#-----|-----

R0001:C00033-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .197 No_date 12:15
18.76 .301 .000
[CN= 73.0: N= 3.00: Tp= .13]

Alta Phase 2 (119-2528)

```

12

```

PRE_Craigleith_SCS24
R0001:C00034-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 02:EXT-2          4.10      .240 No_date  12:15
18.76 .301      .000
    [CN= 73.0: N= 3.00: Tp= .12]
R0001:C00035-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 03:EXT-3          2.20      .124 No_date  12:15
18.76 .301      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00036-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:INT-4          2.00      .152 No_date  12:12
18.76 .301      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00037-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-1          1.40      .064 No_date  12:23
22.56 .361      .000
    [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00038-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    ADD HYD              1.0 05:EXT-1          3.50      .197 No_date  12:15
18.76 n/a      .000
    +              1.0 02:EXT-2          4.10      .240 No_date  12:15
18.76 n/a      .000
    +              1.0 03:EXT-3          2.20      .124 No_date  12:15
18.76 n/a      .000
    +              1.0 04:INT-4          2.00      .152 No_date  12:12
18.76 n/a      .000
    +              1.0 06:INT-1          1.40      .064 No_date  12:23
22.56 n/a      .000
Alta Phase 2 (119-2528)

```

13

```

PRE_Craigleith_SCS24
SUM=      1.0 01:825mm      13.20      .734 No_date  12:14
19.16 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00039-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 04:EXT-4          2.60      .147 No_date  12:15
18.76 .301      .000
    [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00040-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 05:INT-5          .90      .068 No_date  12:12
18.76 .301      .000
    [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00041-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 06:INT-2          5.80      .216 No_date  12:26
20.41 .327      .000
    [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00042-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
    CALIB NASHYD          1.0 07:UNC-3          1.90      .126 No_date  12:12
17.13 .275      .000
    [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00043-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

14

PRE_Craigleith_SCS24
ADD HYD 1.0 04:EXT-4 2.60 .147 No_date 12:15
18.76 n/a .000
18.76 n/a .000 + 1.0 05:INT-5 .90 .068 No_date 12:12
20.41 n/a .000 + 1.0 06:INT-2 5.80 .216 No_date 12:26
17.13 n/a .000 + 1.0 07:UNC-3 1.90 .126 No_date 12:12
19.34 n/a .000 SUM= 1.0 02:900mm 11.20 .472 No_date 12:13
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00044-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .316 No_date 12:14
18.76 .301 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00045-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .053 No_date 12:12
18.76 .301 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00046-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .158 No_date 12:31
20.65 .331 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00047-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .027 No_date 12:27
5.17 .083 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

Alta Phase 2 (119-2528)

15

PRE_Craigleith_SCS24

R0001:C00048-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .316 No_date 12:14
18.76 n/a .000
18.76 n/a .000 + 1.0 06:INT-6 .70 .053 No_date 12:12
18.76 n/a .000 + 1.0 07:INT-3 4.90 .158 No_date 12:31
20.65 n/a .000 + 1.0 08:UNC-4 3.20 .027 No_date 12:27
5.17 n/a .000 SUM= 1.0 03:OUTLET C 14.00 .474 No_date 12:14
16.32 n/a .000
R0001:C00049-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .174 No_date 12:31
18.76 .301 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00050-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .276 No_date 12:18
18.76 .301 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00051-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .412 No_date 12:31
20.95 .336 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

Alta Phase 2 (119-2528)

16

PRE_Craigleith_SCS24

#-----|-----

#-----|-----

R0001:C00052-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.474	No_date	12:14
16.32 n/a .000						
+	1.0	04:Ext-6	6.00	.174	No_date	12:31
18.76 n/a .000						
+	1.0	09:Ext-7	6.00	.276	No_date	12:18
18.76 n/a .000						
+	1.0	10:Ext-8	12.80	.412	No_date	12:31
20.95 n/a .000						
SUM=	1.0	06:NE_DITCH	38.80	1.156	No_date	12:20
18.60 n/a .000						

R0001:C00053-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.273	No_date	12:27
22.53 .361 .000						
[CN= 76.8: N= 3.00: Tp= .34]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----

#-----|-----

#-----|-----

R0001:C00054-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.156	No_date	12:20
18.60 n/a .000						
+	1.0	04:Ext-9	7.00	.273	No_date	12:27
22.53 n/a .000						

Alta Phase 2 (119-2528)

17

PRE_Craigleith_SCS24

SUM= 1.0 05:21A 45.80 1.409 No_date 12:22

19.20 n/a .000
R0001:C00055-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.723	No_date	12:19
11.39 .182 .000						
[CN= 56.0: N= 3.00: Tp= .20]						

#-----|-----

R0001:C00056-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.281	No_date	12:13
19.91 .319 .000						
[CN= 72.9: N= 3.00: Tp= .08]						

#-----|-----

R0001:C00057-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.247	No_date	12:18
18.76 .301 .000						
[CN= 73.0: N= 3.00: Tp= .18]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----

#-----|-----

#-----|-----

R0001:C00058-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	.734	No_date	12:14
19.16 n/a .000						
+	1.0	02:900mm	11.20	.472	No_date	12:13
19.34 n/a .000						
+	1.0	04:Ext-10A	27.90	.723	No_date	12:19

Alta Phase 2 (119-2528)

18

```

PRE_Craigleith_SCS24
11.39 n/a .000 + 1.0 03:Ext-11 3.90 .281 No_date 12:13
19.91 n/a .000 + 1.0 06:Ext-12 5.20 .247 No_date 12:18
18.76 n/a .000 SUM= 1.0 05:WET-STO 61.40 2.341 No_date 12:14
15.68 n/a .000
R0001:C00059-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 2.341 No_date 12:14
15.68 n/a .000 out <= 1.0 04:22 61.40 .287 No_date 13:21
15.68 n/a .000 overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 {MxStoUsed=.3977E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00060-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .145 No_date 12:17
11.83 .190 .000 [CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00061-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .145 No_date 12:17
11.83 n/a .000 + 1.0 04:22 61.40 .287 No_date 13:21
15.68 n/a .000 + 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000 SUM= 1.0 05:22 66.30 .370 No_date 12:20
15.39 n/a .000
Alta Phase 2 (119-2528)

```

19

```

PRE_Craigleith_SCS24
#-----|-----|

#-----|-----10YR SCS-----|

#-----|-----|

R0001:C00062-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 24 hour SCS II storm mass curve
[SDT= 1.00:SDUR= 24.00:PTOT= 72.00]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00063-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .261 No_date 12:15
24.65 .342 .000 [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00064-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .317 No_date 12:14
Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS24
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00065-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .164 No_date 12:15
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00066-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:INT-4 2.00 .199 No_date 12:12
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00067-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-1 1.40 .083 No_date 12:23
29.09 .404 .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----|

#-----|-----|

#-----|-----|

R0001:C00068-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-1 3.50 .261 No_date 12:15
24.65 n/a .000
+ 1.0 02:EXT-2 4.10 .317 No_date 12:14
24.65 n/a .000
+ 1.0 03:EXT-3 2.20 .164 No_date 12:15
24.65 n/a .000
+ 1.0 04:INT-4 2.00 .199 No_date 12:12
24.65 n/a .000
+ 1.0 06:INT-1 1.40 .083 No_date 12:23
29.09 n/a .000
SUM= 1.0 01:825mm 13.20 .971 No_date 12:14
25.12 n/a .000
#-----|-----|

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS24

#-----|-----OUTLET B-----|

R0001:C00069-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:EXT-4 2.60 .194 No_date 12:15
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00070-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:INT-5 .90 .089 No_date 12:12
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00071-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-2 5.80 .284 No_date 12:25
26.59 .369 .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00072-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:UNC-3 1.90 .166 No_date 12:12
22.58 .314 .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00073-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 04:EXT-4 2.60 .194 No_date 12:15
24.65 n/a .000
+ 1.0 05:INT-5 .90 .089 No_date 12:12

Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS24
24.65 n/a .000 + 1.0 06:INT-2 5.80 .284 No_date 12:25
26.59 n/a .000 + 1.0 07:UNC-3 1.90 .166 No_date 12:12
22.58 n/a .000 SUM= 1.0 02:900mm 11.20 .627 No_date 12:13
25.31 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00074-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .418 No_date 12:14
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00075-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .070 No_date 12:12
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00076-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .208 No_date 12:31
26.85 .373 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00077-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .037 No_date 12:27
7.10 .099 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00078-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
Alta Phase 2 (119-2528) 23

PRE_Craigleith_SCS24
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .418 No_date 12:14
24.65 n/a .000 + 1.0 06:INT-6 .70 .070 No_date 12:12
24.65 n/a .000 + 1.0 07:INT-3 4.90 .208 No_date 12:31
26.85 n/a .000 + 1.0 08:UNC-4 3.20 .037 No_date 12:27
7.10 n/a .000 SUM= 1.0 03:OUTLET C 14.00 .630 No_date 12:14
21.41 n/a .000
R0001:C00079-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .232 No_date 12:31
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00080-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .367 No_date 12:18
24.65 .342 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00081-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .542 No_date 12:31
27.22 .378 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

Alta Phase 2 (119-2528) 24

PRE_Craigleith_SCS24

#-----|-----

R0001:C00082-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	03:OUTLET C	14.00	.630	No_date	12:14
21.41 n/a .000						
+	1.0	04:Ext-6	6.00	.232	No_date	12:31
24.65 n/a .000						
+	1.0	09:Ext-7	6.00	.367	No_date	12:18
24.65 n/a .000						
+	1.0	10:Ext-8	12.80	.542	No_date	12:31
27.22 n/a .000						
SUM=	1.0	06:NE_DITCH	38.80	1.538	No_date	12:19
24.33 n/a .000						

R0001:C00083-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-9	7.00	.356	No_date	12:27
29.06 .404 .000						
[CN= 76.8: N= 3.00: Tp= .34]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00084-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	06:NE_DITCH	38.80	1.538	No_date	12:19
24.33 n/a .000						
+	1.0	04:Ext-9	7.00	.356	No_date	12:27
29.06 n/a .000						
SUM=	1.0	05:21A	45.80	1.866	No_date	12:21
25.05 n/a .000						

R0001:C00085-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS24

mm-R.C.---DWFcms

CALIB NASHYD	1.0	04:Ext-10A	27.90	.978	No_date	12:19
15.24 .212 .000						
[CN= 56.0: N= 3.00: Tp= .20]						

#-----|-----

R0001:C00086-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	03:Ext-11	3.90	.365	No_date	12:13
25.88 .359 .000						
[CN= 72.9: N= 3.00: Tp= .08]						

#-----|-----

R0001:C00087-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD	1.0	06:Ext-12	5.20	.327	No_date	12:18
24.65 .342 .000						
[CN= 73.0: N= 3.00: Tp= .18]						

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00088-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD	1.0	01:825mm	13.20	.971	No_date	12:14
25.12 n/a .000						
+	1.0	02:900mm	11.20	.627	No_date	12:13
25.31 n/a .000						
+	1.0	04:Ext-10A	27.90	.978	No_date	12:19
15.24 n/a .000						
+	1.0	03:Ext-11	3.90	.365	No_date	12:13
25.88 n/a .000						

Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS24
+      1.0 06:Ext-12      5.20      .327 No_date  12:18
24.65 n/a      .000
SUM=    1.0 05:WET-STO    61.40    3.120 No_date  12:14
20.67 n/a      .000
R0001:C00089-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR ->    1.0 05:WET-STO    61.40    3.120 No_date  12:14
20.67 n/a      .000
out <=    1.0 04:22      61.40      .331 No_date  13:27
20.67 n/a      .000
overflow <=    1.0 06:OVF      .00      .000 No_date  0:00
.00 n/a      .000
{MxStoUsed=.5592E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf=    0, TotDurOvf=
0.hrs}
R0001:C00090-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 03:Ext-10B    4.90      .193 No_date  12:17
15.65 .217      .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00091-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 03:Ext-10B    4.90      .193 No_date  12:17
15.65 n/a      .000
+      1.0 04:22      61.40      .331 No_date  13:27
20.67 n/a      .000
+      1.0 06:OVF      .00      .000 No_date  0:00
.00 n/a      .000
SUM=    1.0 05:22      66.30      .445 No_date  12:19
20.30 n/a      .000
#-----|-----|

Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS24
#-----|-----25YR SCS-----|

#-----|-----|

R0001:C00092-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 24 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 24.00:PTOT= 86.40]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00093-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:EXT-1      3.50      .365 No_date  12:15
34.27 .397      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00094-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 02:EXT-2      4.10      .443 No_date  12:14
34.27 .397      .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00095-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS24
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 03:EXT-3          2.20      .230 No_date  12:15
34.27 .397      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00096-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:INT-4          2.00      .275 No_date  12:12
34.27 .397      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00097-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-1          1.40      .114 No_date  12:22
39.61 .458      .000
  [CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00098-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD              1.0 05:EXT-1          3.50      .365 No_date  12:15
34.27 n/a      .000
  + 1.0 02:EXT-2          4.10      .443 No_date  12:14
34.27 n/a      .000
  + 1.0 03:EXT-3          2.20      .230 No_date  12:15
34.27 n/a      .000
  + 1.0 04:INT-4          2.00      .275 No_date  12:12
34.27 n/a      .000
  + 1.0 06:INT-1          1.40      .114 No_date  12:22
39.61 n/a      .000
  SUM= 1.0 01:825mm      13.20      1.357 No_date  12:13
34.83 n/a      .000
#-----|-----|

```

```

PRE_Craigleith_SCS24
#-----|-----OUTLET B-----|

R0001:C00099-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 04:EXT-4          2.60      .271 No_date  12:15
34.27 .397      .000
  [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00100-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 05:INT-5          .90      .124 No_date  12:12
34.27 .397      .000
  [CN= 73.0: N= 3.00: Tp= .05]
R0001:C00101-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 06:INT-2          5.80      .396 No_date  12:25
36.61 .424      .000
  [CN= 74.7: N= 3.00: Tp= .31]
R0001:C00102-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD          1.0 07:UNC-3          1.90      .231 No_date  12:12
31.56 .365      .000
  [CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00103-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD              1.0 04:EXT-4          2.60      .271 No_date  12:15
34.27 n/a      .000
  + 1.0 05:INT-5          .90      .124 No_date  12:12
34.27 n/a      .000
  + 1.0 06:INT-2          5.80      .396 No_date  12:25
36.61 n/a      .000
Alta Phase 2 (119-2528)

```

PRE_Craigleith_SCS24
+ 1.0 07:UNC-3 1.90 .231 No_date 12:12
31.56 n/a .000
SUM= 1.0 02:900mm 11.20 .881 No_date 12:13
35.02 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00104-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .583 No_date 12:14
34.27 .397 .000
[CN= 73.0: N= 3.00: Tp= .11]
R0001:C00105-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .096 No_date 12:12
34.27 .397 .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00106-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .290 No_date 12:30
36.91 .427 .000
[CN= 74.8: N= 3.00: Tp= .39]
R0001:C00107-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .056 No_date 12:27
10.48 .121 .000
[CN= 34.4: N= 3.00: Tp= .32]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00108-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .583 No_date 12:14
34.27 n/a .000
Alta Phase 2 (119-2528)

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PRE_Craigleith_SCS24
+ 1.0 06:INT-6 .70 .096 No_date 12:12
34.27 n/a .000
+ 1.0 07:INT-3 4.90 .290 No_date 12:30
36.91 n/a .000
+ 1.0 08:UNC-4 3.20 .056 No_date 12:27
10.48 n/a .000
SUM= 1.0 03:OUTLET C 14.00 .885 No_date 12:14
29.76 n/a .000
R0001:C00109-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .327 No_date 12:30
34.27 .397 .000
[CN= 73.0: N= 3.00: Tp= .39]
#-----|-----

R0001:C00110-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .515 No_date 12:18
34.27 .397 .000
[CN= 73.0: N= 3.00: Tp= .19]
#-----|-----

R0001:C00111-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 .754 No_date 12:31
37.36 .432 .000
[CN= 75.2: N= 3.00: Tp= .40]
#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

32

PRE_Craigleith_SCS24

R0001:C00112-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 .885 No_date 12:14
29.76 n/a .000 + 1.0 04:Ext-6 6.00 .327 No_date 12:30
34.27 n/a .000 + 1.0 09:Ext-7 6.00 .515 No_date 12:18
34.27 n/a .000 + 1.0 10:Ext-8 12.80 .754 No_date 12:31
37.36 n/a .000 SUM= 1.0 06:NE_DITCH 38.80 2.165 No_date 12:19
33.66 n/a .000

R0001:C00113-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .489 No_date 12:27
39.58 .458 .000
[CN= 76.8: N= 3.00: Tp= .34]

#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00114-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 2.165 No_date 12:19
33.66 n/a .000 + 1.0 04:Ext-9 7.00 .489 No_date 12:27
39.58 n/a .000 SUM= 1.0 05:21A 45.80 2.614 No_date 12:21
34.56 n/a .000

R0001:C00115-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.412 No_date 12:19
21.77 .252 .000

Alta Phase 2 (119-2528)

33

PRE_Craigleith_SCS24

[CN= 56.0: N= 3.00: Tp= .20]

#-----|-----

R0001:C00116-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .501 No_date 12:13
35.59 .412 .000
[CN= 72.9: N= 3.00: Tp= .08]

#-----|-----

R0001:C00117-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .460 No_date 12:17
34.27 .397 .000
[CN= 73.0: N= 3.00: Tp= .18]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00118-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.357 No_date 12:13
34.83 n/a .000 + 1.0 02:900mm 11.20 .881 No_date 12:13
35.02 n/a .000 + 1.0 04:Ext-10A 27.90 1.412 No_date 12:19
21.77 n/a .000 + 1.0 03:Ext-11 3.90 .501 No_date 12:13
35.59 n/a .000 + 1.0 06:Ext-12 5.20 .460 No_date 12:17
34.27 n/a .000 SUM= 1.0 05:WET-ST0 61.40 4.407 No_date 12:14

Alta Phase 2 (119-2528)

34

```

PRE_Craigleith_SCS24
28.93 n/a .000
R0001:C00119-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 4.407 No_date 12:14
28.93 n/a .000
out <= 1.0 04:22 61.40 .400 No_date 13:45
28.93 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.8359E+00 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00120-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .275 No_date 12:17
22.10 .256 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00121-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .275 No_date 12:17
22.10 n/a .000
+ 1.0 04:22 61.40 .400 No_date 13:45
28.93 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .565 No_date 12:19
28.43 n/a .000
#-----|-----|

#-----|-----50YR SCS-----|

Alta Phase 2 (119-2528)

```

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```

PRE_Craigleith_SCS24

#-----|-----|

R0001:C00122-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
-----|-----|
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 24 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 24.00:PTOT= 96.00]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00123-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .439 No_date 12:15
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00124-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .532 No_date 12:14
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00125-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .276 No_date 12:15
41.10 .428 .000

Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS24

[CN= 73.0: N= 3.00: Tp= .13]

R0001:C00126-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:INT-4 2.00 .328 No_date 12:12

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00127-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:INT-1 1.40 .135 No_date 12:22

46.99 .490 .000

[CN= 76.8: N= 3.00: Tp= .27]

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT----

#-----|-----|

#-----|-----|

R0001:C00128-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

ADD HYD 1.0 05:EXT-1 3.50 .439 No_date 12:15

41.10 n/a .000

+ 1.0 02:EXT-2 4.10 .532 No_date 12:14

41.10 n/a .000

+ 1.0 03:EXT-3 2.20 .276 No_date 12:15

41.10 n/a .000

+ 1.0 04:INT-4 2.00 .328 No_date 12:12

41.10 n/a .000

+ 1.0 06:INT-1 1.40 .135 No_date 12:22

46.99 n/a .000

SUM= 1.0 01:825mm 13.20 1.631 No_date 12:13

41.73 n/a .000

#-----|-----|

#-----|-----OUTLET B-----|

Alta Phase 2 (119-2528)

37

PRE_Craigleith_SCS24

R0001:C00129-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:EXT-4 2.60 .326 No_date 12:15

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .13]

R0001:C00130-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 05:INT-5 .90 .148 No_date 12:12

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00131-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:INT-2 5.80 .475 No_date 12:25

43.70 .455 .000

[CN= 74.7: N= 3.00: Tp= .31]

R0001:C00132-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 07:UNC-3 1.90 .278 No_date 12:12

37.99 .396 .000

[CN= 69.7: N= 3.00: Tp= .06]

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00133-----DTmin-ID:NHYD-----AREAh-QPEAKcms-TpeakDate_hh:mm----RV

mm-R.C.---DWFcms

ADD HYD 1.0 04:EXT-4 2.60 .326 No_date 12:15

41.10 n/a .000

+ 1.0 05:INT-5 .90 .148 No_date 12:12

41.10 n/a .000

+ 1.0 06:INT-2 5.80 .475 No_date 12:25

43.70 n/a .000

+ 1.0 07:UNC-3 1.90 .278 No_date 12:12

37.99 n/a .000

SUM= 1.0 02:900mm 11.20 1.061 No_date 12:13

Alta Phase 2 (119-2528)

38

PRE_Craigleith_SCS24

41.92 n/a .000

#-----|-----

#-----|-----OUTLET C-----|

R0001:C00134-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 05:EXT-5 5.20 .700 No_date 12:14

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00135-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 06:INT-6 .70 .115 No_date 12:12

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00136-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 07:INT-3 4.90 .347 No_date 12:30

44.02 .459 .000

[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00137-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 08:UNC-4 3.20 .070 No_date 12:27

13.05 .136 .000

[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00138-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

ADD HYD 1.0 05:EXT-5 5.20 .700 No_date 12:14

41.10 n/a .000

+ 1.0 06:INT-6 .70 .115 No_date 12:12

41.10 n/a .000

+ 1.0 07:INT-3 4.90 .347 No_date 12:30

Alta Phase 2 (119-2528)

39

PRE_Craigleith_SCS24

44.02 n/a .000

+ 1.0 08:UNC-4 3.20 .070 No_date 12:27

13.05 n/a .000

SUM= 1.0 03:OUTLET C 14.00 1.067 No_date 12:14

35.71 n/a .000

R0001:C00139-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 04:Ext-6 6.00 .395 No_date 12:30

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----

R0001:C00140-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 09:Ext-7 6.00 .620 No_date 12:18

41.10 .428 .000

[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00141-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV

mm-R.C.---DWFcms

CALIB NASHYD 1.0 10:Ext-8 12.80 .903 No_date 12:31

44.52 .464 .000

[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

40

PRE_Craigleith_SCS24
R0001:C00142-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 1.067 No_date 12:14
35.71 n/a .000
+ 1.0 04:Ext-6 6.00 .395 No_date 12:30
41.10 n/a .000
+ 1.0 09:Ext-7 6.00 .620 No_date 12:18
41.10 n/a .000
+ 1.0 10:Ext-8 12.80 .903 No_date 12:31
44.52 n/a .000
SUM= 1.0 06:NE_DITCH 38.80 2.611 No_date 12:19
40.28 n/a .000
R0001:C00143-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .583 No_date 12:27
46.96 .489 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00144-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 2.611 No_date 12:19
40.28 n/a .000
+ 1.0 04:Ext-9 7.00 .583 No_date 12:27
46.96 n/a .000
SUM= 1.0 05:21A 45.80 3.145 No_date 12:21
41.30 n/a .000
R0001:C00145-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.732 No_date 12:19
26.57 .277 .000
[CN= 56.0: N= 3.00: Tp= .20]
#-----|-----

Alta Phase 2 (119-2528)

41

PRE_Craigleith_SCS24

R0001:C00146-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .597 No_date 12:13
42.48 .443 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

R0001:C00147-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .554 No_date 12:17
41.10 .428 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00148-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.631 No_date 12:13
41.73 n/a .000
+ 1.0 02:900mm 11.20 1.061 No_date 12:13
41.92 n/a .000
+ 1.0 04:Ext-10A 27.90 1.732 No_date 12:19
26.57 n/a .000
+ 1.0 03:Ext-11 3.90 .597 No_date 12:13
42.48 n/a .000
+ 1.0 06:Ext-12 5.20 .554 No_date 12:17
41.10 n/a .000
SUM= 1.0 05:WET-STO 61.40 5.332 No_date 12:14
34.87 n/a .000
R0001:C00149-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS24
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 5.332 No_date 12:14
34.87 n/a .000
out <= 1.0 04:22 61.40 .450 No_date 14:15
34.87 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1044E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00150-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .335 No_date 12:17
26.82 .279 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----

#-----|-----

R0001:C00151-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .335 No_date 12:17
26.82 n/a .000
+ 1.0 04:22 61.40 .450 No_date 14:15
34.87 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .654 No_date 12:19
34.27 n/a .000
#-----|-----

#-----|-----100YR SCS-----|-----

#-----|-----

Alta Phase 2 (119-2528)

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```

PRE_Craigleith_SCS24

R0001:C00152-----
-----
MASS STORM
Filename = C:\SWMHYMO\Projects\119-2528 Alta Phase
II\2021.06.30\Craigleith_SC
Comment = 24 hour SCS II storm mass curve

[SDT= 1.00:SDUR= 24.00:PTOT= 108.00]
#-----|-----

#-----|-----PRE-DEVELOPMENT-----|-----

#-----|-----

#-----|-----OUTLET A-----|-----

#-----|-----

R0001:C00153-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-1 3.50 .535 No_date 12:15
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00154-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 02:EXT-2 4.10 .649 No_date 12:14
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .12]
R0001:C00155-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:EXT-3 2.20 .336 No_date 12:15
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00156-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)

```

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```

PRE_Craigleith_SCS24
CALIB NASHYD      1.0 04:INT-4      2.00      .397 No_date  12:12
50.04 .463      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00157-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-1      1.40      .163 No_date  12:22
56.57 .524      .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----|

#-----|-----|

R0001:C00158-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
50.04 n/a      .000      1.0 05:EXT-1      3.50      .535 No_date  12:15
+      1.0 02:EXT-2      4.10      .649 No_date  12:14
50.04 n/a      .000
+      1.0 03:EXT-3      2.20      .336 No_date  12:15
50.04 n/a      .000
+      1.0 04:INT-4      2.00      .397 No_date  12:12
50.04 n/a      .000
+      1.0 06:INT-1      1.40      .163 No_date  12:22
56.57 n/a      .000
SUM=      1.0 01:825mm      13.20      1.987 No_date  12:13
50.73 n/a      .000
#-----|-----|

#-----|-----OUTLET B-----|

R0001:C00159-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
Alta Phase 2 (119-2528)

```

45

```

PRE_Craigleith_SCS24
CALIB NASHYD      1.0 04:EXT-4      2.60      .397 No_date  12:15
50.04 .463      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00160-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:INT-5      .90      .179 No_date  12:12
50.04 .463      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00161-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-2      5.80      .578 No_date  12:25
52.92 .490      .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00162-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 07:UNC-3      1.90      .339 No_date  12:12
46.43 .430      .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----|

#-----|-----|

R0001:C00163-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD
50.04 n/a      .000      1.0 04:EXT-4      2.60      .397 No_date  12:15
+      1.0 05:INT-5      .90      .179 No_date  12:12
50.04 n/a      .000
+      1.0 06:INT-2      5.80      .578 No_date  12:25
52.92 n/a      .000
+      1.0 07:UNC-3      1.90      .339 No_date  12:12
46.43 n/a      .000
SUM=      1.0 02:900mm      11.20      1.297 No_date  12:13
50.92 n/a      .000
#-----|-----|

Alta Phase 2 (119-2528)

```

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PRE_Craigleith_SCS24

#-----|-----OUTLET C-----|

R0001:C00164-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .853 No_date 12:14
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00165-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .139 No_date 12:12
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00166-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .422 No_date 12:30
53.27 .493 .000
[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00167-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .089 No_date 12:26
16.58 .154 .000
[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----|

R0001:C00168-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .853 No_date 12:14
50.04 n/a .000
+ 1.0 06:INT-6 .70 .139 No_date 12:12
50.04 n/a .000
+ 1.0 07:INT-3 4.90 .422 No_date 12:30
53.27 n/a .000
+ 1.0 08:UNC-4 3.20 .089 No_date 12:26
16.58 n/a .000

Alta Phase 2 (119-2528)

47

PRE_Craigleith_SCS24

SUM= 1.0 03:OUTLET C 14.00 1.305 No_date 12:14
43.52 n/a .000
R0001:C00169-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .484 No_date 12:30
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----|

R0001:C00170-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .758 No_date 12:18
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----|

R0001:C00171-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 1.097 No_date 12:30
53.83 .498 .000
[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----|

#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----|

#-----|-----|

R0001:C00172-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 1.305 No_date 12:14

Alta Phase 2 (119-2528)

48

PRE_Craigleith_SCS24
43.52 n/a .000
+ 1.0 04:Ext-6 6.00 .484 No_date 12:30
50.04 n/a .000
+ 1.0 09:Ext-7 6.00 .758 No_date 12:18
50.04 n/a .000
+ 1.0 10:Ext-8 12.80 1.097 No_date 12:30
53.83 n/a .000
SUM= 1.0 06:NE_DITCH 38.80 3.195 No_date 12:19
48.94 n/a .000
R0001:C00173-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .705 No_date 12:26
56.54 .523 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----|

#-----|-----|

R0001:C00174-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 3.195 No_date 12:19
48.94 n/a .000
+ 1.0 04:Ext-9 7.00 .705 No_date 12:26
56.54 n/a .000
SUM= 1.0 05:21A 45.80 3.839 No_date 12:20
50.10 n/a .000
R0001:C00175-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 2.161 No_date 12:19
32.99 .305 .000
[CN= 56.0: N= 3.00: Tp= .20]
#-----|-----|

R0001:C00176-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
Alta Phase 2 (119-2528) 49

PRE_Craigleith_SCS24
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .722 No_date 12:13
51.47 .477 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----|

R0001:C00177-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .677 No_date 12:17
50.04 .463 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----|

#-----|-----|

R0001:C00178-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.987 No_date 12:13
50.73 n/a .000
+ 1.0 02:900mm 11.20 1.297 No_date 12:13
50.92 n/a .000
+ 1.0 04:Ext-10A 27.90 2.161 No_date 12:19
32.99 n/a .000
+ 1.0 03:Ext-11 3.90 .722 No_date 12:13
51.47 n/a .000
+ 1.0 06:Ext-12 5.20 .677 No_date 12:17
50.04 n/a .000
SUM= 1.0 05:WET-STO 61.40 6.549 No_date 12:14
42.69 n/a .000
R0001:C00179-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ROUTE RESERVOIR -> 1.0 05:WET-STO 61.40 6.549 No_date 12:14
42.69 n/a .000
out <= 1.0 04:22 61.40 .488 No_date 14:20
Alta Phase 2 (119-2528) 50

PRE_Craigleith_SCS24
42.69 n/a .000
overflow <= 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
{MxStoUsed=.1340E+01 m3, TotOvfVol=.0000E+00 m3, N-Ovf= 0, TotDurOvf=
0.hrs}
R0001:C00180-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-10B 4.90 .415 No_date 12:17
33.14 .307 .000
[CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00181-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:Ext-10B 4.90 .415 No_date 12:17
33.14 n/a .000
+ 1.0 04:22 61.40 .488 No_date 14:20
42.69 n/a .000
+ 1.0 06:OVF .00 .000 No_date 0:00
.00 n/a .000
SUM= 1.0 05:22 66.30 .771 No_date 12:19
41.99 n/a .000
R0001:C00182-----

FINISH

WARNINGS / ERRORS / NOTES

Simulation ended on 2021-06-30 at 12:19:12
=====

Alta Phase 2 (119-2528)

PRE_Craigleith_SCS24

PRE_Timmins

=====

SSSSS W W M M H H Y Y M M 000 222 000 11
77777 =====
S W W W MM MM H H Y Y MM MM O O 2 0 0 11
7 7
SSSSS W W W M M M HHHH Y M M M O O 2 0 0 11
7 Ver4.05.0
S W W M M H H Y M M O O 222 0 0 11
7 APR 2017
SSSSS W W M M H H Y M M 000 2 0 0 11
7 =====
2 0 0 11
7 # 3737016
StormWater Management HYdrologic Model 222 000 11
7 =====

***** SWMHYMO Ver4.05.0

***** A single event and continuous hydrologic simulation model

***** based on the principles of HYMO and its successors

***** OTTHYMO-83 and OTTHYMO-89.

***** Distributed by: J.F. Sabourin and Associates Inc.

***** Ottawa, Ontario: (613) 836-3884

***** Gatineau, Quebec: (819) 243-6858

***** E-Mail: swmhymo@jfsa.com

+++++

Alta Phase 2 (119-2528)

1

PRE_Timmins

++++++ Licensed user: C.F. Crozier & Associates Inc.

