

PRELIMINARY GEOTECHNICAL INVESTIGATION PROPOSED RESIDENTIAL SUBDIVISION **GREY ROAD 21** TOWN OF BLUE MOUNTAINS, ONTARIO for **ROYALTON HOMES INC.**

PETO MacCALLUM LTD. 25 SANDFORD FLEMING DRIVE UNIT 2 COLLINGWOOD, ONTARIO

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PML Ref.: 18CF004 Report: 1

June 2018

Peto MacCallum Ltd.

June 19, 2018 PML Ref.: 18CF004 Report: 1

Mr. Samer Chaaya Royalton Homes Inc. 10114 Highway 26 Unit 4 Collingwood, Ontario L9Y 3Z1

Dear Mr. Chaaya

Preliminary Geotechnical Investigation Proposed Residential Subdivision Grey Road 21 Town of Blue Mountains, Ontario

Peto MacCallum Ltd. (PML) is pleased to present the results of the preliminary geotechnical investigation recently completed at the above noted project site. Authorization for this work was provided by Mr. J. Acres of C.C. Tatham & Associates Ltd. (CCT) in an email dated March 19, 2018, on behalf of the Client.

A 150 to 200 unit residential subdivision is proposed for the approximate 21 ha parcel of land just north of the Scandinave Spa on the west side of Grey Road 21 in the Town of Blue Mountains. A concept plan for the site has not been established at this time, however, full site servicing and paved roads are proposed.

A preliminary geotechnical investigation has been requested to determine the general subsurface conditions at the site, and based on this information, provide preliminary assessment of the geotechnical conditions for preliminary planning and design of the proposed residential subdivision, including earthworks, house foundations, service installation and pavement design.

A limited chemical testing program was included with the geotechnical work to check the geoenvironmental quality of the site soils in order to provide comments regarding on-site reuse or off-site reuse/disposal options for excess excavated soil.

The comments and recommendations provided in this report are based on the site conditions as revealed in a limited number of boreholes and test pits at the time of the investigation. Design is in the conceptual stages and the details of the development plans, including final grades were not available at the time of this study. Accordingly, the comments and recommendations provided in this report are general in nature and suitable only for preliminary design and planning purposes. When design details are available, supplementary investigation and analysis will be required to finalize the geotechnical recommendations.

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INVESTIGATION PROCEDURES

The field work for this investigation consisted of Boreholes 2 to 4, 7 and 8, drilled to 6.2 to 6.5 m depth on April 20 and 23, 2018 and Test Pits 1, 5 and 6, excavated to 2.9 to 3.0 m depth on May 11, 2018. Borehole and Test Pit locations are shown on the Borehole/Test Pit Location Plan,

Drawing 1, appended. It is noted that Boreholes 1, 5 and 6 were inaccessible with a drill rig. Test

pits were carried out at the borehole locations and the numbering system was kept the same.

The locations of the boreholes and test pits were established in the field by PML during a site meeting with the Client and CCT. Co-ordination of clearances of underground utilities was provided by PML. Boreholes were drilled and test pits excavated cognizant of underground

utilities.

The boreholes were advanced using continuous flight solid stem augers, powered by a track mounted D-50 drill rig, equipped with an automatic hammer, supplied and operated by a specialist

drilling contractor working under the full time supervision of a member of our engineering staff.

The test pits were excavated using a track mounted excavator, operated by an excavating

company working for the Client, supervised by a member of our engineering staff.

Representative samples of the subgrade soils in the boreholes were recovered at frequent depth intervals for identification purposes using a conventional split spoon sampler. Standard penetration tests were carried out simultaneously with the sampling operations to assess the strength characteristics of the substrata. The ground water conditions in the boreholes were assessed during drilling by visual examination of the soil samples, the sampler, and drill rods, as the samples were retrieved and measurement of the water level in the open boreholes, if any.

The topsoil thicknesses at the surface in the boreholes were measured.

In the test pits the topsoil thickness was measured and the subsurface soil and ground water

conditions were logged. Samples of the subgrade units were collected for identification purposes.