+++++

+++++

+++++

Collingwood

SERIAL#:3737016

+++++

***** S U M M A R Y O U T P U T

*

RUN DATE: 2021-06-30

TIME: 12:19:34

RUN COUNTER: 000006

*

* Input file: C:\SWMHYMO\Projects\119-2528 Alta Phase

II\2021.06.30\Timmins\PRE_Timmins.Dat *

* Output file: C:\SWMHYMO\Projects\119-2528 Alta Phase

II\2021.06.30\Timmins\PRE_Timmins.out *

* Summary file: C:\SWMHYMO\Projects\119-2528 Alta Phase

II\2021.06.30\Timmins\PRE_Timmins.sum *

* User comments:

*

*

1: _____

_____*

*

2: _____

_____*

Alta Phase 2 (119-2528)

2

```
PRE_Timmins
*
3:_____
      *
*****
*****

#*****

# Project Name: [ALTA PHASE II]   Project Number: [119-2528]

# Date      : 2021.06.30

# Modified   : 2021.06.30

# Modeller   : [Z. Holland]

# Company    : C.F. Crozier & Associates Inc.

# License #   : 3737016

#*****

RUN#:COMMAND#
R0001:C00001-----
-----
START
[TZERO = .00 hrs on      0]
[METOUT= 2   (1=imperial, 2=metric output)]
[NSTORM= 0 ]
[NRUN  = 0001 ]

Alta Phase 2 (119-2528)
```

```
PRE_Timmins
#-----|-----TIMMINS-----|

#-----|-----|

R0001:C00002-----
-----
      READ STORM
      Filename = tim.stm

      Comment  = Timmins Storm Event

      [SDT=60.00:SDUR= 12.00:PTOT= 193.00]
#-----|-----|

#-----|-----PRE-DEVELOPMENT-----|

#-----|-----|

#-----|-----OUTLET A-----|

#-----|-----|

R0001:C00003-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
      CALIB NASHYD      1.0 05:EXT-1      3.50      .318 No_date      7:00
120.92 .627 .000
      [CN= 73.0: N= 3.00: Tp= .13]
R0001:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
      CALIB NASHYD      1.0 02:EXT-2      4.10      .373 No_date      7:00
120.92 .627 .000
      [CN= 73.0: N= 3.00: Tp= .12]
R0001:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms

Alta Phase 2 (119-2528)
```

```

PRE_Timmins
CALIB NASHYD      1.0 03:EXT-3      2.20      .200 No_date      7:00
120.92 .627      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:INT-4      2.00      .185 No_date      7:00
120.92 .627      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-1      1.40      .131 No_date      7:02
130.75 .677      .000
[CN= 76.8: N= 3.00: Tp= .27]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 800mm CULVERT-----|

#-----|-----

#-----|-----

R0001:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 05:EXT-1      3.50      .318 No_date      7:00
120.92 n/a      .000
+      1.0 02:EXT-2      4.10      .373 No_date      7:00
120.92 n/a      .000
+      1.0 03:EXT-3      2.20      .200 No_date      7:00
120.92 n/a      .000
+      1.0 04:INT-4      2.00      .185 No_date      7:00
120.92 n/a      .000
+      1.0 06:INT-1      1.40      .131 No_date      7:02
130.75 n/a      .000
SUM=      1.0 01:825mm      13.20      1.206 No_date      7:00
121.97 n/a      .000
#-----|-----

#-----|-----OUTLET B-----|

Alta Phase 2 (119-2528)

```

```

PRE_Timmins

R0001:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 04:EXT-4      2.60      .236 No_date      7:00
120.92 .627      .000
[CN= 73.0: N= 3.00: Tp= .13]
R0001:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 05:INT-5      .90      .083 No_date      7:00
120.92 .627      .000
[CN= 73.0: N= 3.00: Tp= .05]
R0001:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 06:INT-2      5.80      .514 No_date      7:04
125.33 .649      .000
[CN= 74.7: N= 3.00: Tp= .31]
R0001:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD      1.0 07:UNC-3      1.90      .166 No_date      7:00
114.55 .594      .000
[CN= 69.7: N= 3.00: Tp= .06]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT |

#-----|-----

#-----|-----

R0001:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD      1.0 04:EXT-4      2.60      .236 No_date      7:00
120.92 n/a      .000
+      1.0 05:INT-5      .90      .083 No_date      7:00
120.92 n/a      .000
+      1.0 06:INT-2      5.80      .514 No_date      7:04
125.33 n/a      .000
+      1.0 07:UNC-3      1.90      .166 No_date      7:00

Alta Phase 2 (119-2528)

```

PRE_Timmins
114.55 n/a .000
SUM= 1.0 02:900mm 11.20 .995 No_date 7:00
122.12 n/a .000
#-----|-----

#-----|-----OUTLET C-----|

R0001:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 05:EXT-5 5.20 .474 No_date 7:00
120.92 .627 .000
[CN= 73.0: N= 3.00: Tp= .11]

R0001:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:INT-6 .70 .065 No_date 7:00
120.92 .627 .000
[CN= 73.0: N= 3.00: Tp= .05]

R0001:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 07:INT-3 4.90 .418 No_date 7:06
125.78 .652 .000
[CN= 74.8: N= 3.00: Tp= .39]

R0001:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 08:UNC-4 3.20 .107 No_date 7:06
50.32 .261 .000
[CN= 34.4: N= 3.00: Tp= .32]

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO OUTLET C-----|

#-----|-----

R0001:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 05:EXT-5 5.20 .474 No_date 7:00
120.92 n/a .000
+ 1.0 06:INT-6 .70 .065 No_date 7:00

Alta Phase 2 (119-2528)

7

PRE_Timmins
120.92 n/a .000
+ 1.0 07:INT-3 4.90 .418 No_date 7:06
125.78 n/a .000
+ 1.0 08:UNC-4 3.20 .107 No_date 7:06
50.32 n/a .000
SUM= 1.0 03:OUTLET C 14.00 1.052 No_date 7:00
106.48 n/a .000
R0001:C00019-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-6 6.00 .494 No_date 7:07
120.92 .627 .000
[CN= 73.0: N= 3.00: Tp= .39]

#-----|-----

R0001:C00020-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 09:Ext-7 6.00 .537 No_date 7:01
120.92 .627 .000
[CN= 73.0: N= 3.00: Tp= .19]

#-----|-----

R0001:C00021-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 10:Ext-8 12.80 1.094 No_date 7:07
126.67 .656 .000
[CN= 75.2: N= 3.00: Tp= .40]

#-----|-----

#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO THE NE DITCH |

#-----|-----

#-----|-----

Alta Phase 2 (119-2528)

8

PRE_Timmins

R0001:C00022-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 03:OUTLET C 14.00 1.052 No_date 7:00
106.48 n/a .000
+ 1.0 04:Ext-6 6.00 .494 No_date 7:07
120.92 n/a .000
+ 1.0 09:Ext-7 6.00 .537 No_date 7:01
120.92 n/a .000
+ 1.0 10:Ext-8 12.80 1.094 No_date 7:07
126.67 n/a .000
SUM= 1.0 06:NE_DITCH 38.80 3.149 No_date 7:01
117.61 n/a .000
R0001:C00023-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-9 7.00 .636 No_date 7:04
130.71 .677 .000
[CN= 76.8: N= 3.00: Tp= .34]
#-----|-----

#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|

#-----|-----

#-----|-----

R0001:C00024-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 06:NE_DITCH 38.80 3.149 No_date 7:01
117.61 n/a .000
+ 1.0 04:Ext-9 7.00 .636 No_date 7:04
130.71 n/a .000
SUM= 1.0 05:21A 45.80 3.781 No_date 7:02
119.61 n/a .000
R0001:C00025-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 04:Ext-10A 27.90 1.802 No_date 7:02
88.48 .458 .000
[CN= 56.0: N= 3.00: Tp= .20]

Alta Phase 2 (119-2528)

9

PRE_Timmins

#-----|-----
R0001:C00026-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 03:Ext-11 3.90 .359 No_date 7:00
122.52 .635 .000
[CN= 72.9: N= 3.00: Tp= .08]
#-----|-----

R0001:C00027-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
CALIB NASHYD 1.0 06:Ext-12 5.20 .467 No_date 7:01
120.92 .627 .000
[CN= 73.0: N= 3.00: Tp= .18]
#-----|-----

#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|

#-----|-----

#-----|-----

R0001:C00028-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RV
mm-R.C.---DWFcms
ADD HYD 1.0 01:825mm 13.20 1.206 No_date 7:00
121.97 n/a .000
+ 1.0 02:900mm 11.20 .995 No_date 7:00
122.12 n/a .000
+ 1.0 04:Ext-10A 27.90 1.802 No_date 7:02
88.48 n/a .000
+ 1.0 03:Ext-11 3.90 .359 No_date 7:00
122.52 n/a .000
+ 1.0 06:Ext-12 5.20 .467 No_date 7:01
120.92 n/a .000
SUM= 1.0 05:WET-STO 61.40 4.822 No_date 7:00
106.73 n/a .000

Alta Phase 2 (119-2528)

10

```
PRE_Timmins
R0001:C00029-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ROUTE RESERVOIR ->   1.0 05:WET-ST0      61.40   4.822 No_date   7:00
106.73 n/a      .000
  out <=   1.0 04:22      55.85   .934 No_date   9:28
106.73 n/a      .000
  overflow <=   1.0 06:OVF      5.55   .955 No_date   9:28
106.73 n/a      .000
  {MxStoUsed=.3689E+01 m3, TotOvfVol=.5921E+00 m3, N-Ovf=    2, TotDurOvf=
  3.hrs}
R0001:C00030-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  CALIB NASHYD      1.0 03:Ext-10B      4.90   .315 No_date   7:01
87.71 .454      .000
  [CN= 54.6: N= 3.00: Tp= .17]
#-----|-----|

#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW -----|

#-----|-----|

#-----|-----|

R0001:C00031-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RV
mm-R.C.---DWFcms
  ADD HYD      1.0 03:Ext-10B      4.90   .315 No_date   7:01
87.71 n/a      .000
  +      1.0 04:22      55.85   .934 No_date   9:28
106.73 n/a      .000
  +      1.0 06:OVF      5.55   .955 No_date   9:28
106.73 n/a      .000
  SUM=      1.0 05:22      66.30   2.015 No_date   9:28
105.32 n/a      .000
R0001:C00032-----
-----
  FINISH
-----
*****
*****
Alta Phase 2 (119-2528)
```

```
PRE_Timmins
  WARNINGS / ERRORS / NOTES
  -----
  Simulation ended on 2021-06-30   at 12:19:35
  =====
  =====
```



```

00001# 02 Metric units
00002# #
00003# # Project Name: [ALTA PHASE-1] Project Number: [119-2528]
00004# # Date: 2021.06.30
00005# # Modified: 2021.06.30
00006# # Modeler: [Z. Holland]
00007# # Company: C.F. Crozier & Associates Inc.
00008# # License #: 3737016
00009# #
00010# START
00011# [ ] <- storm filename, one per line for NStorm time
00012# #
00013# #
00014# #
00015# READ STORM
00016# STORM_FILENAME=[25mm.stm]
00017# #
00018# #
00019# #
00020# #
00021# #
00022# CALIB NASHYO
00023# ID=[2], NHYD=[EXT-1"], DT=[1]min, AREA=[3.5](ha),
00024# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00025# N=[3], TP=[0.23]hrs,
00026# RAINFALL=[ , , , ](mm/hr), END=1
00027# #
00028# CALIB NASHYO
00029# ID=[3], NHYD=[INT-3"], DT=[1]min, AREA=[0.2](ha),
00030# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00031# N=[3], TP=[0.05]hrs,
00032# RAINFALL=[ , , , ](mm/hr), END=1
00033# #
00034# CALIB NASHYO
00035# ID=[4], NHYD=[UNC-1"], DT=[1]min, AREA=[0.8](ha),
00036# DWF=[0](cms), CN/C=[73], IA=[4.52](mm),
00037# N=[3], TP=[0.23]hrs,
00038# RAINFALL=[ , , , ](mm/hr), END=1
00039# #
00040# #
00041# #
00042# #
00043# #
00044# #
00045# CALIB NASHYO
00046# ID=[5], NHYD=[EXT-2"], DT=[1]min, AREA=[4.1](ha),
00047# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00048# N=[3], TP=[0.12]hrs,
00049# RAINFALL=[ , , , ](mm/hr), END=1
00050# #
00051# CALIB NASHYO
00052# ID=[8], NHYD=[EXT-3"], DT=[1]min, AREA=[2.2](ha),
00053# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00054# N=[3], TP=[0.13]hrs,
00055# RAINFALL=[ , , , ](mm/hr), END=1
00056# #
00057# CALIB STANDHYD
00058# ID=[6], NHYD=[INT-2"], DT=[1]min, AREA=[3](ha),
00059# XMP=[0.15], TWP=[0.31], DWF=[0](cms), LOSS=[2],
00060# SCS curve number CWC=[79]
00061# Pervious surfaces: Iaper=[5](mm), SLPP=[2](N),
00062# LOP=[65](m), MWP=[0.25], SCP=[0](min),
00063# Impervious surfaces: IAImp=[2](mm), SLPI=[0.5](N),
00064# LGI=[144](m), MWI=[0.013], SCI=[0](min),
00065# RAINFALL=[ , , , ](mm/hr), END=1
00066# #
00067# CALIB NASHYO
00068# ID=[7], NHYD=[INT-4"], DT=[1]min, AREA=[0.6](ha),
00069# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00070# N=[3], TP=[0.06]hrs,
00071# RAINFALL=[ , , , ](mm/hr), END=1
00072# #
00073# CALIB STANDHYD
00074# ID=[9], NHYD=[INT-1"], DT=[1]min, AREA=[0.6](ha),
00075# XMP=[0.168], TWP=[0.431], DWF=[0](cms), LOSS=[2],
00076# SCS curve number CWC=[79]
00077# Pervious surfaces: Iaper=[5](mm), SLPP=[2](N),
00078# LOP=[65](m), MWP=[0.25], SCP=[0](min),
00079# Impervious surfaces: IAImp=[2](mm), SLPI=[0.5](N),
00080# LGI=[144](m), MWI=[0.013], SCI=[0](min),
00081# RAINFALL=[ , , , ](mm/hr), END=1
00082# #
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00001 *****
00002 *****
00003 SSSSS W W W M M H H Y Y M M 000 222 000 11 77777 =====
00004 S W W W M M M H H Y Y M M M 0 0 2 0 0 11 7 7 Ver4.05.0
00005 SSSSS W W W M M M H H H Y Y M M M 0 0 2 0 0 11 7 7
00006 S W W M M H H Y Y M M 000 222 0 0 11 7 APR 2017
00007 SSSSS W W W M M H H Y Y M M 000 2 0 0 11 7 # 3737016
00008 *****
00009 Stormwater Management Hydrologic Model
00010 *****
00011 *****
00012 ***** SMWYMO Ver4.05.0 *****
00013 ***** A single event and continuous hydrologic simulation model *****
00014 ***** based on the principles of HYMO and its successors *****
00015 ***** OTHYMO-83 and OTHYMO-89 *****
00016 *****
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018 ***** Ottawa, Ontario: (613) 838-3884 *****
00019 ***** Gatineau, Quebec: (819) 243-6858 *****
00020 ***** E-Mail: smwymo@fss.com *****
00021 *****
00022 *****
00023 *****
00024 ***** Licensed user: C.F. Crozier & Associates Inc. *****
00025 ***** Collingwood SERIAL#:3737016 *****
00026 *****
00027 *****
00028 *****
00029 ***** ***** PROGRAM ARRAY DIMENSIONS ***** *****
00030 ***** Maximum value for ID numbers : 15 *****
00031 ***** Max. number of rainfall points : 105408 *****
00032 ***** Max. number of flow points : 105408 *****
00033 *****
00034 *****
00035 ***** SUMMARY OUTPUT *****
00036 *****
00037 ***** RUN DATE: 2022-02-11 TIME: 10:06:18 RUN COUNTER: 000002 *****
00038 *****
00039 ***** Input file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022_01.s *****
00040 ***** Output file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022_01.s *****
00041 ***** Input file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022_01.s *****
00042 ***** Output file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022_01.s *****
00043 ***** User comments: *****
00044 *****
00045 *****
00046 *****
00047 *****
00048 *****
00049 *****
00050 *****
00051 *****
00052 *****
00053 ***** Project Name: [ALTA PHASE-II] Project Number: [19-2528] *****
00054 ***** Date: 2021.06.30 *****
00055 ***** Modified: 2021.06.30 *****
00056 ***** Modeler: [Z. No.101] *****
00057 ***** Company: C.F. Crozier & Associates Inc. *****
00058 ***** License #: 1737016 *****
00059 *****
00060 *****
00061 *****
00062 *****
00063 ***** START *****
00064 ***** [TZERO = 0] hrs on [0] *****
00065 ***** [NETOUT = 2] [1=imperial, 2=metric output] *****
00066 ***** [NETOUT = 0] *****
00067 ***** [NRUN = 0001] *****
00068 ***** *****
00069 ***** *****
00070 ***** *****
00071 ***** *****
00072 ***** *****
00073 ***** READ STORM *****
00074 ***** *****
00075 ***** *****
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00001-2 Metric units
00002-#
00003-# Project Name: [ALTA PHASE-1] Project Number: [119-2528]
00004-# Date: 2022.06.30
00005-# Modified: 2022.01.07
00006-# Modeler: [J. Kerschbaum]
00007-# Company: [C.F. Crozier & Associates Inc.]
00008-# License #: 373010
00009-#
00010-START
00011-#
00012-# [] <- storm filename, one per line for storm time
00013-#
00014-#
00015-READ STORM
00016-#
00017-#
00018-#
00019-#
00020-#
00021-#
00022-CALIB NASHYD
00023-#
00024-#
00025-#
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00030-#
00031-#
00032-CALIB NASHYD
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00375# ImperVIOUS surfaces: IALp=[2](mm), SLPI=[0.5](%),
00376# LGI=[100](m), MNI=[0.013], SCI=[0](min),
00377# RAINFALL=[ , , , ](mm/hr), END=1
00378#
00379# CALIB NASHYO
00380# ID=[4], NHYD=["EXT-3"], DT=[1]min, AREA=[2.0](ha),
00381# DWF=[0](cms), CN/C=[75.3], IA=[0.61](mm),
00382# N=[3], TP=[0.05]hrs,
00383# RAINFALL=[ , , , ](mm/hr), END=1
00384#
00385# THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT
00386#
00387# ADD HYD
00388# IDsum=[2], NHYD=["900mm"], IDs to add=[4,6,7,10]
00389#
00390# CALIB NASHYO
00391# ID=[4], NHYD=["EXT-4"], DT=[1]min, AREA=[2.6](ha),
00392# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00393# N=[3], TP=[0.13]hrs,
00394# RAINFALL=[ , , , ](mm/hr), END=1
00395#
00396# CALIB NASHYO
00397# ID=[5], NHYD=["EXT-5"], DT=[1]min, AREA=[5.2](ha),
00398# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00399# N=[3], TP=[0.13]hrs,
00400# RAINFALL=[ , , , ](mm/hr), END=1
00401#
00402# CALIB NASHYO
00403# ID=[8], NHYD=["INT-5"], DT=[1]min, AREA=[8.1](ha),
00404# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00405# N=[3], TP=[0.05]hrs,
00406# RAINFALL=[ , , , ](mm/hr), END=1
00407#
00408# THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT
00409#
00410# ADD HYD
00411# IDsum=[4], NHYD=["POOLINT"], IDs to add=[5,6,7,9]
00412#
00413# ROUTE CHANNEL
00414# IDout=[5], NHYD=["WC21A"], IDin=[6],
00415# CHLTH=[730](m), CHSLOPE=[5.5](%),
00416# FFSLOPE=[5.5](%),
00417# NSE=[3]
00418# ( SEGROUGH, SEGISTO (m)=[0.07,4.8 - 0.07,19.0 0.07,41] NSEG times
00419# ( DISTANCE (m), ELEVATION (m)=[0,220]
00420# [19,0,215]
00421# [34,217,5]
00422# [41,220]
00423#
00424# CALIB NASHYO
00425# ID=[4], NHYD=["UNC-4"], DT=[1]min, AREA=[3.10](ha),
00426# DWF=[0](cms), CN/C=[36.7], IA=[0.00](mm),
00427# N=[3], TP=[0.30]hrs,
00428# RAINFALL=[ , , , ](mm/hr), END=1
00429#
00430# THE ADD HYD BELOW MODELS FLOW TO WC21A AT SITE
00431#
00432# ADD HYD
00433# IDsum=[3], NHYD=["EXT UNC"], IDs to add=[5,4]
00434#
00435# CALIB NASHYO
00436# ID=[7], NHYD=["EXT-6"], DT=[1]min, AREA=[6.0](ha),
00437# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00438# N=[3], TP=[0.39]hrs,
00439# RAINFALL=[ , , , ](mm/hr), END=1
00440#
00441# CALIB NASHYO
00442# ID=[9], NHYD=["EXT-7"], DT=[1]min, AREA=[6.0](ha),
00443# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00444# N=[3], TP=[0.13]hrs,
00445# RAINFALL=[ , , , ](mm/hr), END=1
00446#
00447# CALIB NASHYO
00448# ID=[10], NHYD=["EXT-8"], DT=[1]min, AREA=[13.1](ha),
00449# DWF=[0](cms), CN/C=[75.2], IA=[0.74](mm),
00450# N=[3], TP=[0.40]hrs,
00451# RAINFALL=[ , , , ](mm/hr), END=1
00452#
00453# THE ADD HYD BELOW MODELS SUBWATERSHED FLOW
00454#
00455# ADD HYD
00456# IDsum=[4], NHYD=["EXT-9"], DT=[1]min, AREA=[7.0](ha),
00457# DWF=[0](cms), CN/C=[76.8], IA=[0.00](mm),
00458# N=[3], TP=[0.34]hrs,
00459# RAINFALL=[ , , , ](mm/hr), END=1
00460#
00461# THE ADD HYD BELOW MODELS Subwatershed 21A Outflow
00462#
00463# ADD HYD
00464# IDsum=[5], NHYD=["21A"], IDs to add=[4,6]
00465#
00466# CALIB NASHYO
00467# ID=[4], NHYD=["EXT-10A"], DT=[1]min, AREA=[27.9](ha),
00468# DWF=[0](cms), CN/C=[56.0], IA=[0.70](mm),
00469# N=[3], TP=[0.20]hrs,
00470# RAINFALL=[ , , , ](mm/hr), END=1
00471#
00472# CALIB NASHYO
00473# ID=[3], NHYD=["EXT-11"], DT=[1]min, AREA=[3.9](ha),
00474# DWF=[0](cms), CN/C=[72.0], IA=[7.96](mm),
00475# N=[3], TP=[0.08]hrs,
00476# RAINFALL=[ , , , ](mm/hr), END=1
00477#
00478# CALIB NASHYO
00479# ID=[6], NHYD=["EXT-12"], DT=[1]min, AREA=[5.2](ha),
00480# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00481# N=[3], TP=[0.18]hrs,
00482# RAINFALL=[ , , , ](mm/hr), END=1
00483#
00484# THE ADD HYD BELOW MODELS FLOW INTO EX STORAGE AREA
00485#
00486# ADD HYD
00487# IDsum=[5], NHYD=["MET-STO"], IDs to add=[1,2,4,3,6]
00488#
00489# ROUTE RESERVOIR
00490# IDout=[4], NHYD=["22"], IDin=[5],
00491# ROT=[1](min),
00492# TABLE of ( OUTFLOW-STORAGE ) values
00493# ( cms ) - ( ha-m )
00494# {
00495# 0.0, 0.0
00496# 0.0102, 0.002
00497# 0.04230, 0.004
00498# 0.0939, 0.006
00499# 0.1206, 0.008
00500# 0.16339, 0.040
00501# 0.2489, 0.262
00502# 0.4601, 1.008
00503# 0.5195, 1.623
00504# 0.579, 3.253
00505# 0.7014, 2.253
00506# 0.8216, 2.953
00507# 0.9345, 3.689
00508# } (max twenty pts)
00509# IDout=[6], NHYD=["OVFC"]
00510#
00511# CALIB NASHYO
00512# ID=[3], NHYD=["EXT-10B"], DT=[1]min, AREA=[4.9](ha),
00513# DWF=[0](cms), CN/C=[54.6], IA=[0.15](mm),
00514# N=[3], TP=[0.17]hrs,
00515# RAINFALL=[ , , , ](mm/hr), END=1
00516#
00517# THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW
00518#
00519# ADD HYD
00520# IDsum=[5], NHYD=["22"], IDs to add=[3,4,6]
00521#
00522#
00523# 10 YEAR KOUH
00524#
00525# READ STORM
00526# STORM_FILENAME=[10yr.stm]
00527#
00528# POST-DEVELOPMENT
00529#
00530# OUTLET A
00531#
00532# CALIB NASHYO
00533# ID=[2], NHYD=["EXT-1"], DT=[1]min, AREA=[3.5](ha),
00534# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00535# N=[3], TP=[0.13]hrs,
00536# RAINFALL=[ , , , ](mm/hr), END=1
00537#
00538# CALIB NASHYO
00539# ID=[3], NHYD=["INT-3"], DT=[1]min, AREA=[0.2](ha),
00540# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00541# N=[3], TP=[0.05]hrs,
00542# RAINFALL=[ , , , ](mm/hr), END=1
00543#
00544# CALIB NASHYO
00545# ID=[4], NHYD=["UNC-1"], DT=[1]min, AREA=[0.8](ha),
00546# DWF=[0](cms), CN/C=[82], IA=[4.52](mm),
00547# N=[3], TP=[0.26]hrs,
00548# RAINFALL=[ , , , ](mm/hr), END=1
00549#
00550# THE ADD HYD BELOW MODELS FLOW INTO THE 825mm CULVERT
00551#
00552# ADD HYD
00553# IDsum=[1], NHYD=["825mm"], IDs to add=[2,3,4]
00554#
00555# OUTLET B
00556#
00557# CALIB NASHYO
00558# ID=[5], NHYD=["EXT-2"], DT=[1]min, AREA=[4.1](ha),
00559# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00560# N=[3], TP=[0.12]hrs,
00561# RAINFALL=[ , , , ](mm/hr), END=1
00562#
00563# CALIB NASHYO
00564# ID=[8], NHYD=["EXT-3"], DT=[1]min, AREA=[2.2](ha),
00565# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00566# N=[3], TP=[0.13]hrs,
00567# RAINFALL=[ , , , ](mm/hr), END=1
00568#
00569# CALIB STANHYDYO
00570# ID=[6], NHYD=["INT-2"], DT=[1](min), AREA=[3](ha),
00571# XIMP=[0.15], TIMP=[0.31], DWF=[0](cms), LOSS=[2],
00572# SCS curve number CN=[78],
00573# Pervious surfaces: IALp=[5](mm), SLPI=[2](%),
00574# LGI=[65](m), MNI=[0.25], SCI=[0](min),
00575# ImperVIOUS surfaces: IALp=[2](mm), SLPI=[0.5](%),
00576# LGI=[14](m), MNI=[0.013], SCI=[0](min),
00577# RAINFALL=[ , , , ](mm/hr), END=1
00578#
00579# CALIB NASHYO
00580# ID=[7], NHYD=["INT-4"], DT=[1]min, AREA=[6.6](ha),
00581# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00582# N=[3], TP=[0.05]hrs,
00583# RAINFALL=[ , , , ](mm/hr), END=1
00584#
00585# CALIB STANHYDYO
00586# ID=[9], NHYD=["INT-1"], DT=[1](min), AREA=[8.00](ha),
00587# XIMP=[0.168], TIMP=[0.431], DWF=[0](cms), LOSS=[2],
00588# SCS curve number CN=[78],
00589# Pervious surfaces: IALp=[5](mm), SLPI=[2](%),
00590# LGI=[65](m), MNI=[0.25], SCI=[0](min),
00591# ImperVIOUS surfaces: IALp=[2](mm), SLPI=[0.5](%),
00592# LGI=[14](m), MNI=[0.013], SCI=[0](min),
00593# RAINFALL=[ , , , ](mm/hr), END=1
00594#
00595# ADD HYD
00596# IDsum=[4], NHYD=["POOLINT"], IDs to add=[5,6,7,9]
00597#
00598# CALIB STANHYDYO
00599# ID=[2], NHYD=["SWMP"], DT=[1](min), AREA=[0.8](ha),
00600# XIMP=[0.5], TIMP=[0.5], DWF=[0](cms), LOSS=[2],
00601# SCS curve number CN=[78],
00602# Pervious surfaces: IALp=[5](mm), SLPI=[2](%),
00603# LGI=[20](m), MNI=[0.25], SCI=[0](min),
00604# ImperVIOUS surfaces: IALp=[2](mm), SLPI=[0.5](%),
00605# LGI=[14](m), MNI=[0.013], SCI=[0](min),
00606# RAINFALL=[ , , , ](mm/hr), END=1
00607#
00608# ADD HYD
00609# IDsum=[3], NHYD=["POOL"], IDs to add=[4,2]
00610#
00611# ROUTE RESERVOIR
00612# IDout=[6], NHYD=["POOL"], IDin=[3],
00613# ROT=[1](min),
00614# TABLE of ( OUTFLOW-STORAGE ) values
00615# ( cms ) - ( ha-m )
00616# {
00617# 0.0, 0.0
00618# 0.0102, 0.002
00619# 0.04230, 0.004
00620# 0.0939, 0.006
00621# 0.1206, 0.008
00622# 0.16339, 0.040
00623# 0.2489, 0.262
00624# 0.4601, 1.008
00625# 0.5195, 1.623
00626# 0.579, 3.253
00627# 0.7014, 2.253
00628# 0.8216, 2.953
00629# 0.9345, 3.689
00630# } (max twenty pts)
00631# IDout=[7], NHYD=["OVFC"]
00632#
00633# CALIB STANHYDYO
00634# ID=[10], NHYD=["UNC-2"], DT=[1](min), AREA=[1.5](ha),
00635# XIMP=[0.075], TIMP=[0.221], DWF=[0](cms), LOSS=[2],
00636# SCS curve number CN=[78],
00637# Pervious surfaces: IALp=[5](mm), SLPI=[2](%),
00638# LGI=[20](m), MNI=[0.25], SCI=[0](min),
00639# ImperVIOUS surfaces: IALp=[2](mm), SLPI=[0.5](%),
00640# LGI=[14](m), MNI=[0.013], SCI=[0](min),
00641# RAINFALL=[ , , , ](mm/hr), END=1
00642#
00643# CALIB NASHYO
00644# ID=[4], NHYD=["UNC-3"], DT=[1]min, AREA=[2.0](ha),
00645# DWF=[0](cms), CN/C=[75.3], IA=[0.61](mm),
00646# N=[3], TP=[0.05]hrs,
00647# RAINFALL=[ , , , ](mm/hr), END=1
00648#
00649# THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT
00650#
00651# ADD HYD
00652# IDsum=[2], NHYD=["900mm"], IDs to add=[4,6,7,10]
00653#
00654# OUTLET C
00655#
00656# CALIB NASHYO
00657# ID=[4], NHYD=["EXT-4"], DT=[1]min, AREA=[2.6](ha),
00658# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00659# N=[3], TP=[0.13]hrs,
00660# RAINFALL=[ , , , ](mm/hr), END=1
00661#
00662# CALIB NASHYO
00663# ID=[5], NHYD=["EXT-5"], DT=[1]min, AREA=[5.2](ha),
00664# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00665# N=[3], TP=[0.13]hrs,
00666# RAINFALL=[ , , , ](mm/hr), END=1
00667#
00668# CALIB NASHYO
00669# ID=[8], NHYD=["INT-5"], DT=[1]min, AREA=[8.1](ha),
00670# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00671# N=[3], TP=[0.05]hrs,
00672# RAINFALL=[ , , , ](mm/hr), END=1
00673#
00674# THE ADD HYD BELOW MODELS FLOW TO WC21A AT SITE
00675#
00676# ADD HYD
00677# IDsum=[3], NHYD=["EXT UNC"], IDs to add=[5,4]
00678#
00679# CALIB NASHYO
00680# ID=[7], NHYD=["EXT-6"], DT=[1]min, AREA=[6.0](ha),
00681# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00682# N=[3], TP=[0.39]hrs,
00683# RAINFALL=[ , , , ](mm/hr), END=1
00684#
00685# CALIB NASHYO
00686# ID=[9], NHYD=["EXT-7"], DT=[1]min, AREA=[6.0](ha),
00687# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00688# N=[3], TP=[0.13]hrs,
00689# RAINFALL=[ , , , ](mm/hr), END=1
00690#
00691# CALIB NASHYO
00692# ID=[10], NHYD=["EXT-8"], DT=[1]min, AREA=[13.1](ha),
00693# DWF=[0](cms), CN/C=[75.2], IA=[0.74](mm),
00694# N=[3], TP=[0.40]hrs,
00695# RAINFALL=[ , , , ](mm/hr), END=1
00696#
00697# THE ADD HYD BELOW MODELS SUBWATERSHED FLOW
00698#
00699# ADD HYD
00700# IDsum=[4], NHYD=["EXT-9"], IDs to add=[7,9,9,10]
00701#
00702# CALIB NASHYO
00703# ID=[4], NHYD=["UNC-4"], DT=[1]min, AREA=[3.10](ha),
00704# DWF=[0](cms), CN/C=[36.7], IA=[0.00](mm),
00705# N=[3], TP=[0.30]hrs,
00706# RAINFALL=[ , , , ](mm/hr), END=1
00707#
00708# THE ADD HYD BELOW MODELS Subwatershed 21A Outflow
00709#
00710# ADD HYD
00711# IDsum=[5], NHYD=["21A"], IDs to add=[4,6]
00712#
00713# CALIB NASHYO
00714# ID=[4], NHYD=["EXT-10A"], DT=[1]min, AREA=[27.9](ha),
00715# DWF=[0](cms), CN/C=[56.0], IA=[0.70](mm),
00716# N=[3], TP=[0.20]hrs,
00717# RAINFALL=[ , , , ](mm/hr), END=1
00718#
00719# CALIB NASHYO
00720# ID=[3], NHYD=["EXT-11"], DT=[1]min, AREA=[3.9](ha),
00721# DWF=[0](cms), CN/C=[72.0], IA=[7.96](mm),
00722# N=[3], TP=[0.08]hrs,
00723# RAINFALL=[ , , , ](mm/hr), END=1
00724#
00725# CALIB NASHYO
00726# ID=[6], NHYD=["EXT-12"], DT=[1]min, AREA=[5.2](ha),
00727# DWF=[0](cms), CN/C=[73], IA=[10](mm),
00728# N=[3], TP=[0.18]hrs,
00729# RAINFALL=[ , , , ](mm/hr), END=1
00730#
00731# THE ADD HYD BELOW MODELS FLOW INTO EX STORAGE AREA
00732#
00733# ADD HYD
00734# IDsum=[5], NHYD=["MET-STO"], IDs to add=[1,2,4,3,6]
00735#
00736# ROUTE RESERVOIR
00737# IDout=[4], NHYD=["22"], IDin=[5],
00738# ROT=[1](min),
00739# TABLE of ( OUTFLOW-STORAGE ) values
00740# ( cms ) - ( ha-m )
00741# {
00742# 0.0, 0.0
00743# 0.0102, 0.002
00744# 0.04230, 0.004
00745# }

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Page 3

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01497> "#-----|-----|
01498> CALIB NASHYD ID=[5], NHYD=["Ext-12"], DT=[1]min, AREA=[5.2](ha),
01499> DMF=[0](cms), CN/C=[73], IAc=[10](mm),
01500> N=[3], TP=[0.19]hrs,
01501> RAINFALL=[ , , , ](mm/hr), END=-1
01502> "#-----|-----|
01503> "#-----|-----|
01504> "#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|
01505> "#-----|-----|
01506> "#-----|-----|
01507> ADD HYD IDsum=[5], NHYD=["MET-STD"], IDs to add=[1,2,4,3,6]
01508> "#-----|-----|
01509> ROUTE RESERVOIR IDout=[4], NHYD=["22"], IDIn=[5],
01510> RDT=[1](min),
01511> TABLE of ( OUTFLOW-STORAGE ) values
01512> (cms) - (ha-m)
01513> [ 0.0 , 0.0 ]
01514> [ 0.0102 , 0.002 ]
01515> [ 0.04220 , 0.004 ]
01516> [ 0.0939 , 0.006 ]
01517> [ 0.1296 , 0.008 ]
01518> [ 0.16330 , 0.045 ]
01519> [ 0.2489 , 0.262 ]
01520> [ 0.3488 , 0.622 ]
01521> [ 0.4601 , 1.088 ]
01522> [ 0.5195 , 1.021 ]
01523> [ 0.579 , 1.925 ]
01524> [ 0.7014 , 2.353 ]
01525> [ 0.8216 , 2.951 ]
01526> [ 0.9345 , 3.089 ]
01527> [ -1 , -1 ] (max twenty pts)
01528> IDovr=[6], NHYDovr=["OVR"]
01529> "#-----|-----|
01530> CALIB NASHYD ID=[3], NHYD=["Ext-108"], DT=[1]min, AREA=[4.9](ha),
01531> DMF=[0](cms), CN/C=[54.6], IAc=[6.15](mm),
01532> N=[3], TP=[0.17]hrs,
01533> RAINFALL=[ , , , ](mm/hr), END=-1
01534> "#-----|-----|
01535> "#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW-----|
01536> "#-----|-----|
01537> "#-----|-----|
01538> "#-----|-----|
01539> ADD HYD IDsum=[5], NHYD=["22"], IDs to add=[3,4,6]
01540> "#-----|-----|
01541>
01542>
01543> FINISH
01544>
01545>

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00001 =====
00002 SSSSS W W W M M H H Y Y M M 000 222 000 11 77777 =====
00003 S S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00004 S S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00005 S S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00006 S S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00007 SSSSS W W W M M H H Y Y M M 000 222 000 11 77777 =====
00008 Stormwater Management Hydrologic Model
00009
00010 ***** SWMHYD Ver4.05.0 *****
00011 ***** A single event and continuous hydrologic simulation model *****
00012 ***** based on the principles of HYDRO and its successors *****
00013 ***** OTHYMO-83 and OTHYMO-89 *****
00014 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00015 ***** Ottawa, Ontario: (613) 886-3884 *****
00016 ***** Gatineau, Quebec: (819) 243-8888 *****
00017 ***** E-Mail: swmhyd@fusa.com *****
00018 *****
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00021 *****
00022 *****
00023 *****
00024 ***** Licensed user: C.F. Crozier & Associates Inc. *****
00025 ***** Collingwood SERIAL#:3737016 *****
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00374 *****
```

Page 1

[illegible]

Page 3

```

00001-2 Metric units
00002-#
00003-# Project Name: [ALTA PHASE-1] Project Number: [119-2528]
00004-# Date: 2021.06.30
00005-# Modified: 2021.06.30
00006-# Modeler: [Z. Holland]
00007-# Company: C.F. Crozier & Associates Inc.
00008-# License #: 3737016
00009-#
00010-START TZERO=[0.0], METOUT=[2], NSTORM=[0], NRUN=[0]
00011-# [ ] <- store filename, one per line for NSTORM time
00012-#
00013-#
00014-# TWS SCS 12 HR
00015-#
00016-
00017-MASS STORM PTOTAL=[39.6](mm), CSDT=[1](min),
00018-CURVE_FILENAME=[\"SCS2H11.mst\"]
00019-
00020-#
00021-#
00022-# POST-DEVELOPMENT
00023-#
00024-# OUTLET A
00025-#
00026-CALIB NASHVO ID=[2], NYHD=[\"EXT-1\"], DT=[1](min), AREA=[0.5](ha),
00027-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00028-RAINFALL=[ , , , ](mm/hr), END=1
00029-#
00031-CALIB NASHVO ID=[3], NYHD=[\"INT-3\"], DT=[1](min), AREA=[0.2](ha),
00032-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00033-N=[3], TP=[0.05]hrs,
00034-RAINFALL=[ , , , ](mm/hr), END=1
00035-#
00036-CALIB NASHVO ID=[4], NYHD=[\"UNC-1\"], DT=[1](min), AREA=[0.8](ha),
00037-DWF=[0](cms), CN/C=[82], IA=[4.52](mm),
00038-N=[3], TP=[0.20]hrs,
00039-RAINFALL=[ , , , ](mm/hr), END=1
00040-#
00041-# THE ADD HYD BELOW MODELS FLOW INTO THE 825mm CULVERT
00042-#
00043-#
00044-ADD HYD Idsum=[1], NYHD=[\"825mm\"], Ids to add=[2,3,4]
00045-#
00046-#
00047-#
00048-#
00049-CALIB NASHVO ID=[5], NYHD=[\"EXT-2\"], DT=[1](min), AREA=[4.1](ha),
00050-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00051-N=[3], TP=[0.12]hrs,
00052-RAINFALL=[ , , , ](mm/hr), END=1
00053-#
00054-CALIB NASHVO ID=[8], NYHD=[\"EXT-3\"], DT=[1](min), AREA=[2.2](ha),
00055-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00056-N=[3], TP=[0.13]hrs,
00057-RAINFALL=[ , , , ](mm/hr), END=1
00058-#
00059-CALIB STANDHYD ID=[5], NYHD=[\"UNC-2\"], DT=[1](min), AREA=[0.8](ha),
00060-XIMP=[0.15], TIMP=[0.31], DWF=[0](cms), LOSS=[2],
00061-SCS curve number CN=[79],
00062-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00063-IAPER=[65](mm), MNP=[0.25], SCP=[0](min),
00064-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00065-LGI=[141](m), MNI=[0.013], SCI=[0](min),
00066-RAINFALL=[ , , , ](mm/hr), END=1
00067-#
00068-CALIB NASHVO ID=[7], NYHD=[\"INT-4\"], DT=[1](min), AREA=[0.6](ha),
00069-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00070-N=[3], TP=[0.05]hrs,
00071-RAINFALL=[ , , , ](mm/hr), END=1
00072-#
00073-CALIB STANDHYD ID=[8], NYHD=[\"EXT-1\"], DT=[1](min), AREA=[0.8](ha),
00074-XIMP=[0.168], TIMP=[0.431], DWF=[0](cms), LOSS=[2],
00075-SCS curve number CN=[79],
00076-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00077-IAPER=[65](mm), MNP=[0.25], SCP=[0](min),
00078-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00079-LGI=[230](m), MNI=[0.013], SCI=[0](min),
00080-RAINFALL=[ , , , ](mm/hr), END=1
00081-#
00082-# THE ADD HYD BELOW MODELS FLOW INTO THE SWM
00083-#
00084-#
00085-#
00086-ADD HYD Idsum=[4], NYHD=[\"POOLINT\"], Ids to add=[5,6,7,9]
00087-#
00088-CALIB STANDHYD ID=[2], NYHD=[\"SWM\"], DT=[1](min), AREA=[0.80](ha),
00089-XIMP=[0.5], TIMP=[0.5], DWF=[0](cms), LOSS=[2],
00090-SCS curve number CN=[79],
00091-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00092-LGP=[65](mm), MNP=[0.25], SCP=[0](min),
00093-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00094-LGI=[68](m), MNI=[0.013], SCI=[0](min),
00095-RAINFALL=[ , , , ](mm/hr), END=1
00096-#
00097-ADD HYD Idsum=[3], NYHD=[\"POOL\"], Ids to add=[4,2]
00098-#
00099-#
00100-ROUTE RESERVOIR Idout=[6], NYHD=[\"POOL\"], IdIn=[3],
00101-ROT=[1](min),
00102-TABLE of (OUTFLOW-STORAGE) values
00103- (cms) - (ha-m)
00104- 0 0 0
00105- 0.012 0.126
00106- 0.024 0.189
00107- 0.042 0.251
00108- 0.117 0.440
00109- 0.215 0.564
00110- 0.292 0.652
00111- 0.376 0.728
00112- 0.514 0.887
00113- 0.849 1.317
00114- 1.089 1.380
00115- 1.105 1.360
00116- -1 -1 (max twenty pts)
00117- Idout=[7], NYHDovr=[\"OVF-1\"]
00118-#
00119-CALIB STANDHYD ID=[10], NYHD=[\"UNC-2\"], DT=[1](min), AREA=[1.5](ha),
00120-XIMP=[0.075], TIMP=[0.221], DWF=[0](cms), LOSS=[2],
00121-SCS curve number CN=[79],
00122-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00123-LGP=[65](mm), MNP=[0.25], SCP=[0](min),
00124-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00125-LGI=[160](m), MNI=[0.013], SCI=[0](min),
00126-RAINFALL=[ , , , ](mm/hr), END=1
00127-#
00128-CALIB NASHVO ID=[4], NYHD=[\"EXT-3\"], DT=[1](min), AREA=[2.2](ha),
00129-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00130-N=[3], TP=[0.05]hrs,
00131-RAINFALL=[ , , , ](mm/hr), END=1
00132-#
00133-# THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT
00134-#
00135-#
00136-ADD HYD Idsum=[2], NYHD=[\"900mm\"], Ids to add=[4,6,7,10]
00137-#
00138-#
00139-# OUTLET C
00140-#
00141-CALIB NASHVO ID=[4], NYHD=[\"EXT-4\"], DT=[1](min), AREA=[2.6](ha),
00142-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00143-N=[3], TP=[0.30]hrs,
00144-RAINFALL=[ , , , ](mm/hr), END=1
00145-#
00146-CALIB NASHVO ID=[5], NYHD=[\"EXT-5\"], DT=[1](min), AREA=[5.2](ha),
00147-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00148-N=[3], TP=[0.11]hrs,
00149-RAINFALL=[ , , , ](mm/hr), END=1
00150-#
00151-CALIB NASHVO ID=[8], NYHD=[\"INT-5\"], DT=[1](min), AREA=[0.1](ha),
00152-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00153-N=[3], TP=[0.05]hrs,
00154-RAINFALL=[ , , , ](mm/hr), END=1
00155-#
00156-# THE ADD HYD MODELS FLOW TO WC23A
00157-#
00158-#
00159-ADD HYD Idsum=[5], NYHD=[\"WC23A\"], Ids to add=[4,5,8,9]
00160-#
00161-ROUTE CHANNEL Idout=[5], NYHD=[\"WC23A\"], IdIn=[6],
00162-ROT=[1](min),
00163-CHLGR=[730](m), CHLSLOPE=[5.5](N),
00164-PSLOPE=[0.51](N),
00165-SECNUM=[1,1], NSEG=[3]
00166- ( SEGMENT, SEGIDIT (m)=[0.07,4.9,0.07,19.0,0.07,41] NSEG times
00167- ( DISTANCE, ELEVATION (m)=[0.228]
00168- 4.8,217.5]
00169- 4.9,215]
00170- 34,217.5]
00171- 41,220]
00172-#
00173-#
00174-CALIB NASHVO ID=[4], NYHD=[\"UNC-4\"], DT=[1](min), AREA=[0.1](ha),
00175-DWF=[0](cms), CN/C=[37.0], IA=[8.97](mm),
00176-N=[3], TP=[0.30]hrs,
00177-RAINFALL=[ , , , ](mm/hr), END=1
00178-#
00179-# THE ADD HYD MODELS FLOW TO WC23A AT SITE
00180-#
00181-#
00182-ADD HYD Idsum=[3], NYHD=[\"EXT_UNC\"], Ids to add=[5,4]
00183-#
00184-CALIB NASHVO ID=[7], NYHD=[\"EXT-6\"], DT=[1](min), AREA=[0.8](ha),
00185-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00186-N=[3], TP=[0.20]hrs,
00187-RAINFALL=[ , , , ](mm/hr), END=1
00188-#

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00189-CALIB NASHVO ID=[9], NYHD=[\"EXT-7\"], DT=[1](min), AREA=[6.8](ha),
00190-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00191-N=[3], TP=[0.19]hrs,
00192-RAINFALL=[ , , , ](mm/hr), END=1
00193-CALIB NASHVO ID=[10], NYHD=[\"EXT-8\"], DT=[1](min), AREA=[13.1](ha),
00194-DWF=[0](cms), CN/C=[73], IA=[8.74](mm),
00195-N=[3], TP=[0.40]hrs,
00196-RAINFALL=[ , , , ](mm/hr), END=1
00197-#
00198-# THE ADD HYD BELOW MODELS SUBWATERSHED FLOW
00199-#
00200-#
00201-ADD HYD Idsum=[4], NYHD=[\"ME-DITCH\"], Ids to add=[7,8,10]
00202-#
00203-CALIB NASHVO ID=[5], NYHD=[\"EXT-9\"], DT=[1](min), AREA=[7.0](ha),
00204-DWF=[0](cms), CN/C=[76.8], IA=[8.06](mm),
00205-N=[3], TP=[0.34]hrs,
00206-RAINFALL=[ , , , ](mm/hr), END=1
00207-#
00208-# THE ADD HYD BELOW MODELS SUBWATERSHED 21A Outflow
00209-#
00210-#
00211-ADD HYD Idsum=[5], NYHD=[\"21A\"], Ids to add=[4,6]
00212-#
00213-CALIB NASHVO ID=[4], NYHD=[\"EXT-10A\"], DT=[1](min), AREA=[27.9](ha),
00214-DWF=[0](cms), CN/C=[56.0], IA=[8.70](mm),
00215-N=[3], TP=[0.20]hrs,
00216-RAINFALL=[ , , , ](mm/hr), END=1
00217-#
00218-CALIB NASHVO ID=[3], NYHD=[\"EXT-11\"], DT=[1](min), AREA=[3.9](ha),
00219-DWF=[0](cms), CN/C=[72.0], IA=[7.90](mm),
00220-N=[3], TP=[0.08]hrs,
00221-RAINFALL=[ , , , ](mm/hr), END=1
00222-#
00223-# THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA
00224-#
00225-#
00226-ADD HYD Idsum=[5], NYHD=[\"EXT-12\"], DT=[1](min), AREA=[5.2](ha),
00227-DWF=[0](cms), CN/C=[82], IA=[10](mm),
00228-N=[3], TP=[0.18]hrs,
00229-RAINFALL=[ , , , ](mm/hr), END=1
00230-#
00231-# THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA
00232-#
00233-#
00234-ADD HYD Idsum=[5], NYHD=[\"NET-STO\"], Ids to add=[1,2,4,3,6]
00235-#
00236-ROUTE RESERVOIR Idout=[4], NYHD=[\"22\"], IdIn=[5],
00237-ROT=[1](min),
00238-TABLE of (OUTFLOW-STORAGE) values
00239- (cms) - (ha-m)
00240- 0 0 0
00241- 0.012 0.002
00242- 0.042 0.004
00243- 0.093 0.006
00244- 0.133 0.008
00245- 0.249 0.008
00246- 0.408 0.022
00247- 0.461 0.088
00248- 0.595 1.022
00249- 0.579 1.925
00250- 0.704 2.253
00251- 0.821 2.951
00252- 0.934 3.689
00253- -1 -1 (max twenty pts)
00254- Idout=[6], NYHDovr=[\"OVF-1\"]
00255-#
00256-CALIB NASHVO ID=[3], NYHD=[\"EXT-10B\"], DT=[1](min), AREA=[4.9](ha),
00257-DWF=[0](cms), CN/C=[54.6], IA=[6.15](mm),
00258-N=[3], TP=[0.27]hrs,
00259-RAINFALL=[ , , , ](mm/hr), END=1
00260-#
00261-# THE ADD HYD BELOW MODELS SUBWATERSHED 22 Outflow
00262-#
00263-#
00264-ADD HYD Idsum=[5], NYHD=[\"22\"], Ids to add=[3,4,5]
00265-#
00266-#
00267-#
00268-#
00269-#
00270-#
00271-#
00272-#
00273-#
00274-MASS STORM PTOTAL=[56.2](mm), CSDT=[1](min),
00275-CURVE_FILENAME=[\"SCS2H11.mst\"]
00276-#
00277-#
00278-# POST-DEVELOPMENT
00279-#
00280-# OUTLET A
00281-#
00282-CALIB NASHVO ID=[2], NYHD=[\"EXT-1\"], DT=[1](min), AREA=[3.5](ha),
00283-DWF=[0](cms), CN/C=[82], IA=[4.52](mm),
00284-N=[3], TP=[0.13]hrs,
00285-RAINFALL=[ , , , ](mm/hr), END=1
00286-#
00287-#
00288-CALIB NASHVO ID=[3], NYHD=[\"EXT-3\"], DT=[1](min), AREA=[0.2](ha),
00289-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00290-N=[3], TP=[0.05]hrs,
00291-RAINFALL=[ , , , ](mm/hr), END=1
00292-#
00293-CALIB NASHVO ID=[4], NYHD=[\"UNC-1\"], DT=[1](min), AREA=[0.8](ha),
00294-DWF=[0](cms), CN/C=[82], IA=[4.52](mm),
00295-N=[3], TP=[0.20]hrs,
00296-RAINFALL=[ , , , ](mm/hr), END=1
00297-#
00298-# THE ADD HYD BELOW MODELS FLOW INTO THE 825mm CULVERT
00299-#
00300-#
00301-ADD HYD Idsum=[1], NYHD=[\"825mm\"], Ids to add=[2,3,4]
00302-#
00303-#
00304-# OUTLET B
00305-#
00306-CALIB NASHVO ID=[5], NYHD=[\"UNC-2\"], DT=[1](min), AREA=[4.1](ha),
00307-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00308-N=[3], TP=[0.12]hrs,
00309-RAINFALL=[ , , , ](mm/hr), END=1
00310-#
00311-CALIB NASHVO ID=[8], NYHD=[\"EXT-3\"], DT=[1](min), AREA=[2.2](ha),
00312-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00313-N=[3], TP=[0.13]hrs,
00314-RAINFALL=[ , , , ](mm/hr), END=1
00315-#
00316-CALIB STANDHYD ID=[6], NYHD=[\"INT-2\"], DT=[1](min), AREA=[3](ha),
00317-XIMP=[0.15], TIMP=[0.31], DWF=[0](cms), LOSS=[2],
00318-SCS curve number CN=[79],
00319-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00320-LGP=[65](mm), MNP=[0.25], SCP=[0](min),
00321-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00322-LGI=[141](m), MNI=[0.013], SCI=[0](min),
00323-RAINFALL=[ , , , ](mm/hr), END=1
00324-#
00325-CALIB NASHVO ID=[7], NYHD=[\"INT-4\"], DT=[1](min), AREA=[0.6](ha),
00326-DWF=[0](cms), CN/C=[73], IA=[10](mm),
00327-N=[3], TP=[0.05]hrs,
00328-RAINFALL=[ , , , ](mm/hr), END=1
00329-#
00330-CALIB STANDHYD ID=[9], NYHD=[\"INT-1\"], DT=[1](min), AREA=[8.60](ha),
00331-XIMP=[0.168], TIMP=[0.431], DWF=[0](cms), LOSS=[2],
00332-SCS curve number CN=[79],
00333-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00334-LGP=[65](mm), MNP=[0.25], SCP=[0](min),
00335-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00336-LGI=[230](m), MNI=[0.013], SCI=[0](min),
00337-RAINFALL=[ , , , ](mm/hr), END=1
00338-#
00339-# THE ADD HYD BELOW MODELS FLOW INTO THE SWM
00340-#
00341-#
00342-#
00343-ADD HYD Idsum=[4], NYHD=[\"POOLINT\"], Ids to add=[5,6,7,9]
00344-#
00345-CALIB STANDHYD ID=[2], NYHD=[\"SWM\"], DT=[1](min), AREA=[0.80](ha),
00346-XIMP=[0.5], TIMP=[0.5], DWF=[0](cms), LOSS=[2],
00347-SCS curve number CN=[79],
00348-Pervious surfaces: IAPER=[5](mm), SLP=[2](N),
00349-LGP=[65](mm), MNP=[0.25], SCP=[0](min),
00350-Imperious surfaces: IALMP=[2](mm), SLP=[0.5](N),
00351-LGI=[68](m), MNI=[0.013], SCI=[0](min),
00352-RAINFALL=[ , , , ](mm/hr), END=1
00353-#
00354-ADD HYD Idsum=[3], NYHD=[\"POOL\"], Ids to add=[4,2]
00355-#
00356-#
00357-ROUTE RESERVOIR Idout=[6], NYHD=[\"POOL\"], IdIn=[3],
00358-ROT=[1](min),
00359-TABLE of (OUTFLOW-STORAGE) values
00360- (cms) - (ha-m)
00361- 0 0 0
00362- 0.012 0.126
00363- 0.024 0.189
00364- 0.042 0.251
00365- 0.117 0.440
00366- 0.215 0.564
00367- 0.292 0.652
00368- 0.376 0.743
00369- 0.514 0.887
00370- 0.704 1.317
00371- 1.089 1.330
00372- 1.105 1.360
00373- -1 -1 (max twenty pts)
00374- Idout=[7], NYHDovr=[\"OVF-1\"]

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01497> "#-----| THE ADD HYD BELOW MODELS Subwatershed 21A Outflow-----|
01498> "#-----|-----|
01499> "#-----|-----|
01500> ADD HYD IDsum=[5], NHYD=["21A"], IDs to add=[4,6]-----|
01501> "#-----|-----|
01502> CALIB NASHYD ID=[4], NHYD=["Ext-10A"], DT=[1]min, AREA=[27.9](ha),-----|
01503> DWF=[0](cms), CN/Cr=[50.0], IAc=[6.70](mm),-----|
01504> N=[3], TP=[0.20]hrs,-----|
01505> RAINFALL=[ , , , ](mm/hr), END=-1-----|
01506> "#-----|-----|
01507> CALIB NASHYD ID=[3], NHYD=["Ext-11"], DT=[1]min, AREA=[3.9](ha),-----|
01508> DWF=[0](cms), CN/Cr=[72.9], IAc=[7.90](mm),-----|
01509> N=[3], TP=[0.00]hrs,-----|
01510> RAINFALL=[ , , , ](mm/hr), END=-1-----|
01511> "#-----|-----|
01512> CALIB NASHYD ID=[0], NHYD=["Ext-12"], DT=[1]min, AREA=[5.2](ha),-----|
01513> DWF=[0](cms), CN/Cr=[75], IAc=[10](mm),-----|
01514> N=[3], TP=[0.10]hrs,-----|
01515> RAINFALL=[ , , , ](mm/hr), END=-1-----|
01516> "#-----|-----|
01517> "#-----|-----|
01518> "#-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|
01519> "#-----|-----|
01520> "#-----|-----|
01521> ADD HYD IDsum=[5], NHYD=["MET-ST0"], IDs to add=[1,2,4,3,6]-----|
01522> "#-----|-----|
01523> ROUTE RESERVOIR IDout=[4], NHYD=["22"], IDIn=[5],-----|
01524> ROT=[1](min),-----|
01525> TABLE of ( OUTFLOW-STORAGE ) values-----|
01526> ( cms ) - ( ha-ft )-----|
01527> [ 0.0 , 0.0 ]-----|
01528> [ 0.0102 , 0.002 ]-----|
01529> [ 0.04230 , 0.004 ]-----|
01530> [ 0.0939 , 0.006 ]-----|
01531> [ 0.1296 , 0.008 ]-----|
01532> [ 0.16330 , 0.045 ]-----|
01533> [ 0.2489 , 0.202 ]-----|
01534> [ 0.3488 , 0.422 ]-----|
01535> [ 0.4601 , 1.088 ]-----|
01536> [ 0.51905 , 1.023 ]-----|
01537> [ 0.579 , 1.925 ]-----|
01538> [ 0.7014 , 2.253 ]-----|
01539> [ 0.8210 , 2.951 ]-----|
01540> [ 0.9345 , 3.689 ]-----|
01541> [ -1 , -1 ] (Max twenty pts)-----|
01542> IDovr=[0], NHYDOvr=["OVr"]-----|
01543> "#-----|-----|
01544> CALIB NASHYD ID=[3], NHYD=["Ext-10B"], DT=[1]min, AREA=[4.9](ha),-----|
01545> DWF=[0](cms), CN/Cr=[54.0], IAc=[6.15](mm),-----|
01546> N=[3], TP=[0.17]hrs,-----|
01547> RAINFALL=[ , , , ](mm/hr), END=-1-----|
01548> "#-----|-----|
01549> "#-----|-----|
01550> "#-----| THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW-----|
01551> "#-----|-----|
01552> "#-----|-----|
01553> ADD HYD IDsum=[5], NHYD=["22"], IDs to add=[3,4,6]-----|
01554> "#-----|-----|
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01559>-----|
01560>-----|
01561>-----|
01562> FINISH-----|
01563>-----|
01564>-----|
01565>-----|

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00001 =====
00002 SSSSS W W M M H H Y Y M M 000 222 000 11 77777 =====
00003 S W W Y Y M M W W M M 0 0 2 0 0 11 7 7 Ver4.05.0
00004 SSSSS W W M M M H H H Y Y M M M 0 0 2 0 0 11 7 7 Ver4.05.0
00005 SSSSS W W M M M H H H Y Y M M M 0 0 2 0 0 11 7 7 Ver4.05.0
00006 S W W M M H H H Y Y M M 000 222 0 0 11 7 APR 2017
00007 SSSSS W W M M M H H Y Y M M 000 2 0 0 11 7 7 3737016
00008 =====
00009 Stormwater Management Hydrologic Model
00010
00011 *****
00012 ***** Summary Ver4.05.0 *****
00013 ***** A single event and continuous hydrologic simulation model *****
00014 ***** Based on the principles of HYMO and its successors *****
00015 ***** OTHYMO-83 and OTHYMO-89 *****
00016 *****
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018 ***** Ottawa, Ontario: (613) 888-3884 *****
00019 ***** Gatineau, Quebec: (819) 243-0858 *****
00020 ***** E-Mail: swmhydro@fusa.com *****
00021 *****
00022 *****
00023 *****
00024 ***** Licensed user: C.F. Crozier & Associates Inc. *****
00025 ***** Collingwood SERIAL#: 3737016 *****
00026 *****
00027 *****
00028 *****
00029 ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** Maximum value for 1D numbers : 15 *****
00031 ***** Max. number of rainfall points: 105400 *****
00032 ***** Max. number of flow points : 105400 *****
00033 *****
00034 *****
00035 ***** SUMMARY OUTPUT *****
00036 *****
00037 ***** RUN DATE: 2022-02-10 TIME: 16:06:47 RUN COUNTER: 000006 *****
00038 *****
00039 ***** Input file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SWMHydro Model\2022.01.1 *****
00040 ***** 9 - regional control\Craigleith\SCS32\POST\Craigleith\SCS32 - regional control\1 *****
00041 ***** 9 - regional control\Craigleith\SCS32\POST\Craigleith\SCS32 - regional control\1 *****
00042 ***** Output file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SWMHydro Model\2022.01.1 *****
00043 ***** 9 - regional control\Craigleith\SCS32\POST\Craigleith\SCS32 - regional control\1 *****
00044 ***** Summary file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SWMHydro Model\2022.01.1 *****
00045 ***** 9 - regional control\Craigleith\SCS32\POST\Craigleith\SCS32 - regional control\1 *****
00046 ***** User comments: *****
00047 ***** 1: *****
00048 ***** 2: *****
00049 ***** 3: *****
00050 ***** *****
00051 *****
00052 *****
00053 *****
00054 ***** Project Name: [ALTA PHASE-II] Project Number: [119-2528] *****
00055 ***** Date: 2021.06.30 *****
00056 ***** Modified: 2021.06.30 *****
00057 ***** Modeler: [Z. No.101] *****
00058 ***** Company: C.F. Crozier & Associates Inc. *****
00059 ***** License #: 3737016 *****
00060 ***** *****
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WARNINGS / ERRORS / NOTES
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Simulation ended on 2022-02-10      at 16:06:49