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Piezometers comprising 19 mm diameter pipe (slots cut in bottom 1.5 m) with filter sand, bentonite seal and above grade protective casing were installed in three of the boreholes. A standpipe comprising 19 mm diameter pipe (slots cut in bottom 1.0 m) and native backfill was installed in one test pit. As per O.Reg. 903, the piezometers and standpipe become the property of the Owner and will have to be decommissioned when no longer required. PML would be pleased to assist in this regard.

A year long ground water level monitoring program is being conducted by PML and results will be provided under separate cover.

The boreholes without piezometers were decommissioned as per O.Reg. 903. The test pits were backfilled with excavated material.

Ground surface elevations of the boreholes and test pits were provided by CCT.

All recovered soil samples were returned to our laboratory for moisture content determinations and detailed examination to confirm field classification. Grain size analyses were carried out on three soil samples with accompanying Atterberg Limits testing. The results are displayed on Figures 1 to 3, appended.

Three soil samples from the boreholes and one from the test pits were submitted for chemical analysis. Geoenvironmental procedural protocols and analytical chemical testing results are presented and discussed later in the report.

SITE DESCRIPTION AND SUMMARIZED SUBSURFACE CONDITIONS

The property is flanked by the Grey Road 21 to the east, a portion of the Monterra golf course to the north, the Scandinave Spa to the south and formerly wooded lots (which have been clear-cut to accommodate new subdivisions) to the west/southwest. A densely wooded unevaluated wetland/creek identified by the Ministry of Natural Resources cuts through the centre of the site. The portion of the site west of the wetland is lightly wooded, while east of the wetland/creek the site comprises farmland. The site has about 8 m of relief, based on the boreholes, dropping from the southwest to the northeast.

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Reference is made to the appended Log of Borehole sheets for details of the subsurface

conditions, including soil classifications, topsoil thicknesses, inferred stratigraphy,

Standard Penetration N values (N-Values), ground water observations, piezometer installation

details and the results of laboratory water content determinations and Atterberg Limits testing.

Reference is also made to the appended Log of Test Pit sheets for details of the subsurface

conditions, including soil classifications, stratigraphy, ground water observations, standpipe

installation details and the results of laboratory water content determinations and Atterberg Limits

testing.

Due to the soil sampling procedures and limited sample size, the depth demarcations on the

borehole logs must be viewed as "transitional" zones between layers, and cannot be construed as

exact geologic boundaries between layers. PML should be retained to assist in defining the

geologic boundaries in the field during construction, if required.

The stratigraphic profile of the site comprises topsoil, locally overlying sand, over a major sand

and silt layer, over clayey sandy silt till, locally underlain by a silt deposit.

<u>Topsoil</u>

A 100 to 400 mm thick layer of silty sand to sand topsoil was encountered at the surface of all

boreholes and test pits.

Sand

A layer of sand with trace to some silt and trace gravel was noted below the topsoil in

Boreholes 4 and 8, at the east end of the site, extending to 2.1 m depth (elevation 205.7 to 207.9).

The layer was very loose to compact (N Values of 3 to 17) and moist to wet with depth, with

moisture contents of 9 to 24%.

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Silt and Sand

Underlying the topsoil, locally the sand unit in the east, a major sand and silt deposit was encountered in all boreholes and test pits, extending to 0.7 to 2.9 m depth (elevation 206.9 to 214.75) in Boreholes 2, 3 and 7 and Test Pits 1, 5 and 6, and to the 6.4 m depth of exploration in Boreholes 4 and 8. The deposit comprised silty fine sand to fine sandy silt, with trace clay and locally some gravel or trace organics noted. A sample of the material was submitted for grain size analysis and the results are presented on Figure 1, appended. Atterberg Limits testing showed the material to be non-plastic. The layer was judged to be loose in the test pits and was revealed as loose to very dense with depth in the boreholes. The unit was typically very moist to wet with depth, with moisture contents ranging from 11 to 24%.

Clayey Sandy Silt Till

Underlying the sand and silt in Boreholes 2 and 7 and Test Pits 1, 5 and 6, a clayey sandy silt till deposit was encountered, being penetrated at 5.5 m depth (elevation 204.3) in Borehole 7, and continuing to the 2.9 to 6.2 m depth of drilling/excavation in Borehole 2 and Test Pits 1, 5 and 6. A sample of the material was submitted for grain size analysis and the results are presented on Figure 2, appended. Accompanying Atterberg Limits testing showed the material to have a plastic limit of 11% and a liquid limit of 19%. The deposit was very stiff to hard (N Values greater than 50 in boreholes). The material was generally drier than plastic limit, locally about plastic limit with water contents of 6 to 13%. Wet layers were noted in the till in the test pits, as seepage was observed.

Silt

A localized deposit of silt was encountered in Boreholes 3 and 7 (central/east part of the site) beneath the till or sand and silt, extending to the 6.4 to 6.5 m depth of exploration. The silt was very dense with N Values greater than 50. A sample of the material was submitted for gradation and the results are presented on Figure 3, appended. Atterberg Limits testing showed the silt to be non-plastic. The material was very moist to moist with water contents of 12 to 18%.

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Ground Water

The first ground water strike (water first noticed during drilling), the water level or wet cave observations in the boreholes/test pits upon completion, and the water levels in the piezometers/standpipe on May 4 and June 11, 2018 are noted in the table below:

		DEPTH (m) / ELE	/ATION	
BOREHOLE / TEST PIT	FIRST GROUND WATER STRIKE	SEEPAGE / WATER / WET CAVE LEVEL UPON COMPLETION	WATER LEVEL IN PIEZOMETERS MAY 4, 2018	WATER LEVEL IN PIEZOMETERS / STANDPIPE JUNE 11, 2018
1	2.9 / 209.8	Seepage at 2.9 / 209.8		
2	1.2 / 209.8	Water at 0.1 / 210.9	-1.0 / 212.0	-0.6 / 211.6
3	0.9 / 208.7	Water at 2.7 / 206.9		
4	2.0 / 205.8	Wet Cave at 1.8 / 206.0	1.2 / 206.6	1.9 / 205.9
5	2.9 / 212.6	Seepage at 2.9 / 212.6		0.5 / 215.0
6	1.0 / 211.0	Seepage at 1.0 / 211.0		
7	0.8 / 209.0	Water at 0.6 / 209.2	0.4 / 209.4	1.2 / 208.6
8	1.5 / 208.5	Water at 1.8 / 208.2		

^{* -} Negative water level is above existing grades.

Ground water was generally encountered within the more pervious sand, or sand and silt deposits, perched within 1 to 2 m of the ground surface, over the less pervious clayey sandy silt till.

The piezometer in Borehole 2 also demonstrates the ground water is locally under some artesian pressure, as evidenced by the water levels noted above existing site grades at this location.

A year-long water level monitoring program has been undertaken in an attempt to gain an appreciation for the seasonal variations of the ground water table. Results will be provided under separate cover.

Ground water levels are subject to seasonal variation and will fluctuate in response to precipitation.

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GEOTECHNICAL ENGINEERING CONSIDERATIONS

General

A 150 to 200 unit residential subdivision is proposed for the approximate 21 ha parcel of land just

north of the Scandinave Spa on the west side of Grey Road 21 in the Town of Blue Mountains. A

concept plan for the site has not been established at this time, however, full site servicing and

paved roads are proposed.

The site is characterized by topsoil, locally overlying sand, over a major sand and silt layer, over

clayey sandy silt till, locally underlain by a silt deposit. Ground water levels were typically perched

within 1 to 2 m of the ground surface. Local artesian ground water is present.

The soils are relatively competent and will provide adequate bearing for residences and other

infrastructure. The high ground water level will impact construction and if basements are

proposed grades will need to be raised.

The comments and recommendations provided in this report are preliminary in nature and are

based on the subsurface conditions as revealed in a limited number of boreholes and test pits at

the site. Details of the development plans, including layout and final grades were not available at

the time of this study. Accordingly, the comments and recommendations provided in this report

are general in nature, and suitable only for preliminary design and planning purposes. When

design details are available, supplementary investigation and analysis will be required to finalize

the geotechnical recommendations.

Site Grading and Engineered Fill

Grading at the site has yet to be established however it is anticipated that some cut/fill operations

will be carried out. The site currently maintains about 8 m of relief, dropping from the southwest to

the northeast.

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Any upfilling under structures must be constructed as engineered fill. Topsoil and very loose to loose soil should be removed and engineered fill can be placed on the native very stiff to hard/compact to very dense soils encountered throughout the site typically below 0.5 to 1.0 m

locally 1.5 m depth. Further recommendations can be provided, if required.