```


00375#	SCS curve number CN=79,	00602#	CALIB NASHVO	ID=5], NYWD="EXT-2", DT=1]min, AREA=4.1]ha),
00376#	Previous surfaces: IAPer=5](mm), SLP=2](%),	00603#	00603#	DWF=0](cms), CN/C=73], IA=10](mm),
00377#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),	00604#	00604#	N=3], TP=0.12]hrs,
00378#	00378#	00605#	00605#	RAINFALL=, , , ,](mm/hr), END=1
00379#	00379#	00606#	00606#	ID=8], NYWD="EXT-3", DT=1]min, AREA=2.2](ha),
00380#	RAINFALL=, , , ,](mm/hr), END=1	00607#	00607#	DWF=0](cms), CN/C=73], IA=10](mm),
00381#	ID=4], NYWD="EXT-3", DT=1]min, AREA=2.0](ha),	00608#	00608#	N=3], TP=0.13]hrs,
00382#	DWF=0](cms), CN/C=73], IA=10](mm),	00609#	00609#	RAINFALL=, , , ,](mm/hr), END=1
00383#	N=3], TP=0.05]hrs,	00610#	00610#	ID=6], NYWD="EXT-2", DT=1]min, AREA=3](ha),
00384#	RAINFALL=, , , ,](mm/hr), END=1	00611#	00611#	XIMP=0.5], TIMP=0.31], DWF=0](cms), LOSS=2],
00385#	00385#	00612#	00612#	SCS curve number CN=79,
00386#	00386#	00613#	00613#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00387#	00387#	00614#	00614#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00388#	THE ADD HYD BELOW MODELS FLOW INTO THE 900mm CULVERT	00615#	00615#	IAPer=2](mm), SLP=0.5](%),
00389#	00389#	00616#	00616#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00390#	00390#	00617#	00617#	RAINFALL=, , , ,](mm/hr), END=1
00391#	00391#	00618#	00618#	ID=7], NYWD="EXT-4", DT=1]min, AREA=0.6](ha),
00392#	00392#	00619#	00619#	DWF=0](cms), CN/C=73], IA=10](mm),
00393#	00393#	00620#	00620#	N=3], TP=0.05]hrs,
00394#	00394#	00621#	00621#	RAINFALL=, , , ,](mm/hr), END=1
00395#	00395#	00622#	00622#	ID=7], NYWD="EXT-4", DT=1]min, AREA=0.6](ha),
00396#	00396#	00623#	00623#	DWF=0](cms), CN/C=73], IA=10](mm),
00397#	00397#	00624#	00624#	N=3], TP=0.05]hrs,
00398#	00398#	00625#	00625#	RAINFALL=, , , ,](mm/hr), END=1
00399#	00399#	00626#	00626#	ID=9], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00400#	00400#	00627#	00627#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00401#	00401#	00628#	00628#	SCS curve number CN=79,
00402#	00402#	00629#	00629#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00403#	00403#	00630#	00630#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00404#	00404#	00631#	00631#	IAPer=2](mm), SLP=0.5](%),
00405#	00405#	00632#	00632#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00406#	00406#	00633#	00633#	RAINFALL=, , , ,](mm/hr), END=1
00407#	00407#	00634#	00634#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00408#	00408#	00635#	00635#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00409#	00409#	00636#	00636#	SCS curve number CN=79,
00410#	00410#	00637#	00637#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00411#	00411#	00638#	00638#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00412#	00412#	00639#	00639#	IAPer=2](mm), SLP=0.5](%),
00413#	00413#	00640#	00640#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00414#	00414#	00641#	00641#	RAINFALL=, , , ,](mm/hr), END=1
00415#	00415#	00642#	00642#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00416#	00416#	00643#	00643#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00417#	00417#	00644#	00644#	SCS curve number CN=79,
00418#	00418#	00645#	00645#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00419#	00419#	00646#	00646#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00420#	00420#	00647#	00647#	IAPer=2](mm), SLP=0.5](%),
00421#	00421#	00648#	00648#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00422#	00422#	00649#	00649#	RAINFALL=, , , ,](mm/hr), END=1
00423#	00423#	00650#	00650#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00424#	00424#	00651#	00651#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00425#	00425#	00652#	00652#	SCS curve number CN=79,
00426#	00426#	00653#	00653#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00427#	00427#	00654#	00654#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00428#	00428#	00655#	00655#	IAPer=2](mm), SLP=0.5](%),
00429#	00429#	00656#	00656#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00430#	00430#	00657#	00657#	RAINFALL=, , , ,](mm/hr), END=1
00431#	00431#	00658#	00658#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00432#	00432#	00659#	00659#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00433#	00433#	00660#	00660#	SCS curve number CN=79,
00434#	00434#	00661#	00661#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00435#	00435#	00662#	00662#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00436#	00436#	00663#	00663#	IAPer=2](mm), SLP=0.5](%),
00437#	00437#	00664#	00664#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00438#	00438#	00665#	00665#	RAINFALL=, , , ,](mm/hr), END=1
00439#	00439#	00666#	00666#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00440#	00440#	00667#	00667#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00441#	00441#	00668#	00668#	SCS curve number CN=79,
00442#	00442#	00669#	00669#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00443#	00443#	00670#	00670#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00444#	00444#	00671#	00671#	IAPer=2](mm), SLP=0.5](%),
00445#	00445#	00672#	00672#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00446#	00446#	00673#	00673#	RAINFALL=, , , ,](mm/hr), END=1
00447#	00447#	00674#	00674#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
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00449#	00449#	00676#	00676#	SCS curve number CN=79,
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00451#	00451#	00678#	00678#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00452#	00452#	00679#	00679#	IAPer=2](mm), SLP=0.5](%),
00453#	00453#	00680#	00680#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00454#	00454#	00681#	00681#	RAINFALL=, , , ,](mm/hr), END=1
00455#	00455#	00682#	00682#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00456#	00456#	00683#	00683#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00457#	00457#	00684#	00684#	SCS curve number CN=79,
00458#	00458#	00685#	00685#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00459#	00459#	00686#	00686#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00460#	00460#	00687#	00687#	IAPer=2](mm), SLP=0.5](%),
00461#	00461#	00688#	00688#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
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00463#	00463#	00690#	00690#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00464#	00464#	00691#	00691#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00465#	00465#	00692#	00692#	SCS curve number CN=79,
00466#	00466#	00693#	00693#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00467#	00467#	00694#	00694#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00468#	00468#	00695#	00695#	IAPer=2](mm), SLP=0.5](%),
00469#	00469#	00696#	00696#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00470#	00470#	00697#	00697#	RAINFALL=, , , ,](mm/hr), END=1
00471#	00471#	00698#	00698#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00472#	00472#	00699#	00699#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00473#	00473#	00700#	00700#	SCS curve number CN=79,
00474#	00474#	00701#	00701#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00475#	00475#	00702#	00702#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00476#	00476#	00703#	00703#	IAPer=2](mm), SLP=0.5](%),
00477#	00477#	00704#	00704#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00478#	00478#	00705#	00705#	RAINFALL=, , , ,](mm/hr), END=1
00479#	00479#	00706#	00706#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00480#	00480#	00707#	00707#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00481#	00481#	00708#	00708#	SCS curve number CN=79,
00482#	00482#	00709#	00709#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00483#	00483#	00710#	00710#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00484#	00484#	00711#	00711#	IAPer=2](mm), SLP=0.5](%),
00485#	00485#	00712#	00712#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00486#	00486#	00713#	00713#	RAINFALL=, , , ,](mm/hr), END=1
00487#	00487#	00714#	00714#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00488#	00488#	00715#	00715#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00489#	00489#	00716#	00716#	SCS curve number CN=79,
00490#	00490#	00717#	00717#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00491#	00491#	00718#	00718#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00492#	00492#	00719#	00719#	IAPer=2](mm), SLP=0.5](%),
00493#	00493#	00720#	00720#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00494#	00494#	00721#	00721#	RAINFALL=, , , ,](mm/hr), END=1
00495#	00495#	00722#	00722#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00496#	00496#	00723#	00723#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00497#	00497#	00724#	00724#	SCS curve number CN=79,
00498#	00498#	00725#	00725#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00499#	00499#	00726#	00726#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00500#	00500#	00727#	00727#	IAPer=2](mm), SLP=0.5](%),
00501#	00501#	00728#	00728#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00502#	00502#	00729#	00729#	RAINFALL=, , , ,](mm/hr), END=1
00503#	00503#	00730#	00730#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00504#	00504#	00731#	00731#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00505#	00505#	00732#	00732#	SCS curve number CN=79,
00506#	00506#	00733#	00733#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00507#	00507#	00734#	00734#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00508#	00508#	00735#	00735#	IAPer=2](mm), SLP=0.5](%),
00509#	00509#	00736#	00736#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00510#	00510#	00737#	00737#	RAINFALL=, , , ,](mm/hr), END=1
00511#	00511#	00738#	00738#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00512#	00512#	00739#	00739#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00513#	00513#	00740#	00740#	SCS curve number CN=79,
00514#	00514#	00741#	00741#	Previous surfaces: IAPer=5](mm), SLP=2](%),
00515#	00515#	00742#	00742#	Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00516#	00516#	00743#	00743#	IAPer=2](mm), SLP=0.5](%),
00517#	00517#	00744#	00744#	Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00518#	00518#	00745#	00745#	RAINFALL=, , , ,](mm/hr), END=1
00519#	00519#	00746#	00746#	ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00520#	00520#	00747#	00747#	XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00521#	00521#	00748#	00748#	SCS curve number CN=79,
00522#	00522#			Previous surfaces: IAPer=5](mm), SLP=2](%),
00523#	00523#			Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00524#	00524#			IAPer=2](mm), SLP=0.5](%),
00525#	00525#			Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00526#	00526#			RAINFALL=, , , ,](mm/hr), END=1
00527#	00527#			ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00528#	00528#			XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00529#	00529#			SCS curve number CN=79,
00530#	00530#			Previous surfaces: IAPer=5](mm), SLP=2](%),
00531#	00531#			Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00532#	00532#			IAPer=2](mm), SLP=0.5](%),
00533#	00533#			Impervious surfaces: LGI=141](m), MNI=0.013], SCI=0](min),
00534#	00534#			RAINFALL=, , , ,](mm/hr), END=1
00535#	00535#			ID=7], NYWD="EXT-1", DT=1]min, AREA=8.6](ha),
00536#	00536#			XIMP=0.10], TIMP=0.43], DWF=0](cms), LOSS=2],
00537#	00537#			SCS curve number CN=79,
00538#	00538#			Previous surfaces: IAPer=5](mm), SLP=2](%),
00539#	00539#			Impervious surfaces: LGP=65](m), MNP=0.25], SCP=0](min),
00540#	00540#			IAPer=

00749#	ROTF=[1](min),	00936#	(DISTANCE (m), ELEVATION (m))=[9,220]
00750#	TABLE of (OUTFLOW-STORAGE) values	00937#	[0.0, 0.0]
00751#	(cms) - (ha-s)	00938#	[0.0102, 0.002]
00752#	[0.0, 0.0]	00939#	[0.04230, 0.004]
00753#	[0.0102, 0.002]	00940#	[0.0939, 0.006]
00754#	[0.04230, 0.004]	00941#	[0.1286, 0.008]
00755#	[0.0939, 0.006]	00942#	[0.1630, 0.045]
00756#	[0.1286, 0.008]	00943#	[0.2489, 0.262]
00757#	[0.1630, 0.045]	00944#	[0.3488, 0.222]
00758#	[0.2489, 0.262]	00945#	[0.4601, 1.088]
00759#	[0.3488, 0.222]	00946#	[0.5195, 1.623]
00760#	[0.4601, 1.088]	00947#	[0.579, 1.925]
00761#	[0.5195, 1.623]	00948#	[0.7014, 2.253]
00762#	[0.579, 1.925]	00949#	[0.8216, 2.951]
00763#	[0.7014, 2.253]	00950#	[0.9345, 3.689]
00764#	[0.8216, 2.951]	00951#	-1
00765#	[0.9345, 3.689]	00952#	Idovt=[6], NHYDovr=[QVF] (max twenty pts)
00766#	-1	00953#	
00767#		00954#	
00768#		00955#	
00769#		00956#	
00770#		00957#	
00771#		00958#	
00772#		00959#	
00773#		00960#	
00774#		00961#	
00775#		00962#	
00776#		00963#	
00777#		00964#	
00778#		00965#	
00779#		00966#	
00780#		00967#	
00781#		00968#	
00782#		00969#	
00783#		00970#	
00784#		00971#	
00785#		00972#	
00786#		00973#	
00787#		00974#	
00788#		00975#	
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00790#		00977#	
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00798#		00985#	
00799#		00986#	
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00801#		00988#	
00802#		00989#	
00803#		00990#	
00804#		00991#	
00805#		00992#	
00806#		00993#	
00807#		00994#	
00808#		00995#	
00809#		00996#	
00810#		00997#	
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00813#		01000#	
00814#		01001#	
00815#		01002#	
00816#		01003#	
00817#		01004#	
00818#		01005#	
00819#		01006#	
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00821#		01008#	
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00932#		01119#	
00933#		01120#	
00934#		01121#	
00935#		01122#	

Page 3


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01497> N=[3], TP=[0.20]hrs,
01498> RAINFALL=[ , , , ](mm/hr), END=-1
01499> #-----|
01500> CALIB NASHYD ID=[3], NHYD=["Ext-11"], DT=[1]min, AREA=[3.9](ha),
01501> DMF=[0](cms), CN/C=[72.9], IAc=[7.96](mm),
01502> N=[3], TP=[0.00]hrs,
01503> RAINFALL=[ , , , ](mm/hr), END=-1
01504> #-----|
01505> CALIB NASHYD ID=[6], NHYD=["Ext-12"], DT=[1]min, AREA=[5.2](ha),
01506> DMF=[0](cms), CN/C=[73], IAc=[10](mm),
01507> N=[3], TP=[0.20]hrs,
01508> RAINFALL=[ , , , ](mm/hr), END=-1
01509> #-----|
01510> #-----|
01511> #-----| THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA-----|
01512> #-----|
01513> #-----|
01514> ADD HYD IDsum=[5], NHYD=["MET-570"], IDs to add=[1,2,4,3,6]
01515> #-----|
01516> ROUTE RESERVOIR IDout=[4], NHYD=["22"], IDIn=[5],
01517> ROT=[1](RLD),
01518> TABLE of ( OUTFLOW-STORAGE ) values
01519> (cms) - (ha-ft)
01520> [ 0.0 , 0.0 ]
01521> [ 0.0102 , 0.002 ]
01522> [ 0.04230 , 0.004 ]
01523> [ 0.0939 , 0.006 ]
01524> [ 0.1206 , 0.008 ]
01525> [ 0.16330 , 0.045 ]
01526> [ 0.2409 , 0.202 ]
01527> [ 0.3480 , 0.622 ]
01528> [ 0.4601 , 1.088 ]
01529> [ 0.51905 , 1.021 ]
01530> [ 0.579 , 1.925 ]
01531> [ 0.7014 , 2.353 ]
01532> [ 0.8216 , 2.951 ]
01533> [ 0.9345 , 3.089 ]
01534> -1 -1 (Max twenty pts)
01535> IDovf=[6], NHYDovf=["OVF"]
01536> #-----|
01537> CALIB NASHYD ID=[3], NHYD=["Ext-10B"], DT=[1]min, AREA=[4.9](ha),
01538> DMF=[0](cms), CN/C=[54.0], IAc=[6.15](mm),
01539> N=[3], TP=[0.17]hrs,
01540> RAINFALL=[ , , , ](mm/hr), END=-1
01541> #-----|
01542> #-----|
01543> #-----| THE ADD HYD BELOW MODELS SUBWATERHEED 22 OUTFLOW-----|
01544> #-----|
01545> #-----|
01546> ADD HYD IDsum=[5], NHYD=["22"], IDs to add=[3,4,6]
01547> #-----|
01548>
01549>
01550>
01551>
01552> FINISH
01553>
01554>

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00001 =====
00002 SSSSS W W M M H H Y Y M M 000 222 000 11 77777 =====
00003 S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00004 S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 Ver4.05.0
00005 SSSSS W W M M M H H H Y Y M M M 0 0 2 0 0 11 7 7 Ver4.05.0
00006 S W W M M H H Y Y M M 0 0 2 0 0 11 7 7 APR 2017
00007 SSSSS W W M M H H Y Y M M 000 2 0 0 0 11 7 7 3737016
00008
00009 Stormwater Management Hydrologic Model
00010
00011
00012 ***** SMWYMO Ver4.05.0 *****
00013 A single event and continuous hydrologic simulation model
00014 based on the principles of HYMO and its successors
00015 ***** OTHYMO-83 and OTHYMO-89 *****
00016
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018 ***** Ottawa, Ontario: (613) 888-3884 *****
00019 ***** Gatineau, Quebec: (819) 243-0858 *****
00020 ***** E-Mail: swmhydro@fusa.com *****
00021
00022
00023 *****
00024 ***** Licensed user: C.F. Crozier & Associates Inc. *****
00025 ***** Collingwood SERIAL#:3737016 *****
00026 *****
00027 *****
00028 *****
00029 ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** Maximum value for 1D numbers : 15 *****
00031 ***** Max. number of rainfall points: 105400 *****
00032 ***** Max. number of flow points : 105400 *****
00033 *****
00034 *****
00035 ***** SUMMARY OUTPUT *****
00036 *****
00037 ***** RUN DATE: 2022-02-10 TIME: 16:18:12 RUN COUNTER: 000007 *****
00038 *****
00039 ***** Input file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022.01.1 *****
00040 ***** Output file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022.01.1 *****
00041 ***** Input file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022.01.1 *****
00042 ***** Output file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022.01.1 *****
00043 ***** Summary file: J:\100\119 - Tabera Ltd\2528\Design\SWM\Fourth Submission\SMWYMO Model\2022.01.1 *****
00044 ***** User comments: *****
00045 *****
00046 *****
00047 *****
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00051 *****
00052 *****
00053 ***** Project Name: [ALTA PHASE-1] Project Number: [119-2528] *****
00054 ***** Date: 2021.06.30 *****
00055 ***** Modified: 2021.06.30 *****
00056 ***** Modeler: [Z. No.101] *****
00057 ***** License #: 3737016 *****
00058 ***** Company: C.F. Crozier & Associates Inc. *****
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Page 1