Foundations

House foundations can typically be supported on conventional spread and strip footings founded on the very stiff to hard/compact to very dense native soils typically encountered below 0.5 to

1.0 m depth, locally 1.5 m deep, across the site.

A net geotechnical bearing resistance at Serviceability Limit State (SLS) of 100 to 150 kPa, and a

factored bearing resistance at Ultimate Limit State (ULS) of 150 to 225 kPa are available for

design. Higher bearing capacities are available at increased depths.

Footings can also be supported on engineered fill where a net geotechnical bearing resistance at

SLS of 150 kPa and factored bearing resistance at ULS of 225 kPa can be assumed for design.

The geotechnical bearing resistance at SLS is based on 25 mm or settlement in the bearing

stratum with differential settlement of 75% of the value.

Footings subject to frost action should be provided with a minimum 1.2 m of earth cover or

equivalent.

It is noted that if the subgrade soils are wet in-situ or allowed to become wet due to weather they

will become easily disturbed under construction or pedestrian traffic. If the footing subgrade is

disturbed it will have to be sub-excavated. As such, the contractor should adopt construction

methodology and equipment to suit. Concrete skim coats may be required in some areas.

Prior to placement of structural concrete, all founding surfaces should be reviewed by PML to

verify the design bearing capacity is available, or to reassess the design parameters based on the

actual conditions revealed in the excavation.

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Basement Walls and Floor Slabs

It is currently unknown if basements are planned.

Basement floor slabs should be established a minimum 0.5 m above the ground water level. In

general grades will need to be raised in order to accommodate basements due to the high ground

water levels.

A year long ground water level monitoring program is currently being conducted. Results will be

provided under separate cover.

Basement walls must be designed to resist the unbalanced horizontal earth pressure imposed by the

backfill adjacent to the walls. Also, basement wall backfill should comprise free draining granular

material conforming to OPSS Granular B. Further recommendations can be provided if required.

Basement floor slab-on-grade construction is feasible on native soils or locally engineered fill. In

general, a minimum 150 mm thick base layer of crushed stone (nominal 19 mm size) is

recommended directly under the slab.

Exterior grades should be established to promote surface drainage away from the buildings.

Site Servicing

Design details were not finalized at the time of this report. However for purposes of this report it is

assumed service inverts will be a maximum 3.0 m below existing grade.

Native clayey sandy silt till, silt, or sand and silt is expected at invert levels which is considered

satisfactory for pipe support.

Native backfill is generally satisfactory for trench backfill, however, the high ground water table will

require most of the soil to be dried out in order to achieve compaction.

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Backfill in trenches should comprise select inorganic site soil at a suitable moisture content and be

placed in maximum 200 mm thick loose lifts compacted to at least 95% Standard Proctor

maximum dry density to minimize post construction settlement in the backfill.

Earthworks operations should be inspected by PML to verify subgrade preparation, backfill

materials, placement and compaction efforts and ensure the specified degree of compaction is

achieved throughout.

Excavation and Ground Water Control

Finished site grades are not known at this time.

Excavation is anticipated to a maximum of 3 m depth and will encounter topsoil and the underlying

native sand, sand and silt, and clayey sandy silt till units. Perched ground water is anticipated

within 1 to 2 m of the ground surface. Harder digging and the presence of cobbles and boulders

should be anticipated in the till deposit.

Subject to effective ground water control, the site soils should be considered as Type 3 soil

requiring excavation side walls to be constructed at no steeper than one horizontal to one vertical

(1H:1V) from the base of the excavation in accordance with the Occupational Health and

Safety Act.

In general for excavation to 1.0 to 1.5 m seepage volumes are expected to be handled by

conventional sump pumping techniques. Deeper excavation or excavation adjacent the existing

wetland/creek or in lower lying areas of the site will yield higher seepage volumes which will

necessitate more aggressive ground water control measures such as pumping from keg wells, or

possibly the use of well points.

Excavation should be carried out during the dry time of the year to minimize ground water control

requirements.

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A year-long water level monitoring program has been undertaken in an attempt to gain an appreciation for the seasonal variations of the ground water table. Results will be provided upon its projected completion in April 2019.

Pavement Design and Construction

The location of the roadways have yet to be finalized and grading is still to be determined. Based on the boreholes and test pits, it is anticipated that the pavement subgrade will comprise near surface soil (moderately to highly frost susceptible native sand/sand and silt, typically very moist or wet). The following preliminary pavement structure thicknesses are recommended and should be reviewed when grading/subgrade conditions have been finalized:

	Light Duty (Local Roads)	Heavy Duty (Collector Roads)
Asphalt (mm)	90	110
Granular A Base Course (mm)	150	150
Granular B Subbase Course (mm)	400	600
Total Thickness (mm)	640	860

Geotechnical Review

It is recommended that the final drawings be submitted to PML for general geotechnical review for compatibility with the site conditions and the recommendations provided in this report.

The comments and recommendations provided in the report are based on the site conditions as revealed in a limited number of boreholes and test pits at the time of the investigation. Further, details of the development plans, including layout and final grades were not available at the time of this study. Accordingly, the comments and recommendations provided in this report are general in nature and suitable only for preliminary design and planning purposes. When design details are available, they should be submitted for review by PML to verify the applicability of the recommendations presented in this report and may require additional investigation and/or analysis.

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GEOENVIRONMENTAL CONSIDERATIONS

A limited chemical testing program was carried out to check the geoenvironmental quality of the

soil at selected sampling locations in order to provide comments regarding on site reuse or off-site

disposal options for excess excavated soil.

A Phase One Environmental Site Assessment (ESA) was not within the scope of work for this

assignment. Accordingly, soil impairment that has not been identified by the limited chemical

testing program may exist at the site. The limited chemical testing program does not constitute an

Environmental Site Assessment as defined under the Environmental Protection Act and

O. Reg. 153/04, as amended.

Chemical Testing Protocols

As part of the geoenvironmental procedural protocol, all recovered soil samples were examined

for visual and olfactory evidence of potential contamination. It is noted that none of the samples

contained olfactory evidence of contamination.

The selected geoenvironmental soil samples were placed in laboratory air tight glass containers

and stored in an insulated cooler for transportation to our laboratory for detailed visual

examination.

Soil samples were submitted for chemical analysis to a Canadian Association for Laboratory

Accreditation Inc. (CALA) accredited laboratory. The chemical analyses conducted were in

accordance with the O. Reg. 153/04, as amended Protocol for Analytical Methods Used in the

Assessment of Properties under Part XV.1 of the Environmental Protection Act dated

March 9, 2004, amended as of July 1, 2011.

For general environmental quality characterization, soil samples were tested for the following

analyte groups:

Metals and Inorganics;

Petroleum Hydrocarbons (F1 to F4 fractions).

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The following soil samples were submitted for chemical testing:

Borehole 2 SS 1, (sand and silt – 0.1 to 0.6 m)

Borehole 4 SS 2, (sand – 0.8 to 1.4 m)

Borehole 7 SS 3, (sand and silt – 1.5 to 2.1 m)

Test Pit 5 GS 2, (till – 0.7 to 2.0 m)

Site Condition Standards

In general, the applicable environmental quality guidelines depend on the site location, land use, soil texture and source of potable water at the site. In this regard, PML selected the Generic Criteria of the O. Reg. 153/04, as amended, Soil, Ground Water and Sediment Standards for Use Under Part XV.1 of the Environmental Protection Act dated April 15, 2011.

Based on Sections 41 and 43 of O.Reg. 153/04, as amended, and a review of readily available information, the site is considered a sensitive site. The subject site is considered sensitive due to the presence of an area of natural significance. An unevaluated wetland identified by the Ministry of Natural Resources (MNR), traverses the centre of the site.

Further, the site was reviewed against the County of Grey's Intake Protection Zones (Map 2, June 2013) and other maps for watercourses and private wells as part of the protocol to determine the applicable Site Condition Standards (SCSs) for the site. In this regard, the site is not within an intake protection zone, however, has private drinking water wells within 250 m of the site based on the MOECC well records website, and is within 30 m of a water body as a creek/wetland passes through the middle of the site.

Based on the above reviews, the criteria of Table 1: Full Depth Background Site Condition Standards, Table 1 SCSs, are considered applicable to the site.

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Analytical Findings and Conclusions

The Certificates of Analyses for Chemical Testing are included in Appendix A.