00749#	+	1.0 02:900mm	22.00	.344 No.date	12:12	36.16	n/a	.000	00930#	CALIB NASHVO	1.0 09:Ext-7	6.00	.515 No.date	12:18	34.27	397	.000
00750#	+	1.0 04:Ext-10A	27.00	.078 No.date	12:19	15.24	n/a	.000	00931#	[Cn: 73.0: N= 3.00: Tpr: .16]							
00751#	+	1.0 03:Ext-11	3.90	.305 No.date	12:13	25.88	n/a	.000	00938#	-----							
00752#	+	1.0 04:Ext-12	64.30	.290 No.date	12:19	14.65	n/a	.000	00939#	R0001.C00110	-----						
00753#	SUM#	1.0 05:WET-STO	64.30	2.171 No.date	12:15	24.88	n/a	.000	00940#	CALIB NASHVO	1.0 10:Ext-8	13.10	.771 No.date	12:31	37.36	432	.000
00754#	R0001.C00110	-----							00941#	[Cn: 75.2: N= 3.00: Tpr: .40]							
00755#	ROUTE RESERVOIR ->	1.0 05:WET-STO	64.30	2.171 No.date	12:15	24.88	n/a	.000	00942#	-----							
00757#	+	1.0 04:Ext-10A	64.30	.290 No.date	12:19	14.65	n/a	.000	00943#	-----							
00758#	overFlow <=	1.0 06:OVF	.00	.000 No.date	0:00	.00	n/a	.000	00944#	THE ADD HYD BELOW MODELS SUBWATERSHED FLOW							
00759#	(MxStoUsed=.4097E+00	0.00	.000 No.date	0:00	0.00	.00	n/a	.000	00945#	-----							
00760#	0.00	0.00	.000 No.date	0:00	0.00	.00	n/a	.000	00946#	R0001.C00140	-----						
00761#	R0001.C00111	-----							00947#	ADD HYD	1.0 07:Ext-6	6.00	.327 No.date	12:30	34.27	n/a	.000
00762#	CALIB NASHVO	1.0 03:Ext-10B	4.00	.103 No.date	12:17	15.05	n/a	.000	00948#	+	1.0 03:Ext-10C	11.00	.632 No.date	12:21	27.88	n/a	.000
00763#	[Cn: 54.0: N= 3.00: Tpr: .17]								00949#	+	1.0 09:Ext-7	5.00	.515 No.date	12:18	34.27	n/a	.000
00764#	-----								00950#	+	1.0 10:Ext-8	13.10	.771 No.date	12:31	37.36	n/a	.000
00765#	-----								00951#	SUM#	1.0 06:Ext-9	36.10	2.196 No.date	12:22	33.44	n/a	.000
00766#	-----								00952#	-----							
00767#	THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW								00953#	R0001.C00141	-----						
00768#	-----								00954#	CALIB NASHVO	1.0 06:Ext-9	7.00	.489 No.date	12:27	39.58	n/a	.000
00769#	R0001.C00112	-----							00955#	[Cn: 76.0: N= 3.00: Tpr: .34]							
00770#	ADD HYD	1.0 03:Ext-10B	4.90	.193 No.date	12:17	15.05	n/a	.000	00956#	-----							
00771#	+	1.0 04:Ext-10A	64.30	.290 No.date	12:19	14.65	n/a	.000	00957#	-----							
00772#	+	1.0 06:OVF	.00	.000 No.date	0:00	.00	n/a	.000	00958#	THE ADD HYD BELOW MODELS Subwatershed 21A Outflow							
00773#	SUM#	1.0 05:Ext-12	69.20	.412 No.date	12:19	24.22	n/a	.000	00959#	-----							
00774#	-----								00960#	-----							
00775#	-----								00961#	R0001.C00142	-----						
00776#	-----								00962#	ADD HYD	1.0 04:NE DITCH	36.10	2.196 No.date	12:23	33.44	n/a	.000
00777#	R0001.C00113	-----							00963#	SUM#	1.0 06:Ext-9	7.00	.489 No.date	12:27	39.58	n/a	.000
00778#	MASS STORM								00964#	-----							
00779#	File Name = J:\100\119 - Tabera Ltd\2528\Design\SW\Fourth Submission\SWM\HYD M								00965#	-----							
00780#	Comment = 24 hour SCS II storm mass curve								00966#	R0001.C00143	-----						
00781#	[SDT: 1.00:SOURCE: 24.00:PTOT: 06.00]								00967#	CALIB NASHVO	1.0 04:Ext-10A	27.90	1.412 No.date	12:19	21.77	252	.000
00782#	-----								00968#	[Cn: 56.0: N= 3.00: Tpr: .00]							
00783#	-----								00969#	-----							
00784#	-----								00970#	R0001.C00144	-----						
00785#	-----								00971#	CALIB NASHVO	1.0 03:Ext-11	3.90	.501 No.date	12:13	35.59	412	.000
00786#	-----								00972#	[Cn: 72.9: N= 3.00: Tpr: .08]							
00787#	R0001.C00114	-----							00973#	-----							
00788#	CALIB NASHVO	1.0 03:Ext-11	3.90	.501 No.date	12:13	35.59	n/a	.000	00974#	R0001.C00145	-----						
00789#	[Cn: 73.0: N= 3.00: Tpr: .13]								00975#	-----							
00790#	-----								00976#	[Cn: 73.0: N= 3.00: Tpr: .18]							
00791#	R0001.C00115	-----							00977#	-----							
00792#	CALIB NASHVO	1.0 03:Ext-13	2.0	.627 No.date	12:12	34.27	397	.000	00978#	-----							
00793#	[Cn: 73.0: N= 3.00: Tpr: .05]								00979#	-----							
00794#	R0001.C00116	-----							00980#	THE ADD HYD BELOW MODELS FLOW INTO EX. STORAGE AREA							
00795#	CALIB NASHVO	1.0 04:UNC-1	.80	.078 No.date	12:23	48.71	564	.000	00981#	-----							
00796#	[Cn: 82.0: N= 3.00: Tpr: .28]								00982#	R0001.C00146	-----						
00797#	-----								00983#	ADD HYD	1.0 01:825mm	4.50	.451 No.date	12:15	36.83	n/a	.000
00798#	-----								00984#	+	1.0 02:900mm	22.00	.489 No.date	12:12	47.45	n/a	.000
00799#	-----								00985#	+	1.0 04:Ext-11A	27.90	1.412 No.date	12:19	21.77	n/a	.000
00800#	-----								00986#	+	1.0 03:Ext-11	3.90	.501 No.date	12:13	35.59	n/a	.000
00801#	-----								00987#	SUM#	1.0 06:Ext-9	36.10	2.196 No.date	12:23	33.44	n/a	.000
00802#	R0001.C00117	-----							00988#	-----							
00803#	ADD HYD	1.0 02:Ext-11	3.90	.305 No.date	12:15	34.27	n/a	.000	00989#	R0001.C00147	-----						
00804#	+	1.0 03:Ext-13	2.0	.627 No.date	12:12	34.27	n/a	.000	00990#	ROUTE RESERVOIR ->	1.0 05:WET-STO	64.30	3.992 No.date	12:15	33.78	n/a	.000
00805#	+	1.0 04:UNC-1	.80	.078 No.date	12:23	48.71	n/a	.000	00991#	+	1.0 05:WET-STO	64.30	3.992 No.date	12:15	33.78	n/a	.000
00806#	SUM#	1.0 01:825mm	4.50	.451 No.date	12:15	36.83	n/a	.000	00992#	overFlow <=	1.0 06:OVF	.00	.000 No.date	0:00	.00	n/a	.000
00807#	-----								00993#	(MxStoUsed=.5475E+00	0.00	.000 No.date	0:00	0.00	.00	n/a	.000
00808#	-----								00994#	0.00	0.00	.000 No.date	0:00	0.00	.00	n/a	.000
00809#	-----								00995#	0.00	0.00	.000 No.date	0:00	0.00	.00	n/a	.000
00810#	-----								00996#	R0001.C00148	-----						
00811#	R0001.C00118	-----							00997#	CALIB NASHVO	1.0 03:Ext-10B	4.90	.275 No.date	12:17	22.10	250	.000
00812#	CALIB NASHVO	1.0 05:Ext-2	4.10	.443 No.date	12:14	34.27	397	.000	00998#	[Cn: 54.0: N= 3.00: Tpr: .17]							
00813#	[Cn: 73.0: N= 3.00: Tpr: .12]								00999#	-----							
00814#	-----								01000#	-----							
00815#	R0001.C00119	-----							01001#	THE ADD HYD BELOW MODELS SUBWATERSHED 22 OUTFLOW							
00816#	CALIB NASHVO	1.0 08:Ext-3	2.20	.230 No.date	12:15	34.27	397	.000	01002#	-----							
00817#	[Cn: 73.0: N= 3.00: Tpr: .00]								01003#	-----							
00818#	-----								01004#	R0001.C00149	-----						
00819#	R0001.C00120	-----							01005#	ADD HYD	1.0 03:Ext-10B	4.90	.275 No.date	12:17	22.10	n/a	.000
00820#	CALIB STANDHYD	1.0 06:INT-2	3.00	.339 No.date	12:14	54.68	633	.000	01006#	+	1.0 06:OVF	.00	.000 No.date	0:00	.00	n/a	.000
00821#	[XIMP: 16:TIMP: 31]								01007#	SUM#	1.0 05:Ext-2	69.20	.412 No.date	12:19	32.95	n/a	.000
00822#	[LOSS: 2: Cn: 79.0:]								01008#	-----							
00823#	[Previous area: Iaper= 5.00:SLPP=2.00:LGp= 65: MNP= 250:SCP= 0]								01009#	-----							
00824#	[Interpervious area: Ialmp= 2.00:SLPI= 50:LG1= 141: MN1= 013:SC1= 0]								01010#	-----							
00825#	-----								01011#	MASS STORM							
00826#	R0001.C00121	-----							01012#	R0001.C00150	-----						
00827#	CALIB NASHVO	1.0 07:INT-4	.60	.082 No.date	12:12	34.27	397	.000	01013#	File Name = J:\100\119 - Tabera Ltd\2528\Design\SW\Fourth Submission\SWM\HYD M							
00828#	[Cn: 73.0: N= 3.00: Tpr: .05]								01014#	Comment = 24 hour SCS II storm mass curve							
00829#	-----								01015#	[SDT: 1.00:SOURCE: 24.00:PTOT: 06.00]							
00830#	R0001.C00122	-----							01016#	-----							
00831#	CALIB STANDHYD	1.0 06:INT-1	9.00	.954 No.date	12:16	55.56	643	.000	01017#	-----							
00832#	[XIMP: 16:TIMP: 34]								01018#	-----							
00833#	[LOSS: 2: Cn: 79.0:]								01019#	-----							
00834#	[Previous area: Iaper= 5.00:SLPP=2.00:LGp= 65: MNP= 250:SCP= 0]								01020#	-----							
00835#	[Interpervious area: Ialmp= 2.00:SLPI= 50:LG1= 141: MN1= 013:SC1= 0]								01021#	-----							
00836#	-----								01022#	R0001.C00151	-----						
00837#	-----								01023#	CALIB NASHVO	1.0 02:Ext-11	3.90	.439 No.date	12:15	41.10	428	.000
00838#	-----								01024#	[Cn: 73.0: N= 3.00: Tpr: .13]							
00839#	-----								01025#	-----							
00840#	R0001.C00123	-----							01026#	R0001.C00152	-----						
00841#	ADD HYD	1.0 05:Ext-2	4.10	.443 No.date	12:14	34.27	n/a	.000	01027#	-----							

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APPENDIX E

Stormwater Management Facility Calculations



Project No: 119-2528
Project: Alta Phase II
File: Water Quality
Design by: J. Kerschbaumer
Checked by: G. Cooper
Date: 2022-02-11

Post-Development Scenario Water Quality Requirements

Areas Contributing	Area (ha)	% Imp	25mm RV (mm)	25mm RV (m ³)
POST-1	19.70	21	6.55	1290
Total	19.70	21		1290
MOE Total WQ Volume (m ³ /ha)				105
MOE ED Volume (m ³ /ha)				40
MOE ED Volume (m ³)				788
MOE PP Volume (m ³ /ha)				65
MOE PP Volume (m ³)				1281
Pond Required ED Volume (m ³)				1290
Pond Required PP Volume (m ³)				1281
Pond Required AS Volume (m ³)				5800



Project No: 119-2528
Project: Alta Phase II
File: Extended Detention
Design by: J. Kerschbaumer
Checked by: G. Cooper
Date: 2022-02-11

Extended Detention Specifications

(Per MECP)

Extended Detention Volume (Area x runoff from 25mm event)	1290
t (drawdown time - seconds, <i>hours in italics</i>)	24.0
Ao (cross section area of orifice - sqm)	0.0113
h (maximum water elevation above orifice for extended detention- m)	0.20
C (discharge coefficient)	0.64
Ap (average surface area for extended detention - sqm)	3071

$$t = 2 * A_p * (h^{0.5}) / (C * A_o * (g * 2)^{0.5})$$

Ao = 0.011 sqm d = 120 mm

Extended Detention Orifice Diameter (as designed) d = 120 mm

ACTUAL DRAWDOWN TIME

* Neglecting tailwater conditions*

Extended Detention Volume Used	4400
d (orifice diameter, mm)	120
h (maximum head acting on orifice for extended detention, m)	0.20
Ao (cross section area of orifice, m ²)	0.0113
C (discharge coefficient)	0.64
Ap (average surface area for extended detention, m ²)	3071

$$t = 2 * A_p * (h^{0.5}) / (C * A_o * (g * 2)^{0.5})$$

t (hours) 24

Storage - Outflow Calculations

Outlet Structure		Main Cell Spillway	
E.D. Orifice Diameter:	0.12 m	Emergency Spill Elev.	218.65 m
E.D. Orifice Invert Elevation:	216.05 m	Emerg Spill Bot. Width	0.2 m
Extended Detention Depth:	0.20	Trap. Side Slopes	2 :1
Extended Detention Volume:	4400.00		
Extended Detention Surface Area	3071.43		
Rect weir length	0.14 m		
Rect weir invert	216.25 m		

	Pond Dimensions			Outlet Structure			Cell Spillway		Total Discharge	Storage
	Elev.	Depth	Area	ED Orifice Discharge	V-notch Discharge	Rect. Weir Discharge	Emerg. Weir Ave. Width	Emerg. Weir Discharge		
	(m)	(m)	(sqm)	(cu.m/s)	(cu.m/s)	(cu.m/s)	(m)	(cu.m/s)	(cu.m/s)	(ha-m)
Permanent Pool	216.05	0.00	2700	0.000	0.000	0.000	0.000	0.000	0.000	0.000
	216.15	0.10	2886	0.006	0.000	0.000	0.000	0.000	0.006	0.063
Extended Detention Weir	216.25	0.20	3071	0.012	0.000	0.000	0.000	0.000	0.012	0.129
	216.35	0.30	3257	0.016	0.000	0.008	0.000	0.000	0.024	0.189
	216.45	0.40	3443	0.019	0.000	0.023	0.000	0.000	0.042	0.251
	216.55	0.50	3629	0.021	0.000	0.042	0.000	0.000	0.064	0.314
	216.65	0.60	3814	0.024	0.000	0.065	0.000	0.000	0.089	0.377
	216.75	0.70	4000	0.026	0.000	0.091	0.000	0.000	0.117	0.440
	216.85	0.80	4095	0.028	0.000	0.120	0.000	0.000	0.147	0.480
	216.95	0.90	4190	0.029	0.000	0.151	0.000	0.000	0.180	0.522
	217.05	1.00	4285	0.031	0.000	0.184	0.000	0.000	0.215	0.564
	217.15	1.10	4380	0.033	0.000	0.220	0.000	0.000	0.253	0.608
	217.25	1.20	4475	0.034	0.000	0.258	0.000	0.000	0.292	0.652
	217.35	1.30	4570	0.036	0.000	0.297	0.000	0.000	0.333	0.697
	217.45	1.40	4665	0.037	0.000	0.339	0.000	0.000	0.376	0.743
Active Storage	217.55	1.50	4760	0.038	0.000	0.382	0.000	0.000	0.420	0.790
	217.65	1.60	4855	0.040	0.000	0.427	-3.800	0.000	0.467	0.838
	217.75	1.70	4950	0.041	0.000	0.473	-3.400	0.000	0.514	0.887
	217.85	1.80	5055	0.042	0.000	0.521	-3.000	0.000	0.564	0.938
	217.95	1.90	5160	0.043	0.000	0.571	-2.600	0.000	0.614	0.989
	218.05	2.00	5265	0.045	0.000	0.622	-2.200	0.000	0.667	1.041
	218.15	2.10	5370	0.046	0.000	0.675	-1.800	0.000	0.720	1.094
	218.25	2.20	5475	0.047	0.000	0.729	-1.400	0.000	0.776	1.148
	218.35	2.30	5580	0.048	0.000	0.784	-1.000	0.000	0.832	1.203
	218.45	2.40	5685	0.049	0.000	0.841	-0.600	0.000	0.890	1.260
Spillway	218.55	2.50	5790	0.050	0.000	0.899	-0.200	0.000	0.949	1.317
	218.65	2.60	5895	0.051	0.000	0.958	0.200	0.000	1.009	1.339
Regional	218.75	2.70	6000	0.052	0.000	1.018	0.600	0.035	1.105	1.360



Project No: 119-2528
Project: Alta Phase II
File: Stage-Storage-Discharge
Design by: J. Kerschbaumer
Checked by: G. Cooper
Date: 2022-02-11

Permanent Pool Check

Pond Dimensions			
Elev.	Depth	Area	Storage
	Above PP		Volume
(m)	(m)	(sqm)	(cu.m)
215.15	0.00	300	0
216.05	0.90	2700	1350



Project No: 119-2528
 Project: Alta Phase 2
 File: Forebay Design
 Design by: J. Kerschbaumer
 Checked by: G. Cooper
 Date: 2022-02-11

FOREBAY DESIGN CALCULATIONS

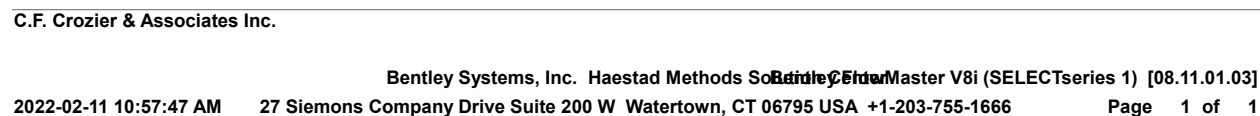
	Variable	Value
Forebay Settling Length	Length of forebay (m)	32.0
	Width of forebay (m)	32.0
	Length-to-width ratio of forebay	1.0
	Peak flow rate from forebay in quality event (m ³ /s)	0.024
	Settling velocity (m/s)	0.0003
	Required Forebay Length (m)	9
Dispersion Length	Inlet flowrate in 5 year event (m ³ /s)	1.21
	Depth of of the permanent pool in the forebay (m)	0.90
	Desired velocity in the forebay (m/s)	0.5
	Length of Dispersion (m)	22
Velocity in Forebay Check	Depth of forebay in 10 year event (m)	1.80
	Cross sectional area (m ²)	63.0
	10 year event flowrate (m ³ /s)	1.63
	Velocity in Forebay (m/s)*	0.03
Forebay Bottom Width	Length of forebay (m)	32.0
	Minimum Forbay Bottom Width (m)	4.00
DESIGN FOREBAY LENGTH (m)		32.0
DESIGN BOTTOM WIDTH (m)		32.0

* Desired maximum average velocity in the forebay is 0.15 m/s, per MOE, 2003, Page 4-56

Project Description

Input Data

Cross Section Image



Worksheet for Emergency Spillway

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Channel Slope 0.47000 m/m
Discharge 0.04 m³/s
Section Definitions

Station (m)	Elevation (m)
0+00	218.75
0+00	218.65
0+00	218.65
0+01	218.75

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 218.75)	(0+01, 218.75)	0.069

Options

Current Roughness Weighted Method Pavlovskii's Method
Open Channel Weighting Method Pavlovskii's Method
Closed Channel Weighting Method Pavlovskii's Method

Results

Normal Depth 0.08 m
Elevation Range 218.65 to 218.75 m
Flow Area 0.03 m²
Wetted Perimeter 0.54 m
Hydraulic Radius 0.05 m
Top Width 0.50 m
Normal Depth 0.08 m
Critical Depth 0.10 m
Critical Slope 0.12703 m/m

C.F. Crozier & Associates Inc.

Worksheet for Emergency Spillway

Results

Velocity	1.33	m/s
Velocity Head	0.09	m
Specific Energy	0.17	m
Froude Number	1.86	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.08	m
Critical Depth	0.10	m
Channel Slope	0.47000	m/m
Critical Slope	0.12703	m/m

APPENDIX F

Hydraulic Calculations

Proposed Overland Flow
Hydraulic Calculations

Cross Section for EXT-1

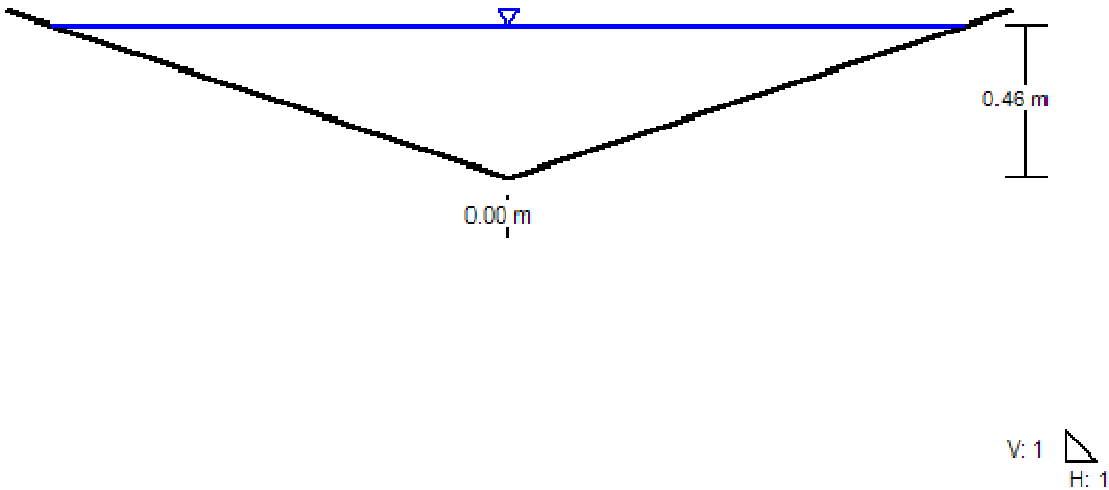
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.01500 m/m
Normal Depth	0.46 m
Left Side Slope	3.00 m/m (H:V)
Right Side Slope	3.00 m/m (H:V)
Bottom Width	0.00 m
Discharge	0.56 m³/s

Cross Section Image



Worksheet for EXT-1

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.050
Channel Slope 0.01500 m/m
Left Side Slope 3.00 m/m (H:V)
Right Side Slope 3.00 m/m (H:V)
Bottom Width 0.00 m
Discharge 0.56 m³/s

Section A-A (Figure 9)

Flow during 100 year SCS-12hr (EXT-1)

Results

Normal Depth 0.46 m
Flow Area 0.63 m²
Wetted Perimeter 2.90 m
Hydraulic Radius 0.22 m
Top Width 2.75 m
Critical Depth 0.37 m
Critical Slope 0.04608 m/m
Velocity 0.89 m/s
Velocity Head 0.04 m
Specific Energy 0.50 m
Froude Number 0.59
Flow Type Subcritical

Depth during 100 year SCS-12hr (EXT-1)

GVF Input Data

Downstream Depth 0.00 m
Length 0.00 m
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 m
Profile Description
Profile Headloss 0.00 m
Downstream Velocity Infinity m/s
Upstream Velocity Infinity m/s
Normal Depth 0.46 m
Critical Depth 0.37 m
Channel Slope 0.01500 m/m
Critical Slope 0.04608 m/m

Cross Section for EXT-2

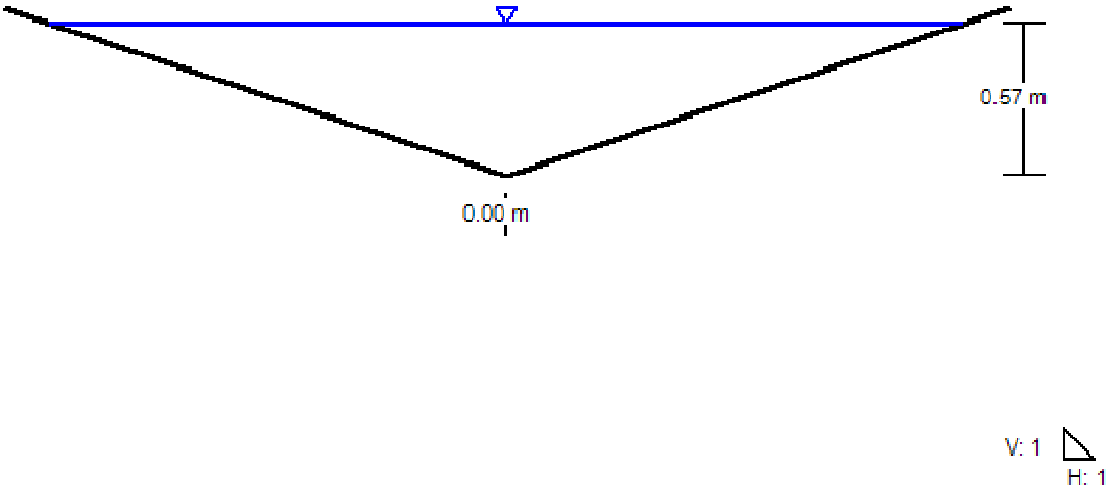
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00700 m/m
Normal Depth	0.57 m
Left Side Slope	3.00 m/m (H:V)
Right Side Slope	3.00 m/m (H:V)
Bottom Width	0.00 m
Discharge	0.68 m³/s

Cross Section Image



Worksheet for EXT-2

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.050
Channel Slope 0.00700 m/m
Left Side Slope 3.00 m/m (H:V)
Right Side Slope 3.00 m/m (H:V)
Bottom Width 0.00 m
Discharge 0.68 m³/s

Section A-A (Figure 9)

Flow during 100 year SCS-12hr (EXT-2)

Results

Normal Depth 0.57 m
Flow Area 0.97 m²
Wetted Perimeter 3.60 m
Hydraulic Radius 0.27 m
Top Width 3.42 m
Critical Depth 0.40 m
Critical Slope 0.04490 m/m
Velocity 0.70 m/s
Velocity Head 0.02 m
Specific Energy 0.59 m
Froude Number 0.42
Flow Type Subcritical

Depth during 100 year SCS-12hr (EXT-2)

GVF Input Data

Downstream Depth 0.00 m
Length 0.00 m
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 m
Profile Description
Profile Headloss 0.00 m
Downstream Velocity Infinity m/s
Upstream Velocity Infinity m/s
Normal Depth 0.57 m
Critical Depth 0.40 m
Channel Slope 0.00700 m/m
Critical Slope 0.04490 m/m

Cross Section for EXT-3

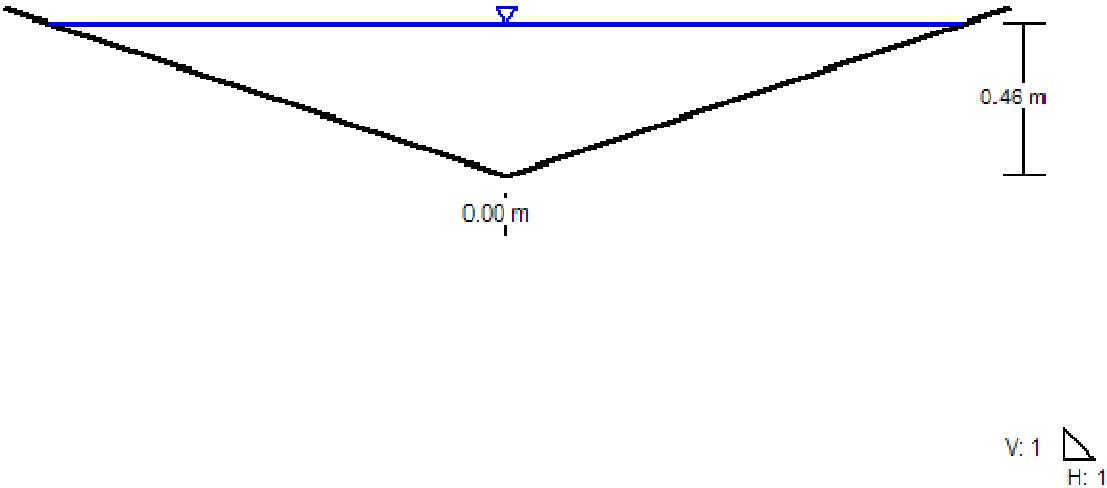
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00600 m/m
Normal Depth	0.46 m
Left Side Slope	3.00 m/m (H:V)
Right Side Slope	3.00 m/m (H:V)
Bottom Width	0.00 m
Discharge	0.35 m³/s