On-Site Reuse

In summary, the concentration of the tested parameters in the submitted soil samples were in conformance with the Table 1 SCSs applicable to the site. Accordingly, based on the testing

results, excavated soil can be reused on-site, subject to geotechnical requirements.

It should be noted that there is no legal imperative to remove or treat soil that exceeds the applicable SCSs provided it is demonstrated that there is no off-site impact or adverse effect. If contaminated soil is left on-site, the landowner assumes liability associated with the site

contamination and potential of off-site contamination. The liability concerns could include

potential scrutiny from the MOECC and the public, potential for decreased value for the land, and

issues during potential divesting of the property due to environmental liability concerns on the part

of the future owners or their financiers/ insurers.

It should also be noted that the soil conditions between and beyond the sampled locations may differ from those encountered during this assignment. PML should be contacted if impacted soil conditions become apparent during future development to further assess and appropriately handle the materials, if any, and evaluate whether modifications to the conclusions documented in this

report are necessary.

This assessment is subject to the Statement of Limitations that is included with this report

(Appendix B) which must be read in conjunction with the report.

Off-Site Reuse/Disposal

O. Reg. 153/04, as amended has nine tables outlining SCSs (Tables 1 to 9) for evaluating

Environmental Soil Characteristics. These tables are further divided based on land use.

The chemical testing results from this project were compared to the various SCSs to evaluate

where the excess soil can be transported.

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Based on the limited chemical testing results the site soil meets the most stringent SCSs (Table 1) and can be transported to any landsite, subject to approval of receiving site authority.

Alternatively, excess excavated soil can be transported to a landfill site, however, additional testing for Toxicity Characteristic Leaching Procedure (TCLP) will be required, in accordance with Ontario Regulation 347, Schedule 4, as amended to Ontario Regulation 558/00, dated March 2001.

When transporting excavated site soil to another site the following are recommended:

- The work must be completed in accordance with local by-laws governing soil movement and/or placement at other sites;
- All analytical results and environmental assessment reports must be fully disclosed to the receiving site owners/authorities and they have agreed to receive the material;
- The applicable SCSs for the receiving site have been determined, as confirmed by the environmental consultant and the SCSs are consistent with the chemical quality of the soil originating at the source site;
- Transportation and placement of the surplus soil is monitored by the environmental consultant to check the material is appropriately placed at the pre-approved site;
- The receiving site must be arranged and/or approved in advance of excavation in order to avoid delays during construction. As well, it is noted the chemical testing requirements for various receiving sites is site-specific and additional testing may be required, beyond that provided in this limited sampling and testing report;
- The excavation work should be conducted in accordance with a written Soil Management Plan prepared by a qualified professional to ensure that all surplus excavated material is tested and managed appropriately, and that imported fill material is of suitable quality and meets the SCSs applicable to the site. Reuse of surplus excavated soil on site is also subject to acceptance for reuse by the geotechnical consultant at the time of construction based on geotechnical considerations;
- Additional sampling and chemical testing should be carried out during construction to verify the chemical quality of the excess soil to assess the appropriate management/disposal options for the actual soil leaving the site;

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• It is recommended that transportation of fill material from the Source Site (s) to the Receiving Site (s) be carried out in accordance with the MOECC document Management of Excess Soil – A Guide for Best Management Practices dated January 2014.

This assessment is subject to the Statement of Limitations that is included with this report (Appendix B) which must be read in conjunction with the report.

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CLOSURE

We trust this report is complete within our terms of reference, and the information presented is sufficient for your present purposes. If you have any questions, or when we may be of further assistance, please do not hesitate to call our office.

Sincerely

Peto MacCallum Ltd.