Cross Section Image



Worksheet for EXT-3

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.050	
Channel Slope	0.00600	m/m
Left Side Slope	3.00	m/m (H:V)
Right Side Slope	3.00	m/m (H:V)
Bottom Width	0.00	m
Discharge	0.35	m³/s

Section A-A (Figure 9)

Flow during 100 year SCS-12hr (EXT-3)

Results

Normal Depth	0.46	m
Flow Area	0.63	m²
Wetted Perimeter	2.89	m
Hydraulic Radius	0.22	m
Top Width	2.74	m
Critical Depth	0.31	m
Critical Slope	0.04906	m/m
Velocity	0.56	m/s
Velocity Head	0.02	m
Specific Energy	0.47	m
Froude Number	0.37	
Flow Type	Subcritical	

Depth during 100 year SCS-12hr (EXT-3)

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.46	m
Critical Depth	0.31	m
Channel Slope	0.00600	m/m
Critical Slope	0.04906	m/m

Cross Section for EXT-4

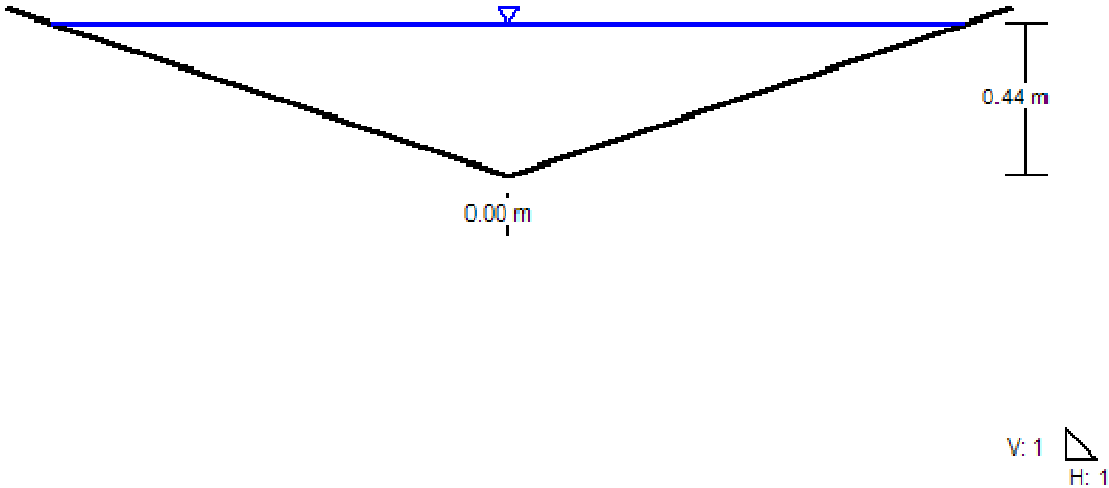
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050	
Channel Slope	0.01000	m/m
Normal Depth	0.44	m
Left Side Slope	3.00	m/m (H:V)
Right Side Slope	3.00	m/m (H:V)
Bottom Width	0.00	m
Discharge	0.42	m³/s

Cross Section Image



Worksheet for EXT-4

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.050
Channel Slope 0.01000 m/m
Left Side Slope 3.00 m/m (H:V)
Right Side Slope 3.00 m/m (H:V)
Bottom Width 0.00 m
Discharge 0.42 m³/s

Section A-A (Figure 9)

Flow during 100 year SCS-12hr (EXT-4)

Results

Normal Depth 0.44 m
Flow Area 0.59 m²
Wetted Perimeter 2.81 m
Hydraulic Radius 0.21 m
Top Width 2.67 m
Critical Depth 0.33 m
Critical Slope 0.04788 m/m
Velocity 0.71 m/s
Velocity Head 0.03 m
Specific Energy 0.47 m
Froude Number 0.48
Flow Type Subcritical

Depth during 100 year SCS-12hr (EXT-4)

GVF Input Data

Downstream Depth 0.00 m
Length 0.00 m
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 m
Profile Description
Profile Headloss 0.00 m
Downstream Velocity Infinity m/s
Upstream Velocity Infinity m/s
Normal Depth 0.44 m
Critical Depth 0.33 m
Channel Slope 0.01000 m/m
Critical Slope 0.04788 m/m

Cross Section for EXT-5

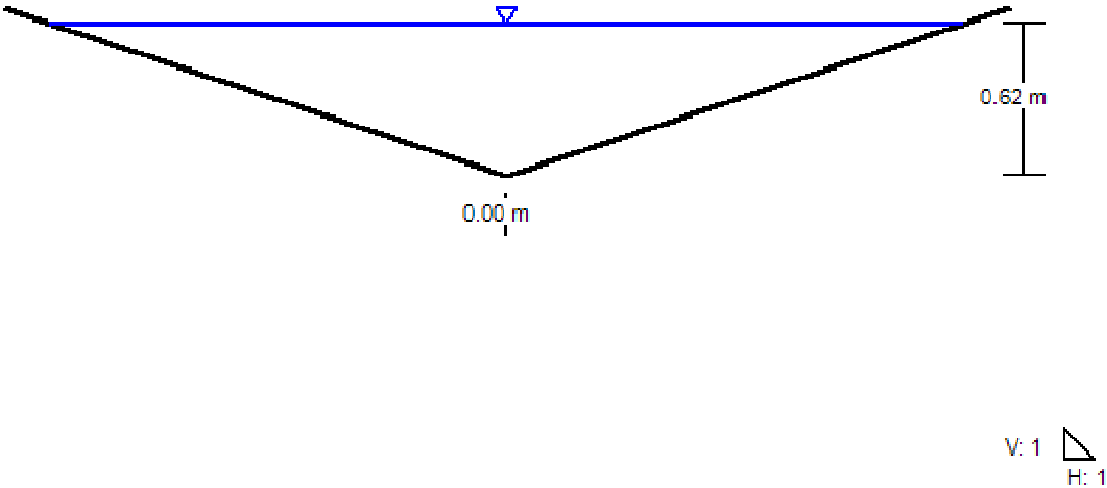
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00750 m/m
Normal Depth	0.62 m
Left Side Slope	3.00 m/m (H:V)
Right Side Slope	3.00 m/m (H:V)
Bottom Width	0.00 m
Discharge	0.90 m³/s

Cross Section Image



Worksheet for EXT-5

Project Description

Friction Method Manning Formula

Solve For Normal Depth

Input Data

Roughness	0.050
-----------	-------

Coefficient	0.000
	0.00000

Channel Slope 0.00750 m/m

Left Side Slope 3.00 m/m (H:V)

Right Side Slope 3.00 m/m (H:V)

Bottom Width 0.00 m

Discharge $0.90 \text{ m}^3/\text{s}$ ←

Section A-A (Figure 9)

Flow during 100 year SCS-12hr (EXT-5)

Results

Normal Depth 0.62 m ←

Flow Area 1.17 m²

Wetted Perimeter 3.95 m

Hydraulic Radius 0.30 m

Top Width 3.74 m

Critical Depth 0.45 m

Critical Slope 0.04327 m/m

Velocity 0.77 m/s

Velocity Head 0.03 m

Specific Energy 0.65 m

Froude Number 0.44

Flow Type	Subcritical
-----------	-------------

Depth during 100 year SCS-12hr (EXT-5)

GVF Input Data

Downstream Depth 0.00 m

Length 0.00 m

Number Of Steps	0
-----------------	---

GVF Output Data

Upstream Depth 0.00 m

Profile Description

Profile Headloss 0.00 m

Downstream Velocity Infinity m/s

Upstream Velocity Infinity m/s

Normal Depth 0.62 m

Critical Depth 0.45 m

Channel Slope 0.00750 m/m

Critical Slope 0.04327 m/m

Cross Section for NE Bypass

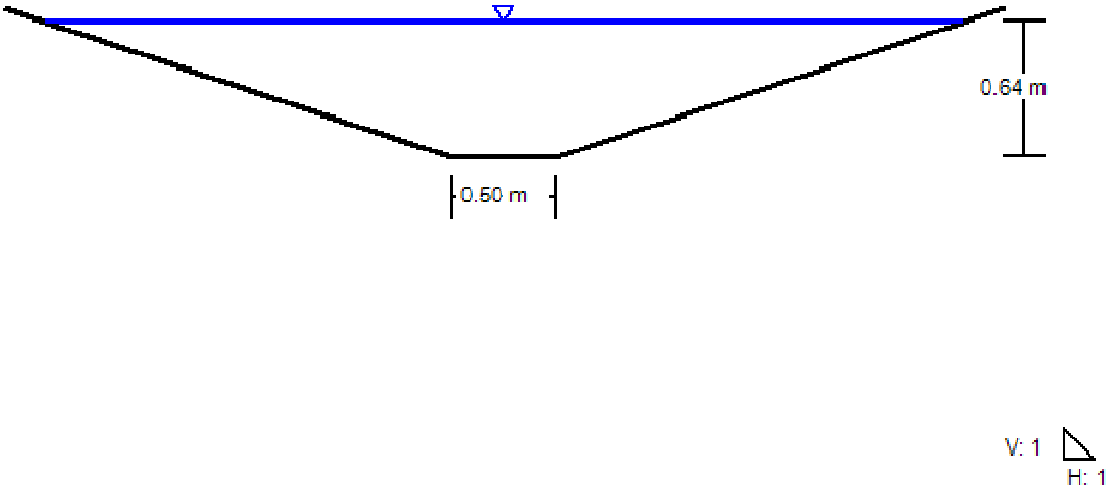
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00750 m/m
Normal Depth	0.64 m
Left Side Slope	3.00 m/m (H:V)
Right Side Slope	3.00 m/m (H:V)
Bottom Width	0.50 m
Discharge	1.32 m³/s

Cross Section Image



Worksheet for NE Bypass

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Location: South of Lot 39

Input Data

Roughness Coefficient 0.050
Channel Slope 0.00750 m/m
Left Side Slope 3.00 m/m (H:V)
Right Side Slope 3.00 m/m (H:V)
Bottom Width 0.50 m
Discharge 1.32 m³/s

Section B-B (Fig 9)

Combination of EXT-4 + EXT-5 (100 year SCS-12hr)

Results

Normal Depth 0.64 m
Flow Area 1.56 m²
Wetted Perimeter 4.56 m
Hydraulic Radius 0.34 m
Top Width 4.35 m
Critical Depth 0.45 m
Critical Slope 0.04082 m/m
Velocity 0.85 m/s
Velocity Head 0.04 m
Specific Energy 0.68 m
Froude Number 0.45
Flow Type Subcritical

Depth during 100 year SCS-12hr

GVF Input Data

Downstream Depth 0.00 m
Length 0.00 m
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 m
Profile Description
Profile Headloss 0.00 m
Downstream Velocity Infinity m/s
Upstream Velocity Infinity m/s
Normal Depth 0.64 m
Critical Depth 0.45 m
Channel Slope 0.00750 m/m
Critical Slope 0.04082 m/m

Sub-Watershed Study
Hydraulic Calculation Sheets

Worksheet for Culvert 1

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.32	m
Critical Depth	0.43	m
Channel Slope	0.07280	m/m
Critical Slope	0.01522	m/m

Cross Section for Culvert 1

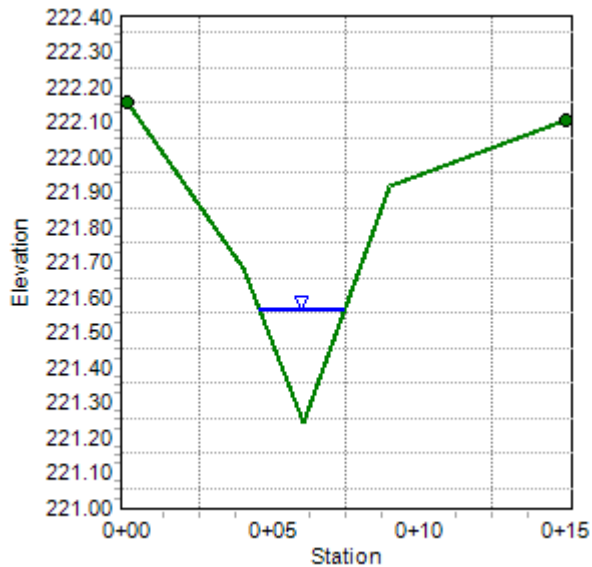
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.07280	m/m
Normal Depth	0.32	m
Discharge	1.21	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 1

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	222.67 m	Headwater Depth/Height	1.56
Computed Headwater Elev.	222.67 m	Discharge	1.2085 m ³ /s
Inlet Control HW Elev.	222.65 m	Tailwater Elevation	221.56 m
Outlet Control HW Elev.	222.67 m	Control Type	Entrance Control

Grades			
Upstream Invert	221.36 m	Downstream Invert	220.70 m
Length	9.90 m	Constructed Slope	0.066667 m/m

Hydraulic Profile			
Profile	CompositePressureProfileS1S2	Depth, Downstream	0.86 m
Slope Type	N/A	Normal Depth	0.46 m
Flow Regime	N/A	Critical Depth	0.66 m
Velocity Downstream	2.19 m/s	Critical Slope	0.023882 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.84 m
Section Size	825 mm	Rise	0.84 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	222.67 m	Upstream Velocity Head	0.34 m
Ke	0.90	Entrance Loss	0.31 m

Inlet Control Properties			
Inlet Control HW Elev.	222.65 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.6 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Worksheet for Culvert 2

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.30	m
Critical Depth	0.43	m
Channel Slope	0.11000	m/m
Critical Slope	0.01649	m/m

Cross Section for Culvert 2

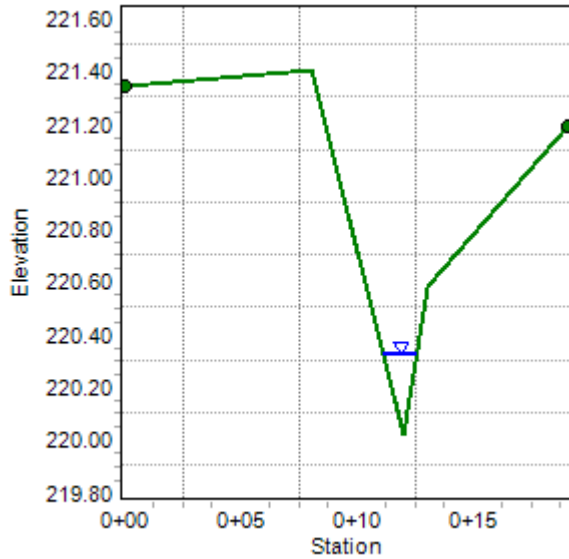
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.11000	m/m
Normal Depth	0.30	m
Discharge	0.65	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 2

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	221.60 m	Headwater Depth/Height	3.48
Computed Headwater Elev.	221.60 m	Discharge	0.6470 m³/s
Inlet Control HW Elev.	221.60 m	Tailwater Elevation	220.32 m
Outlet Control HW Elev.	221.58 m	Control Type	Inlet Control
Grades			
Upstream Invert	220.54 m	Downstream Invert	220.42 m
Length	7.00 m	Constructed Slope	0.017143 m/m
Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.30 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.30 m
Velocity Downstream	2.97 m/s	Critical Slope	0.041125 m/m
Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	3		
Outlet Control Properties			
Outlet Control HW Elev.	221.58 m	Upstream Velocity Head	0.45 m
Ke	0.20	Entrance Loss	0.09 m
Inlet Control Properties			
Inlet Control HW Elev.	221.60 m	Flow Control	N/A
Inlet Type	Groove end w/headwall	Area Full	0.2 m²
K	0.00180	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	2
C	0.02920	Equation Form	1
Y	0.74000		

Culvert Calculator Report

Culvert 3

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	218.30 m	Headwater Depth/Height	1.15
Computed Headwater Elev.	218.30 m	Discharge	0.9043 m³/s
Inlet Control HW Elev.	218.19 m	Tailwater Elevation	215.87 m
Outlet Control HW Elev.	218.30 m	Control Type	Entrance Control

Grades			
Upstream Invert	217.34 m	Downstream Invert	215.87 m
Length	12.00 m	Constructed Slope	0.122500 m/m

Hydraulic Profile			
Profile	S2	Depth, Downstream	0.33 m
Slope Type	Steep	Normal Depth	0.33 m
Flow Regime	Supercritical	Critical Depth	0.57 m
Velocity Downstream	4.45 m/s	Critical Slope	0.018862 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.84 m
Section Size	825 mm	Rise	0.84 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	218.30 m	Upstream Velocity Head	0.26 m
Ke	0.50	Entrance Loss	0.13 m

Inlet Control Properties			
Inlet Control HW Elev.	218.19 m	Flow Control	N/A
Inlet Type	Headwall	Area Full	0.6 m²
K	0.00780	HDS 5 Chart	2
M	2.00000	HDS 5 Scale	1
C	0.03790	Equation Form	1
Y	0.69000		

No tailwater expected

Culvert Calculator Report

Culvert 4

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	196.34 m	Headwater Depth/Height	2.19
Computed Headwater Elev.	196.34 m	Discharge	1.9391 m³/s
Inlet Control HW Elev.	196.34 m	Tailwater Elevation	193.18 m
Outlet Control HW Elev.	196.12 m	Control Type	Inlet Control

Grades			
Upstream Invert	194.34 m	Downstream Invert	193.18 m
Length	7.00 m	Constructed Slope	0.165714 m/m

Hydraulic Profile			
Profile	S2	Depth, Downstream	0.50 m
Slope Type	Steep	Normal Depth	0.44 m
Flow Regime	Supercritical	Critical Depth	0.80 m
Velocity Downstream	5.31 m/s	Critical Slope	0.032373 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	196.12 m	Upstream Velocity Head	0.51 m
Ke	0.90	Entrance Loss	0.46 m

Inlet Control Properties			
Inlet Control HW Elev.	196.34 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

No tailwater expected

Cross Section for PRE D/S Culvert 4

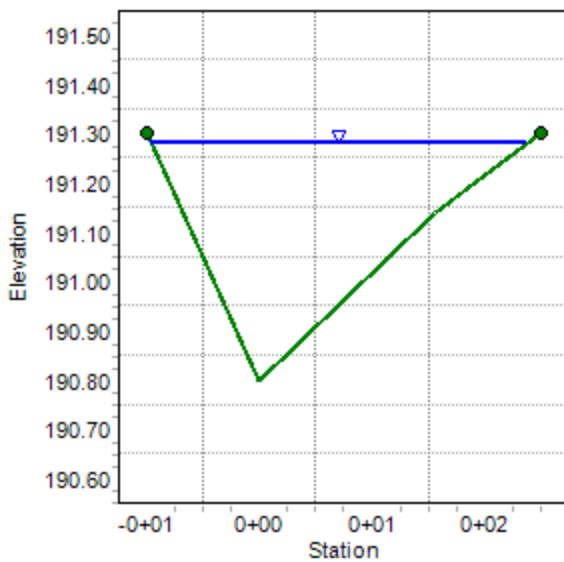
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.01180	m/m
Normal Depth	0.48	m
Discharge	1.00	m³/s

Cross Section Image



Project Description

Input Data

Options

Results

Worksheet for PRE D/S Culvert 4

Results

Velocity	1.31	m/s
Velocity Head	0.09	m
Specific Energy	0.56	m
Froude Number	0.88	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.48	m
Critical Depth	0.45	m
Channel Slope	0.01180	m/m
Critical Slope	0.01562	m/m

Cross Section for POST D/S Culvert 4

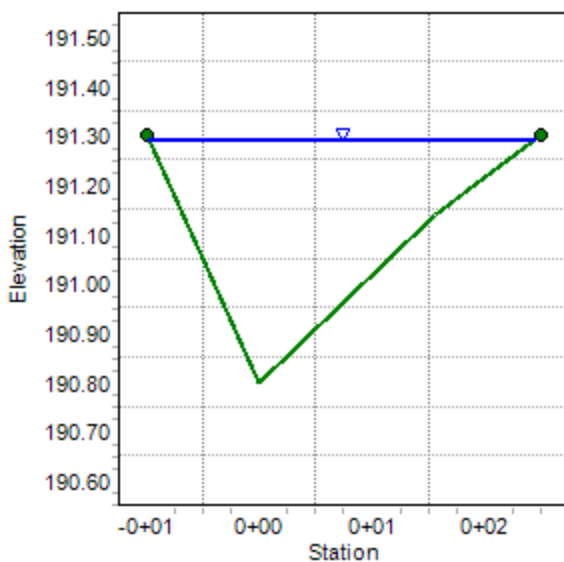
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.01180	m/m
Normal Depth	0.49	m
Discharge	1.09	m³/s

Cross Section Image



Worksheet for POST D/S Culvert 4

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.01180	m/m
Discharge	1.09	m³/s
Section Definitions		

Station (m)	Elevation (m)
-------------	---------------

-0+01	191.30
0+00	190.80
0+02	191.14
0+03	191.30

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(-0+01, 191.30)	(0+03, 191.30)	0.030

Options

Current Roughness Weighted Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results

Normal Depth	0.49	m
Elevation Range	190.80 to 191.30	m
Flow Area	0.81	m ²
Wetted Perimeter	3.60	m
Hydraulic Radius	0.23	m
Top Width	3.44	m
Normal Depth	0.49	m
Critical Depth	0.47	m
Critical Slope	0.01545	m/m

Worksheet for POST D/S Culvert 4

Results

Velocity	1.34	m/s
Velocity Head	0.09	m
Specific Energy	0.58	m
Froude Number	0.88	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.49	m
Critical Depth	0.47	m
Channel Slope	0.01180	m/m
Critical Slope	0.01545	m/m

Worksheet for Culvert 5

Results

Froude Number	1.10
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.38	m
Critical Depth	0.40	m
Channel Slope	0.01800	m/m
Critical Slope	0.01472	m/m

Cross Section for Culvert 5

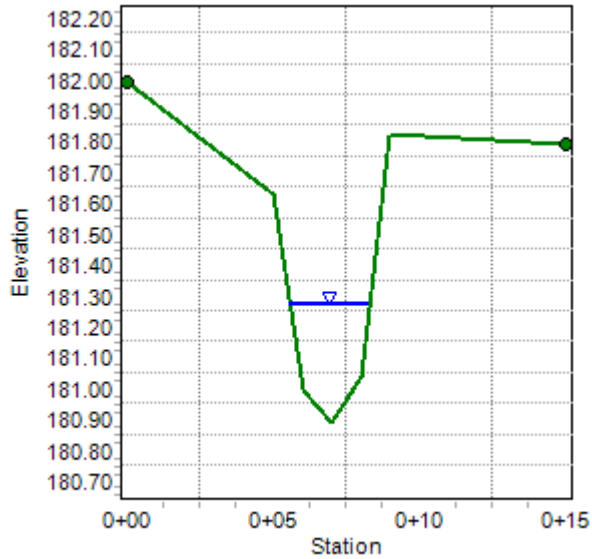
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.01800	m/m
Normal Depth	0.38	m
Discharge	1.29	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 5

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	182.46 m	Headwater Depth/Height	1.72
Computed Headwater Elev.	182.46 m	Discharge	1.2913 m³/s
Inlet Control HW Elev.	182.46 m	Tailwater Elevation	181.27 m
Outlet Control HW Elev.	182.39 m	Control Type	Inlet Control

Grades			
Upstream Invert	181.02 m	Downstream Invert	180.89 m
Length	8.73 m	Constructed Slope	0.014891 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.68 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.68 m
Velocity Downstream	2.69 m/s	Critical Slope	0.025698 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.84 m
Section Size	825 mm	Rise	0.84 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	182.39 m	Upstream Velocity Head	0.28 m
Ke	0.90	Entrance Loss	0.25 m

Inlet Control Properties			
Inlet Control HW Elev.	182.46 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.6 m²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Worksheet for Culvert 6

Results

Flow Type Subcritical

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.33	m
Critical Depth	0.28	m
Channel Slope	0.00905	m/m
Critical Slope	0.01607	m/m

Cross Section for Culvert 6

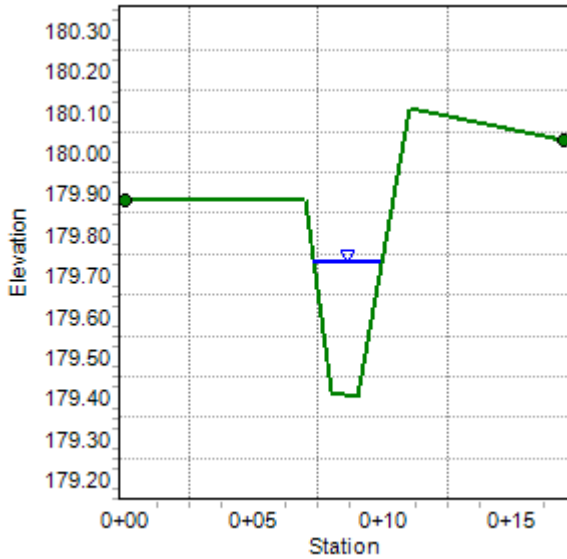
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.00905	m/m
Normal Depth	0.33	m
Discharge	0.66	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 6

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	180.55 m	Headwater Depth/Height	1.19
Computed Headwater Elev.	180.55 m	Discharge	0.6603 m³/s
Inlet Control HW Elev.	180.49 m	Tailwater Elevation	179.73 m
Outlet Control HW Elev.	180.55 m	Control Type	Outlet Control
Grades			
Upstream Invert	179.64 m	Downstream Invert	179.37 m
Length	15.37 m	Constructed Slope	0.017567 m/m
Hydraulic Profile			
Profile	M2	Depth, Downstream	0.50 m
Slope Type	Mild	Normal Depth	0.51 m
Flow Regime	Subcritical	Critical Depth	0.50 m
Velocity Downstream	2.08 m/s	Critical Slope	0.018625 m/m
Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.76 m
Section Size	750 mm	Rise	0.76 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	180.55 m	Upstream Velocity Head	0.21 m
Ke	0.90	Entrance Loss	0.19 m
Inlet Control Properties			
Inlet Control HW Elev.	180.49 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.5 m²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Worksheet for Culvert 7

Results

Froude Number	1.99
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.31	m
Critical Depth	0.44	m
Channel Slope	0.06690	m/m
Critical Slope	0.01532	m/m

Cross Section for Culvert 7

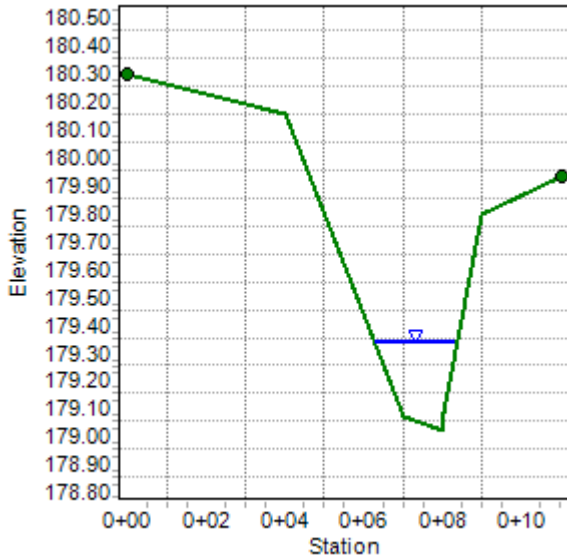
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.06690	m/m
Normal Depth	0.31	m
Discharge	1.18	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 7

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	180.20 m	Headwater Depth/Height	1.63
Computed Headwater Elev.	180.20 m	Discharge	1.1759 m³/s
Inlet Control HW Elev.	180.11 m	Tailwater Elevation	179.33 m
Outlet Control HW Elev.	180.20 m	Control Type	Outlet Control

Grades			
Upstream Invert	178.83 m	Downstream Invert	178.82 m
Length	9.31 m	Constructed Slope	0.001074 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.65 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.65 m
Velocity Downstream	2.55 m/s	Critical Slope	0.023228 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.84 m
Section Size	825 mm	Rise	0.84 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	180.20 m	Upstream Velocity Head	0.23 m
Ke	0.90	Entrance Loss	0.21 m

Inlet Control Properties			
Inlet Control HW Elev.	180.11 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.6 m²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

Culvert 8

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	180.73 m	Headwater Depth/Height	2.35
Computed Headwater Elev.	180.73 m	Discharge	2.8402 m³/s
Inlet Control HW Elev.	180.28 m	Tailwater Elevation	178.28 m
Outlet Control HW Elev.	180.73 m	Control Type	Outlet Control
Grades			
Upstream Invert	178.58 m	Downstream Invert	178.28 m
Length	36.46 m	Constructed Slope	0.008228 m/m
Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.74 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.74 m
Velocity Downstream	3.04 m/s	Critical Slope	0.024621 m/m
Section			
Section Shape	Arch	Mannings Coefficient	0.025
Section Material	Aluminum Var CR Historic	Span	1.47 m
Section Size	1470 x 910 mm	Rise	0.91 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	180.73 m	Upstream Velocity Head	0.37 m
Ke	0.90	Entrance Loss	0.33 m
Inlet Control Properties			
Inlet Control HW Elev.	180.28 m	Flow Control	N/A
Inlet Type	Thin wall projecting	Area Full	1.1 m²
K	0.03400	HDS 5 Chart	34
M	1.50000	HDS 5 Scale	3
C	0.04960	Equation Form	1
Y	0.57000		

No tailwater expected

Culvert Calculator Report

Culvert 9

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	185.21 m	Headwater Depth/Height	0.82
Computed Headwater Elev.	185.21 m	Discharge	0.4805 m³/s
Inlet Control HW Elev.	185.14 m	Tailwater Elevation	184.52 m
Outlet Control HW Elev.	185.21 m	Control Type	Outlet Control
Grades			
Upstream Invert	184.65 m	Downstream Invert	184.52 m
Length	8.60 m	Constructed Slope	0.015116 m/m
Hydraulic Profile			
Profile	M2	Depth, Downstream	0.31 m
Slope Type	Mild	Normal Depth	0.33 m
Flow Regime	Subcritical	Critical Depth	0.31 m
Velocity Downstream	1.64 m/s	Critical Slope	0.017714 m/m
Section			
Section Shape	Arch	Mannings Coefficient	0.028
Section Material	Aluminum 183 Series MCR 1	Span	1.09 m
Section Size	1090 x 690 mm	Rise	0.69 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	185.21 m	Upstream Velocity Head	0.12 m
Ke	0.90	Entrance Loss	0.11 m
Inlet Control Properties			
Inlet Control HW Elev.	185.14 m	Flow Control	N/A
Inlet Type	CR structural plate, projecting	Area Full	0.6 m²
K	0.03000	HDS 5 Chart	35
M	1.50000	HDS 5 Scale	1
C	0.04960	Equation Form	1
Y	0.57000		

No tailwater expected

Culvert Calculator Report

Culvert 10

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	183.15 m	Headwater Depth/Height	1.10
Computed Headwater Elev.	183.15 m	Discharge	1.1486 m³/s
Inlet Control HW Elev.	183.07 m	Tailwater Elevation	182.07 m
Outlet Control HW Elev.	183.15 m	Control Type	Entrance Control

Grades			
Upstream Invert	182.31 m	Downstream Invert	182.07 m
Length	8.00 m	Constructed Slope	0.030000 m/m

Hydraulic Profile			
Profile	S2	Depth, Downstream	0.39 m
Slope Type	Steep	Normal Depth	0.39 m
Flow Regime	Supercritical	Critical Depth	0.47 m
Velocity Downstream	2.41 m/s	Critical Slope	0.017412 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.76 m
Section Size	750 mm	Rise	0.76 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	183.15 m	Upstream Velocity Head	0.20 m
Ke	0.90	Entrance Loss	0.18 m

Inlet Control Properties			
Inlet Control HW Elev.	183.07 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.9 m²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

No tailwater expected

Worksheet for Culvert 11

Project Description

Manning Formula

Normal Depth

Tailwater Calculation for Culvert 11

Input Data

0.03086 m/m

2.72 m³/s

Section Definitions

Station (m)	Elevation (m)
0+00	180.50
0+07	180.31
0+08	179.80
0+09	179.77
0+09	179.77
0+10	180.45

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 180.50)	(0+10, 180.45)	0.030

Options

Improved Lotter's Method

Improved Lotter's Method

Horton's Method

Results

0.60 m

179.77 to 180.50 m

1.26 m²

5.58 m

0.22 m

5.27 m

0.60 m

0.69 m

0.01549 m/m

2.17 m/s

0.24 m

0.84 m

1.42

Results

Supercritical

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.60	m
Critical Depth	0.69	m
Channel Slope	0.03086	m/m
Critical Slope	0.01549	m/m

Cross Section for Culvert 11

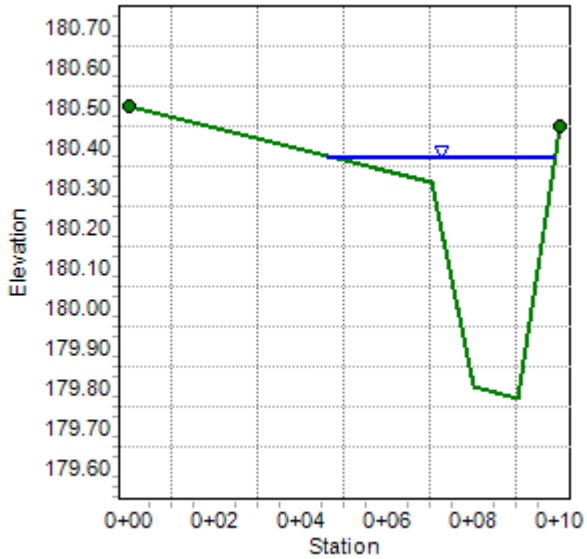
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.03086	m/m
Normal Depth	0.60	m
Discharge	2.72	m ³ /s

Cross Section Image



Culvert Calculator Report

Culvert 11

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	181.60 m	Headwater Depth/Height	1.43
Computed Headwater Elev.	181.60 m	Discharge	2.7182 m³/s
Inlet Control HW Elev.	181.45 m	Tailwater Elevation	180.37 m
Outlet Control HW Elev.	181.60 m	Control Type	Outlet Control

Grades			
Upstream Invert	180.15 m	Downstream Invert	179.96 m
Length	31.35 m	Constructed Slope	0.006061 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.69 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.69 m
Velocity Downstream	2.70 m/s	Critical Slope	0.017183 m/m

Section			
Section Shape	Arch	Mannings Coefficient	0.025
Section Material	Aluminum Var CR Historic	Span	1.65 m
Section Size	1650 x 1020 mm	Rise	1.02 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	181.60 m	Upstream Velocity Head	0.22 m
Ke	0.90	Entrance Loss	0.20 m

Inlet Control Properties			
Inlet Control HW Elev.	181.45 m	Flow Control	N/A
Inlet Type	Thin wall projecting	Area Full	1.3 m²
K	0.03400	HDS 5 Chart	34
M	1.50000	HDS 5 Scale	3
C	0.04960	Equation Form	1
Y	0.57000		

APPENDIX G

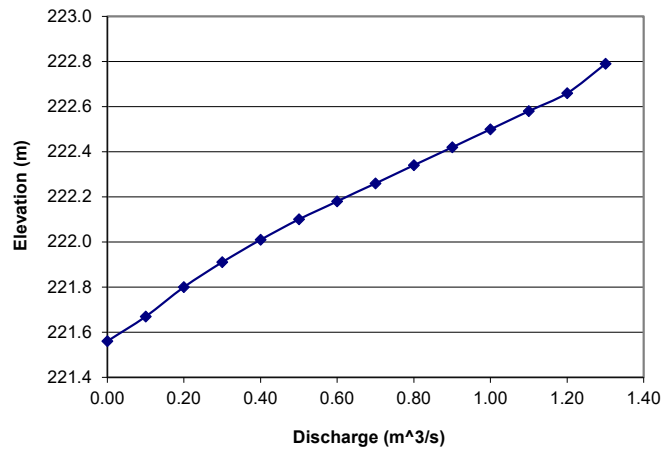
Culvert Data Sheets

CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	1
LOCATION:	Hidden Lake Road	CAPACITY:	1.2 m ³ /s
SIZE/TYPE:	825 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	9.90 m
TOP OF ROAD ELEVATION:	222.76 m
LOW CHORD ELEVATION:	222.19 m
MAX ALLOWABLE HEADWATER	222.67 m
UPSTREAM INVERT ELEVATION:	221.36 m
DOWNSTREAM INVERT ELEVATION:	220.70 m
FLOW AREA:	0.60 m ²



PHOTOGRAPHIC PRESENTATION

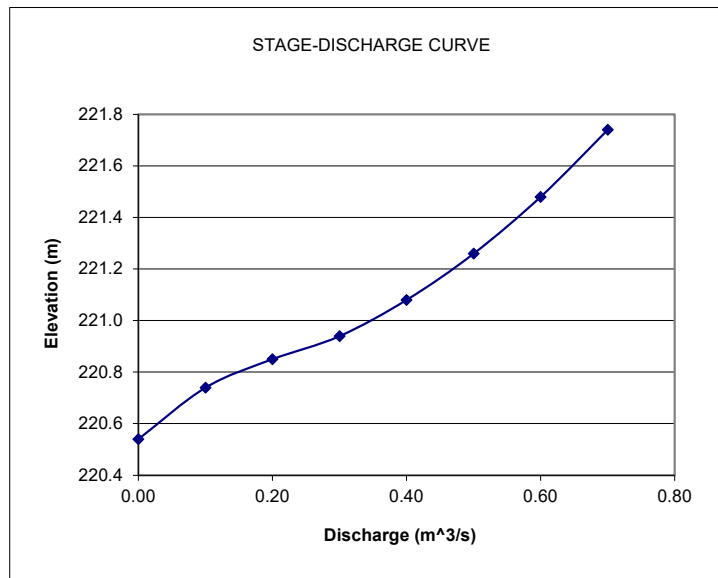


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	2
LOCATION:	Hidden Lake Road - Private Laneway	CAPACITY:	0.6 m ³ /s
SIZE/TYPE:	3 X 300 mm Concrete	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	7.00 m
TOP OF ROAD ELEVATION:	221.60 m
LOW CHORD ELEVATION:	220.84 m
MAX ALLOWABLE HEADWATER	221.60 m
UPSTREAM INVERT ELEVATION:	220.54 m
DOWNSTREAM INVERT ELEVATION:	220.42 m
FLOW AREA:	0.20 m ²



PHOTOGRAPHIC PRESENTATION

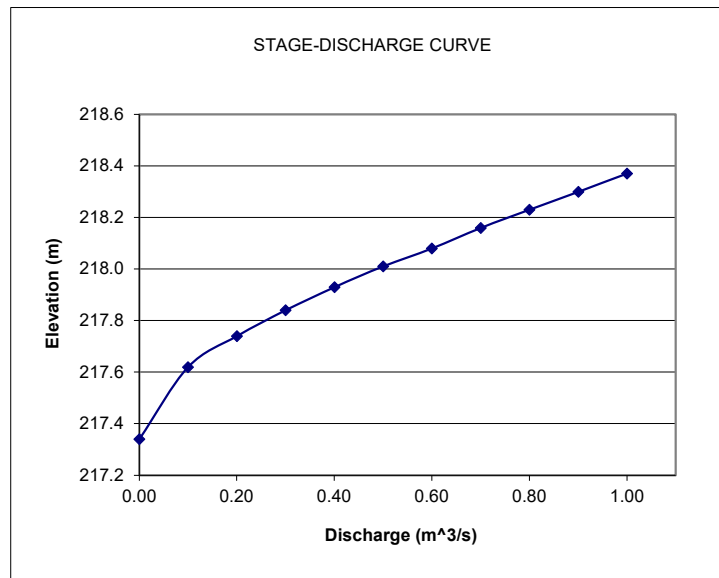


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	3
LOCATION:	Rear Yard	CAPACITY:	0.9 m ³ /s
SIZE/TYPE:	825 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	12.00 m
TOP OF ROAD ELEVATION:	N/A m
LOW CHORD ELEVATION:	218.17 m
MAX ALLOWABLE HEADWATER	218.30 m
UPSTREAM INVERT ELEVATION:	217.34 m
DOWNSTREAM INVERT ELEVATION:	215.87 m
FLOW AREA:	0.60 m ²



PHOTOGRAPHIC PRESENTATION

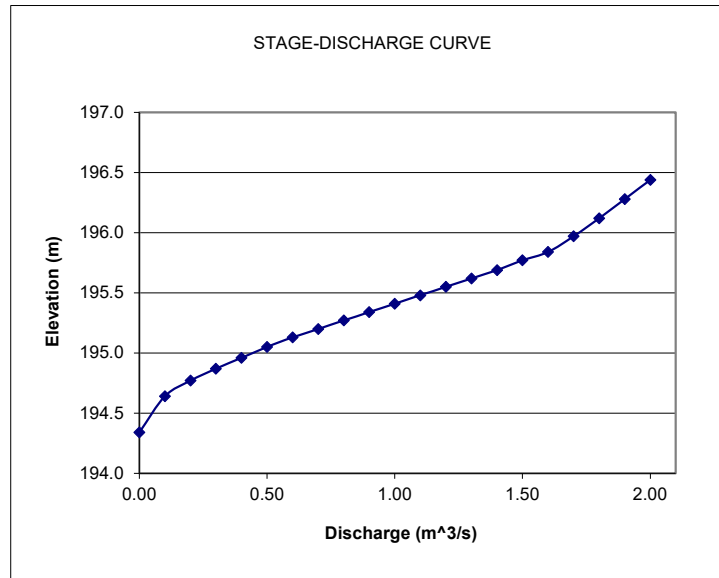


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	4
LOCATION:	Hidden Lake Road	CAPACITY:	1.9 m ³ /s
SIZE/TYPE:	900 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	7.00 m
TOP OF ROAD ELEVATION:	196.34 m
LOW CHORD ELEVATION:	195.24 m
MAX ALLOWABLE HEADWATER	196.34 m
UPSTREAM INVERT ELEVATION:	194.34 m
DOWNSTREAM INVERT ELEVATION:	193.18 m
FLOW AREA:	0.70 m ²



PHOTOGRAPHIC PRESENTATION

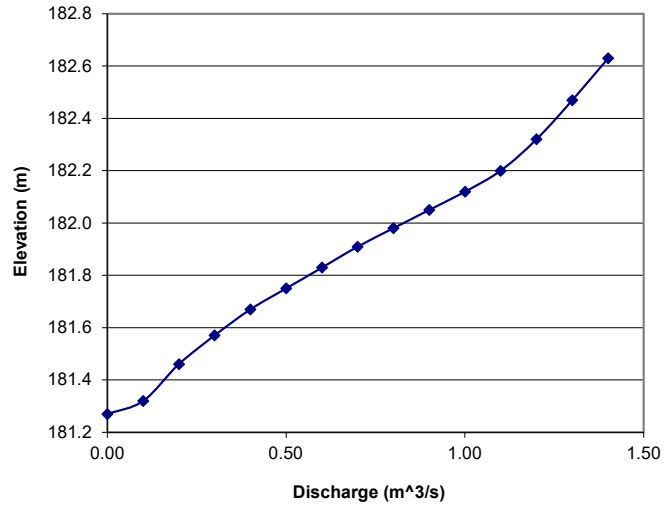


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	5
LOCATION:	Georgian Trail	CAPACITY:	1.3 m ³ /s
SIZE/TYPE:	825 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	8.73 m
TOP OF ROAD ELEVATION:	182.46 m
LOW CHORD ELEVATION:	181.85 m
MAX ALLOWABLE HEADWATER	182.46 m
UPSTREAM INVERT ELEVATION:	181.02 m
DOWNSTREAM INVERT ELEVATION:	180.89 m
FLOW AREA:	0.60 m ²



PHOTOGRAPHIC PRESENTATION

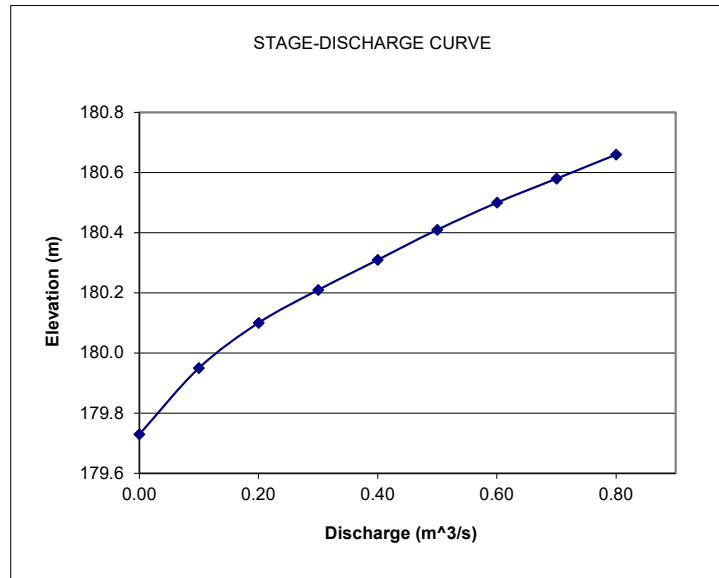


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	6
LOCATION:	Rear Yard	CAPACITY:	0.70 m ³ /s
SIZE/TYPE:	750 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	15.37 m
TOP OF ROAD ELEVATION:	NA m
LOW CHORD ELEVATION:	180.39 m
MAX ALLOWABLE HEADWATER	180.55 m
UPSTREAM INVERT ELEVATION:	179.64 m
DOWNSTREAM INVERT ELEVATION:	179.37 m
FLOW AREA:	0.50 m ²



PHOTOGRAPHIC PRESENTATION

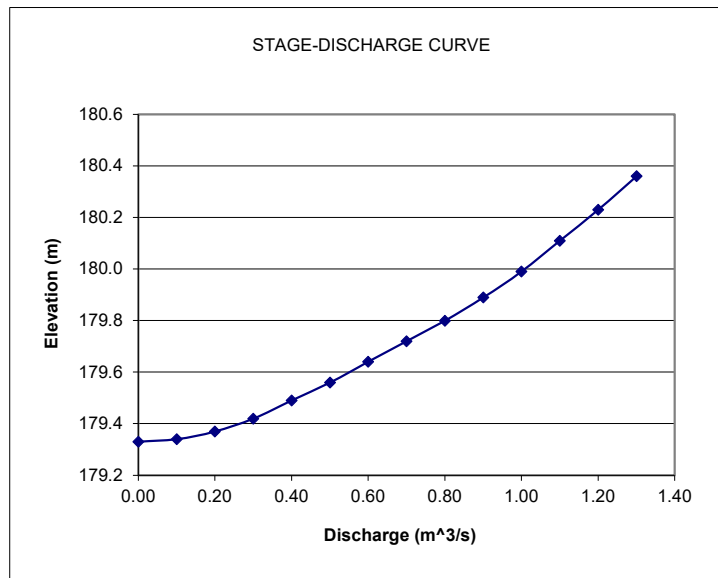


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	7
LOCATION:	Private Driveway	CAPACITY:	1.2 m ³ /s
SIZE/TYPE:	825 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	9.31 m
TOP OF ROAD ELEVATION:	N/A m
LOW CHORD ELEVATION:	179.66 m
MAX ALLOWABLE HEADWATER	180.20 m
UPSTREAM INVERT ELEVATION:	178.83 m
DOWNSTREAM INVERT ELEVATION:	178.82 m
FLOW AREA:	0.60 m ²



PHOTOGRAPHIC PRESENTATION

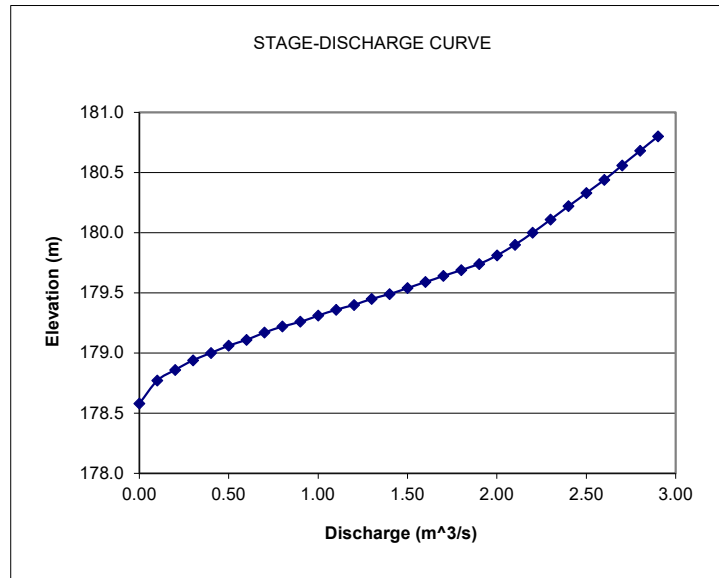


CULVERT DATA

WATERCOURSE:	22	STRUCTURE NO.	8
LOCATION:	Highway 26	CAPACITY:	2.8 m ³ /s
SIZE/TYPE:	1470 X 910 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	36.46 m
TOP OF ROAD ELEVATION:	180.73 m
LOW CHORD ELEVATION:	179.49 m
MAX ALLOWABLE HEADWATER	180.73 m
UPSTREAM INVERT ELEVATION:	178.58 m
DOWNSTREAM INVERT ELEVATION:	178.28 m
FLOW AREA:	1.10 m ²



PHOTOGRAPHIC PRESENTATION

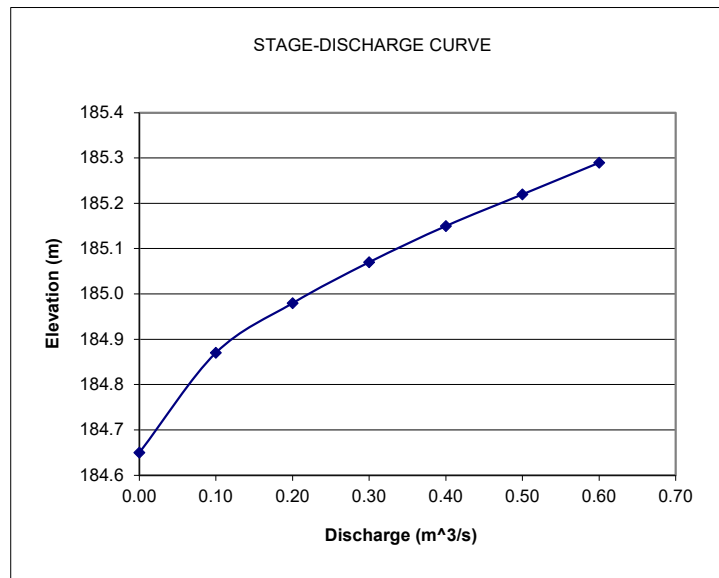


CULVERT DATA

WATERCOURSE:	21A	STRUCTURE NO.	9
LOCATION:	Private Driveways along Hidden Lake Road		
SIZE/TYPE:	1090 x 690 mm CSP Arch	CAPACITY:	0.5 m ³ /s
		RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	8.60 m
TOP OF ROAD ELEVATION:	185.50 m
LOW CHORD ELEVATION:	185.34 m
MAX ALLOWABLE HEADWATER	185.50 m
UPSTREAM INVERT ELEVATION:	184.65 m
DOWNSTREAM INVERT ELEVATION:	184.52 m
FLOW AREA:	0.60 m ²



PHOTOGRAPHIC PRESENTATION

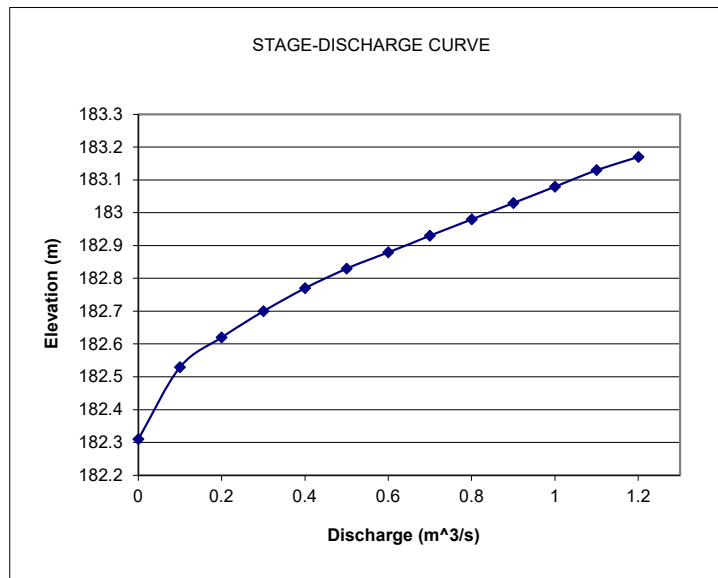


CULVERT DATA

WATERCOURSE:	21A	STRUCTURE NO.	10
LOCATION:	Georgian Trail	CAPACITY:	1.1 m ³ /s
SIZE/TYPE:	2 x 750 mm CSP	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	8.00 m
TOP OF ROAD ELEVATION:	183.15 m
LOW CHORD ELEVATION:	183.06 m
MAX ALLOWABLE HEADWATER	183.15 m
UPSTREAM INVERT ELEVATION:	182.31 m
DOWNSTREAM INVERT ELEVATION:	182.07 m
FLOW AREA:	0.90 m ²



PHOTOGRAPHIC PRESENTATION

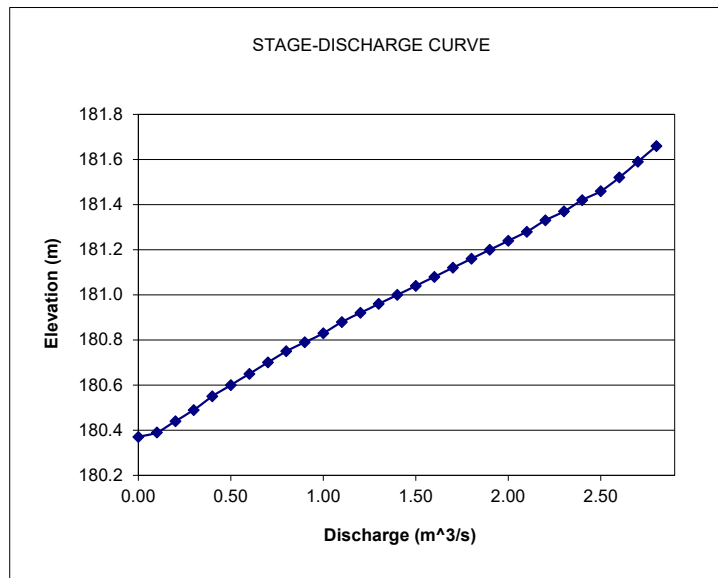


CULVERT DATA

WATERCOURSE:	21A	STRUCTURE NO.	11
LOCATION:	Highway 26	CAPACITY:	2.7 m ³ /s
SIZE/TYPE:	1650 x 1020 mm CSP ellipse	RETURN PERIOD:	>100 yr

SPECIFICATIONS

LENGTH OF STRUCTURE:	31.35 m
TOP OF ROAD ELEVATION:	181.60 m
LOW CHORD ELEVATION:	181.10 m
MAX ALLOWABLE HEADWATER	181.60 m
UPSTREAM INVERT ELEVATION:	180.15 m
DOWNSTREAM INVERT ELEVATION:	179.96 m
FLOW AREA:	1.30 m ²



PHOTOGRAPHIC PRESENTATION



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Figure 12:	Hydraulic Structure Location Plan



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ADMIRAL BUILDING
1 FIRST STREET, SUITE 200
COLLINGWOOD, ON, L9Y 1A1
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705-446-3520 F
WWW.CFCROZIER.CA
INFO@CFCROZIER.CA

PROJECT

ALTA SUBDIVISION PHASE II
TOWN OF THE BLUE MOUNTAINS

TITLE

SITE LOCATION PLAN

DRAWN BY:
J.O.

DATE:
06/28/2021

DRAWING No.:

PROJECT No.:
119-2528-201

SCALE:
N.T.S.

FIG. 1

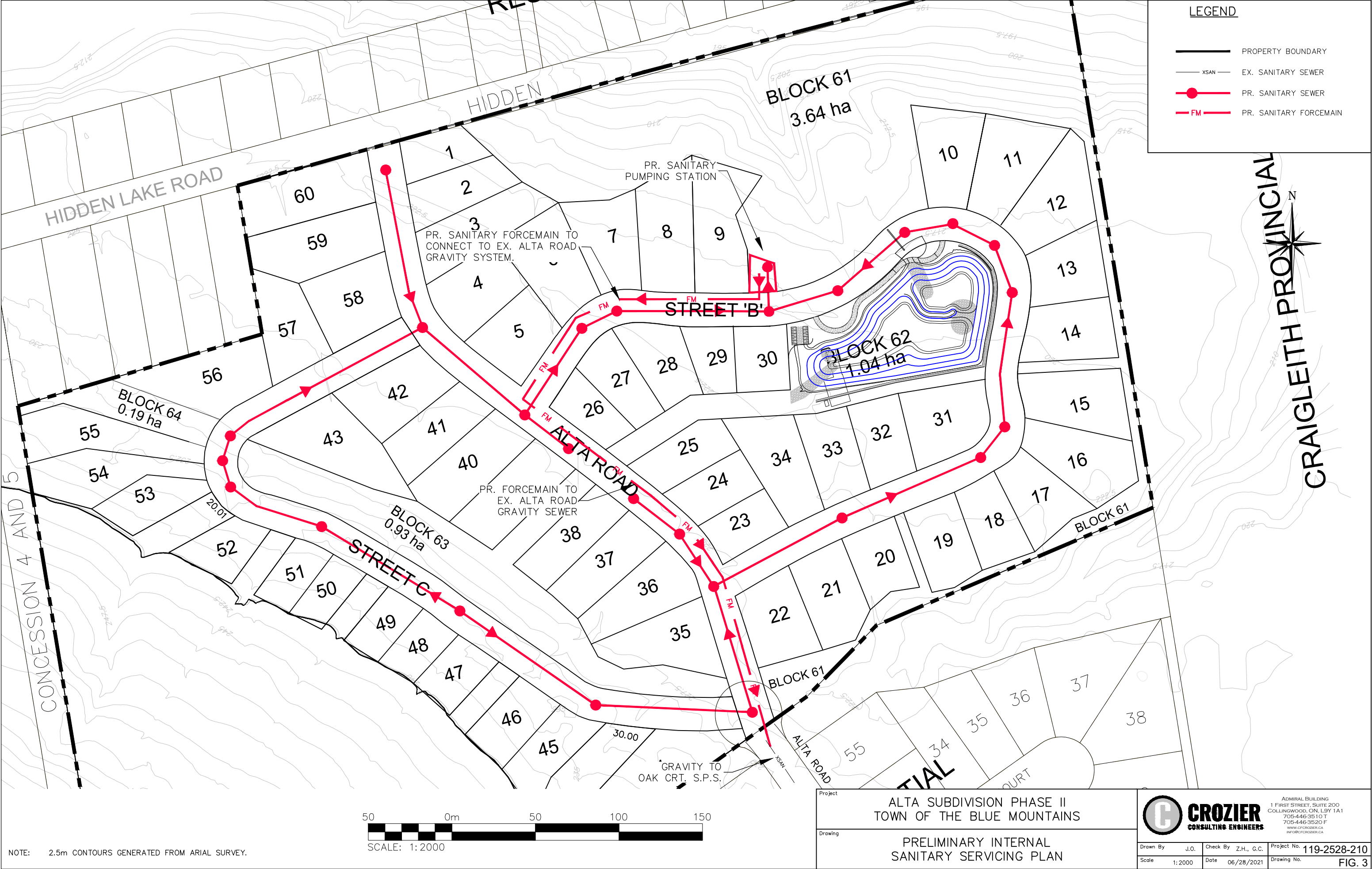


NOTE: TOPOGRAPHIC SURVEY PER PATTEN & THOMSEN.
(DISPLAYED CONTOUR INTERVAL, 1.0m)

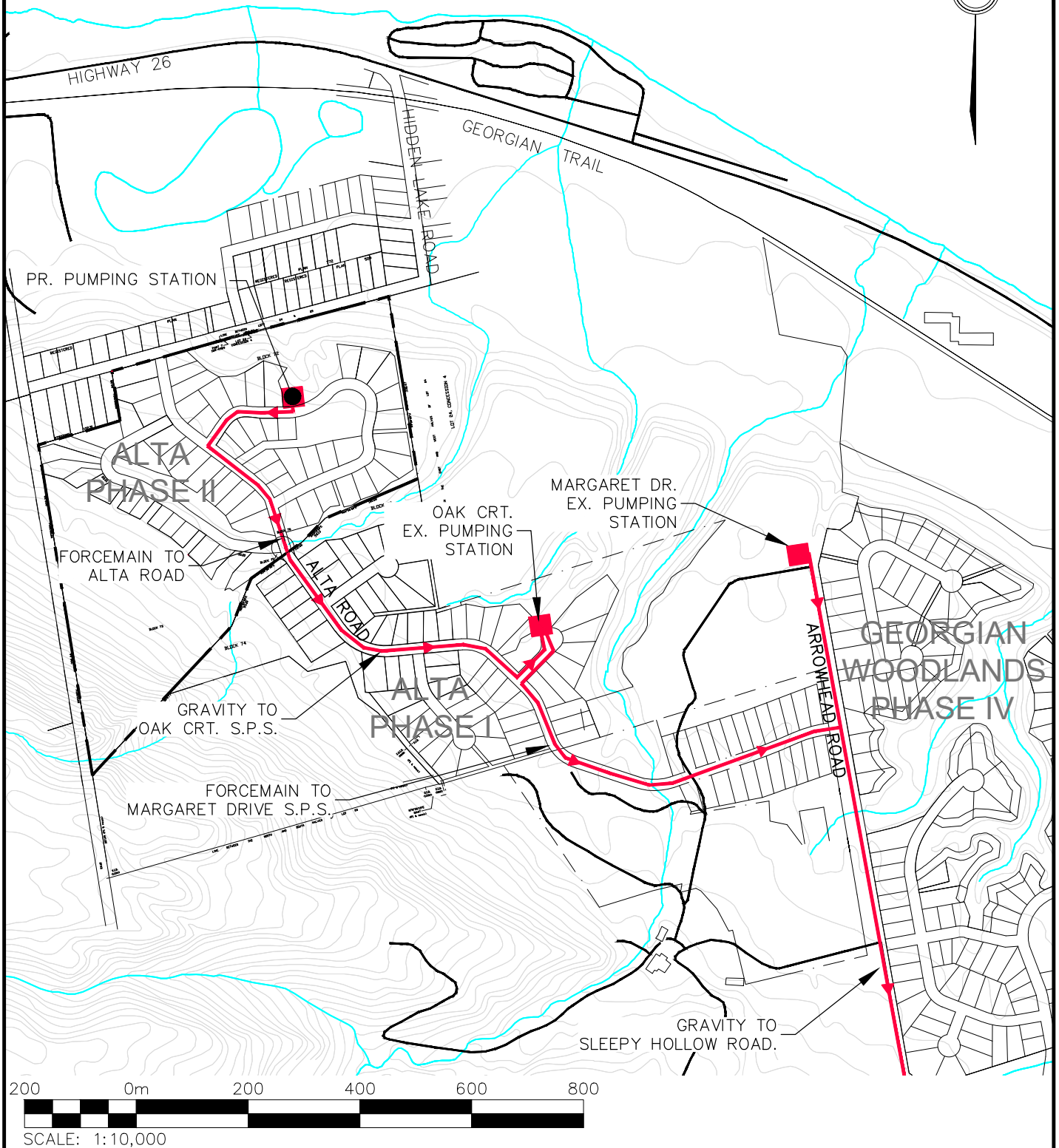
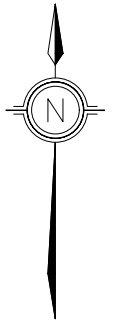
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Drawing	DRAFT PLAN		
Drawn By	J.O.	Check By	Z.H. & G.C.
Scale	1:2500	Date	06/28/2021
Project No.	119-2528-202	Drawing No.	FIG. 2



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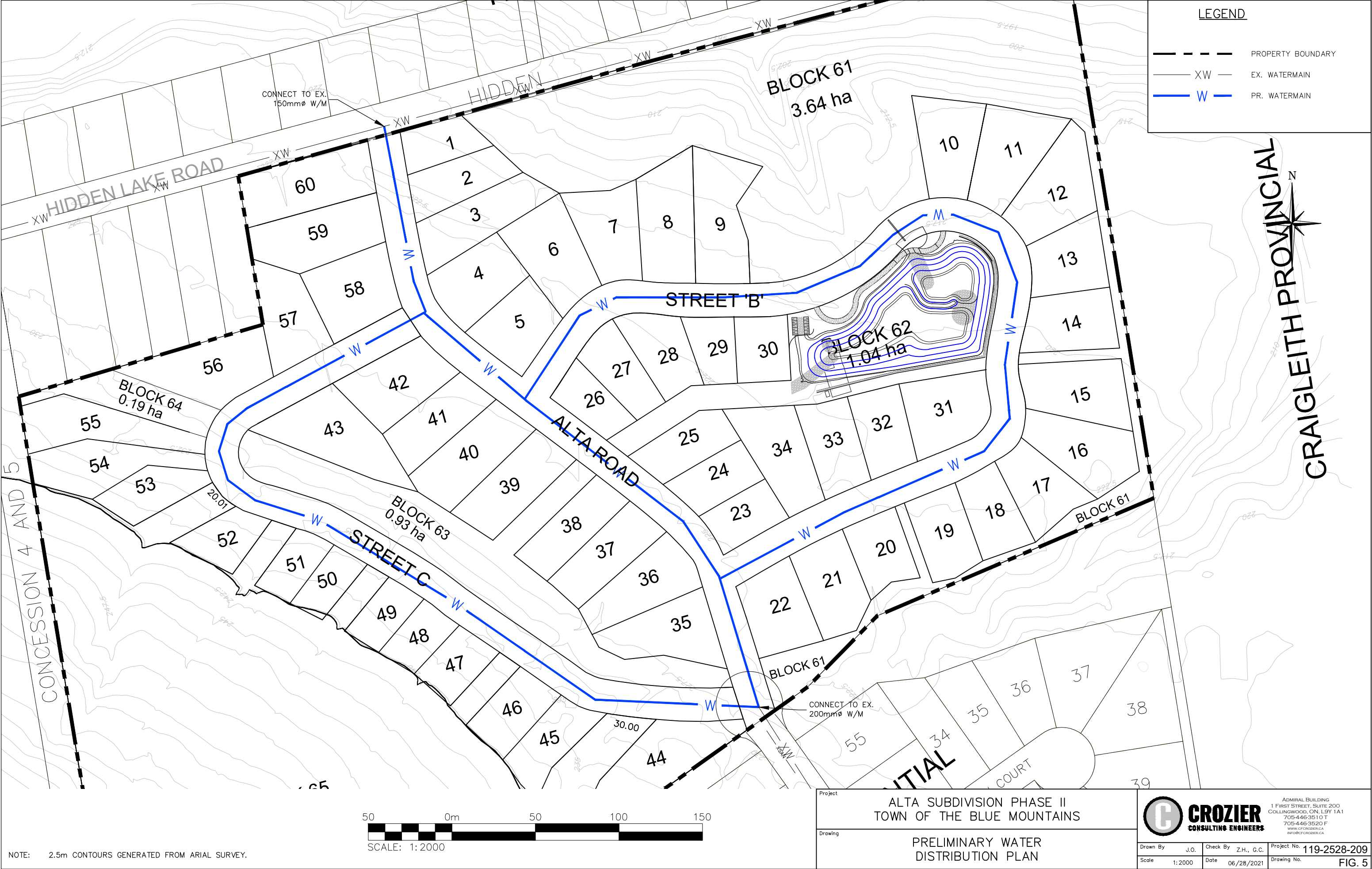
ADMIRAL BUILDING
1 FIRST STREET, SUITE 200
COLLINGWOOD, ON, L9Y 1A1
705-446-3510 T
705-446-3520 F
WWW.CFCROZIER.CA
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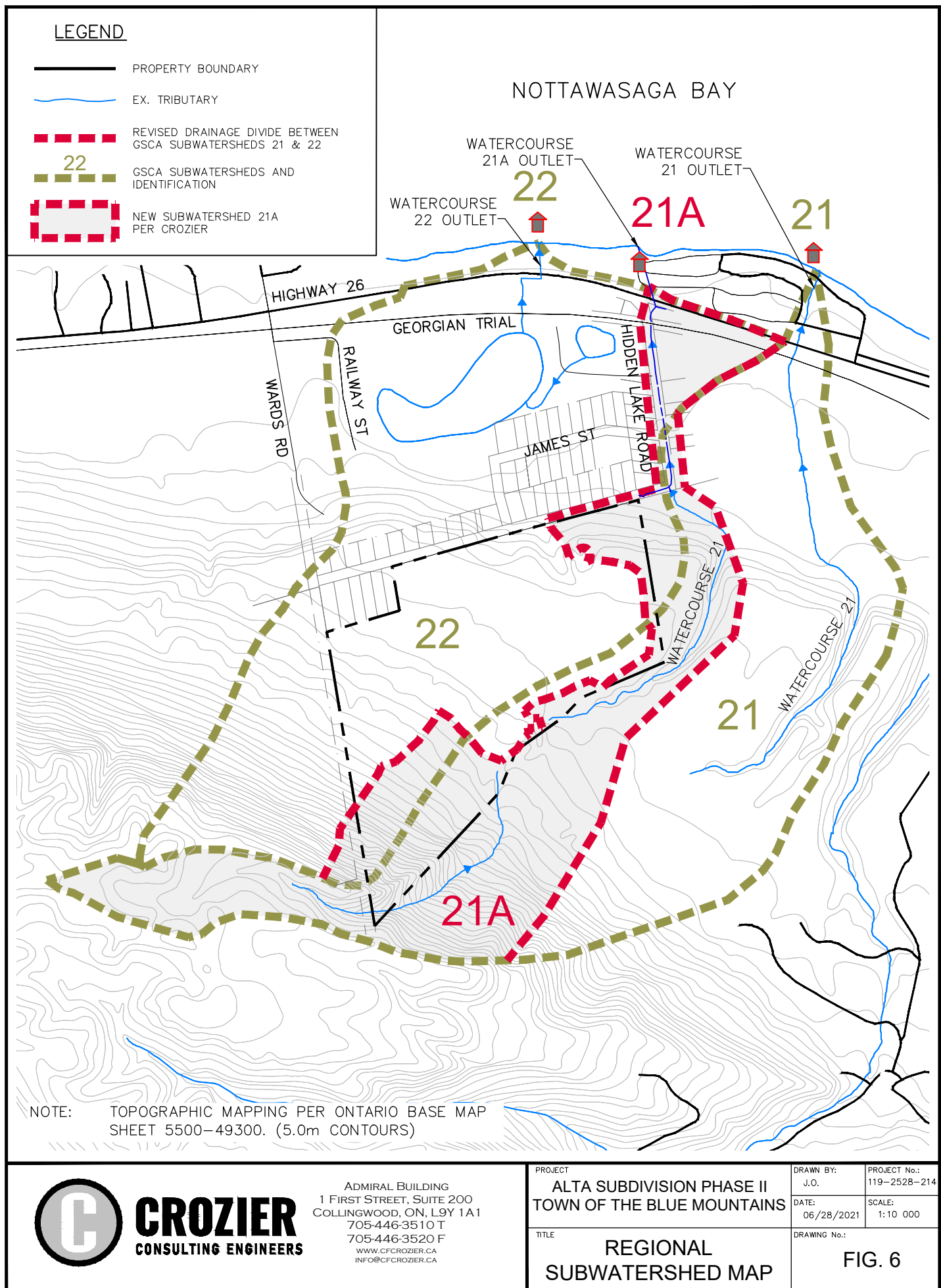
PROJECT
**ALTA SUBDIVISION PHASE II
TOWN OF THE BLUE MOUNTAINS**

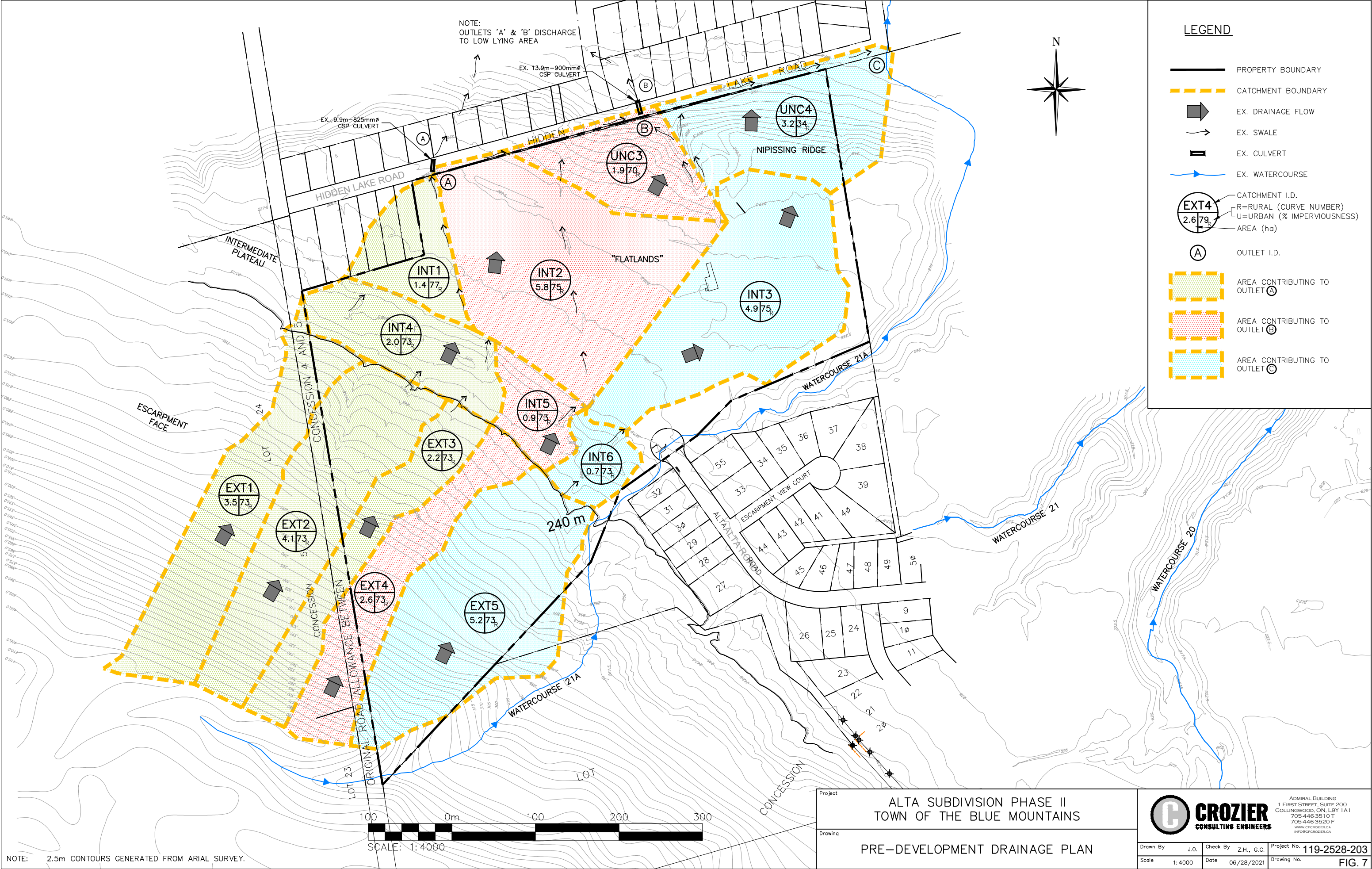
TITLE
**OVERALL SANITARY
DRAINAGE PLAN**

DRAWN BY:
J.O.
DATE:
06/28/2021
PROJECT No.:
119-2528-211
SCALE:
1:10 000

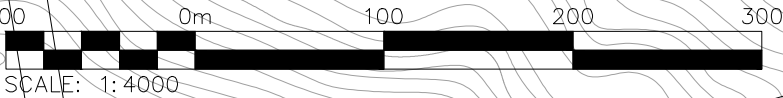
DRAWING No.:
FIG. 4







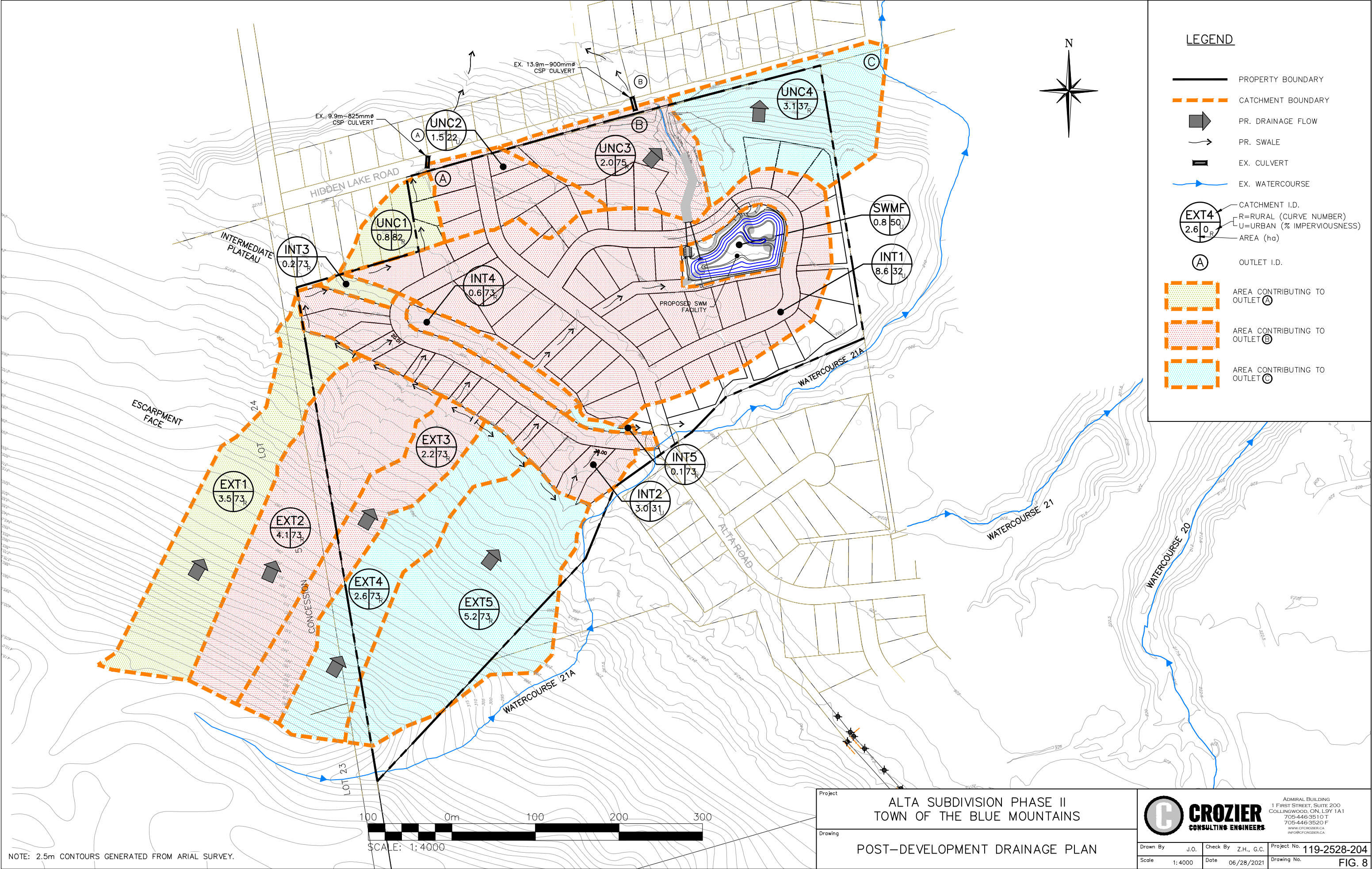
NOTE: 2.5m CONTOURS GENERATED FROM ARIAL SURVEY.

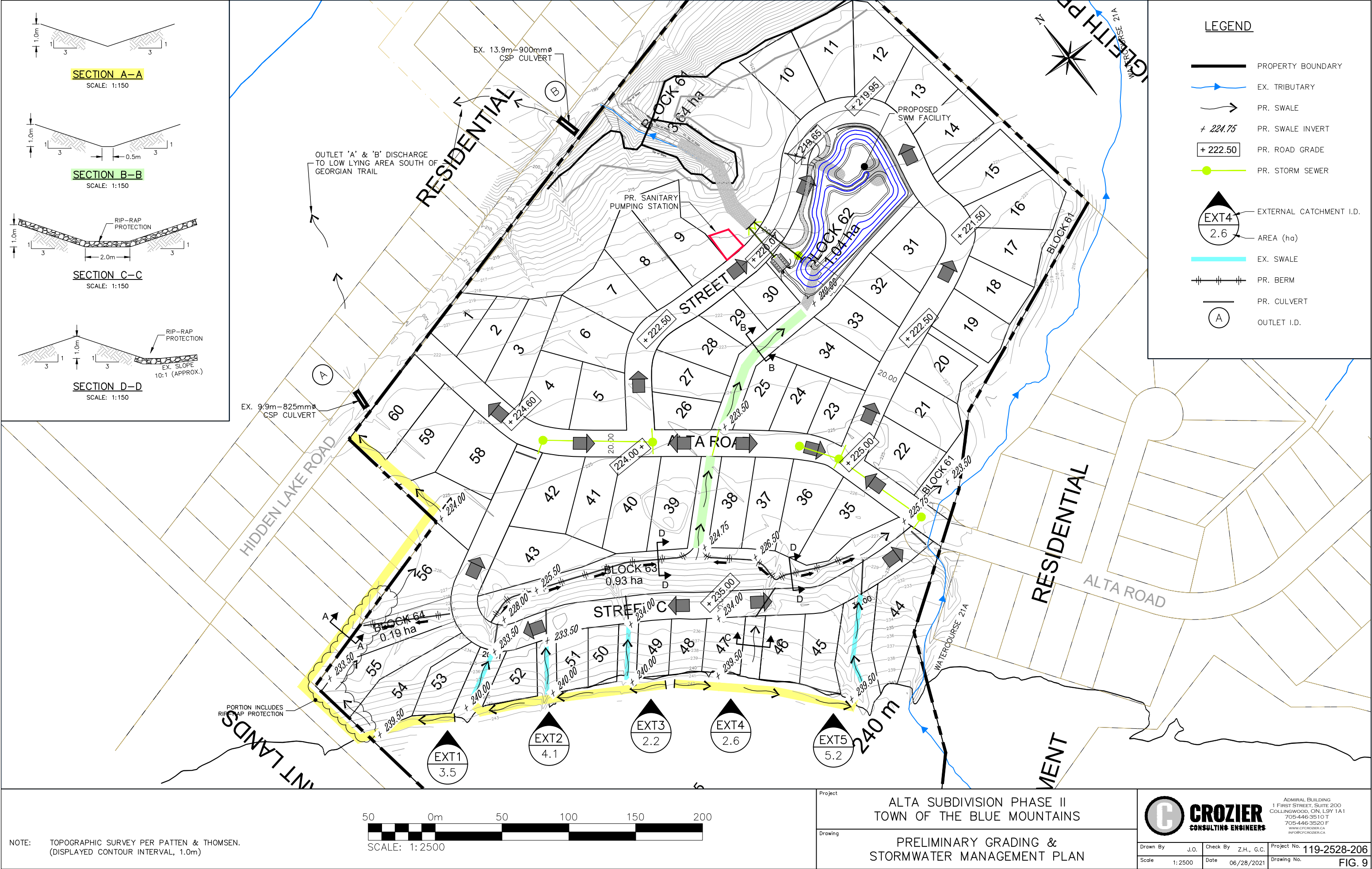


Project		ALTA SUBDIVISION PHASE II TOWN OF THE BLUE MOUNTAINS	
Drawing		PRE-DEVELOPMENT DRAINAGE PLAN	
Drawn By	J.O.	Check By	Z.H., G.C.
Scale	1:4000	Date	06/28/2021
Project No.		119-2528-203	
Drawing No.		FIG. 7	



ADMIRAL BUILDING
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NOTE: TOPOGRAPHIC SURVEY PER PATTEN & THOMSEN.
(DISPLAYED CONTOUR INTERVAL, 1.0m)



Project
ALTA SUBDIVISION PHASE II
TOWN OF THE BLUE MOUNTAINS

Drawing
PRELIMINARY GRADING &
STORMWATER MANAGEMENT PLAN



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Scale	1:2500	Date	06/28/2021	Drawing No.	FIG. 9