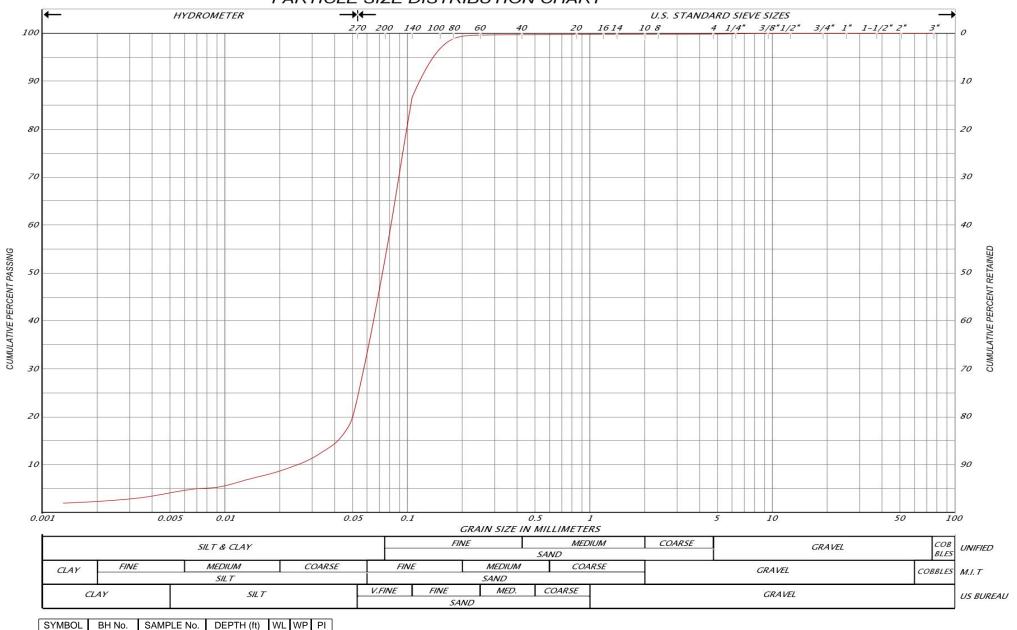
Richard Blair, P.Eng. Project Engineer, Geotechnical Services



Geoffrey R. White, P.Eng. Associate Manager, Geotechnical and Geoenvironmental Services

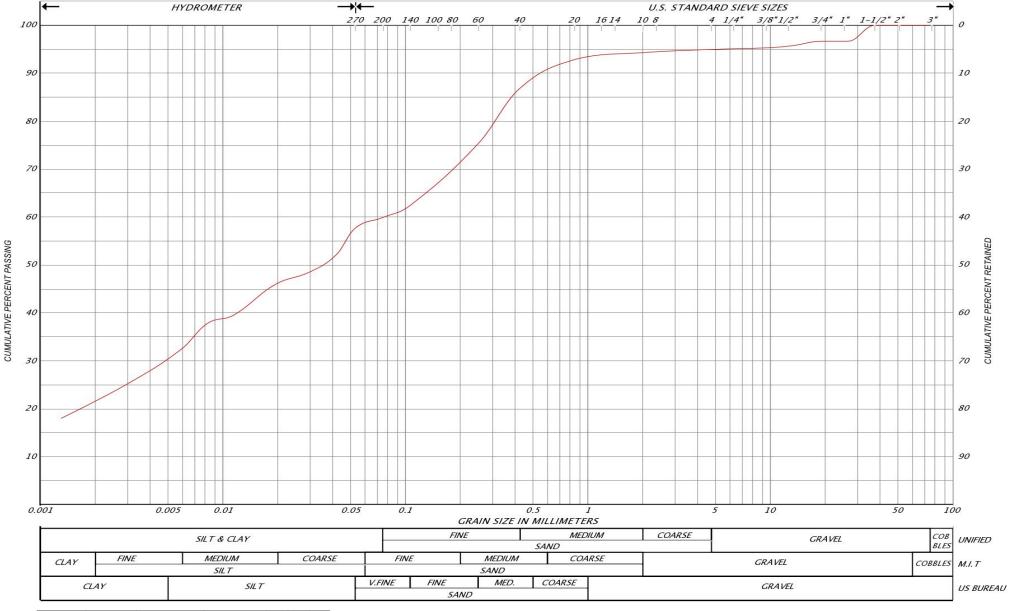
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Enclosure(s):
Figures 1 to 3 – Particle Size Distribution Charts
List of Abbreviations
Log of Test Pit No's 1, 5, 6
Log of Borehole No's 2 to 4, 7, 8
Drawing No. 1 – Borehole/Test Pit Location Plan
Appendix A - Certificates of Analyses for Chemical Testing
Appendix B - Statement of Limitations



REMARKS: Borehole 3, SS 3, 1.5 to 1.9 m depth; SAND AND SILT, Trace Clay; Non-Plastic

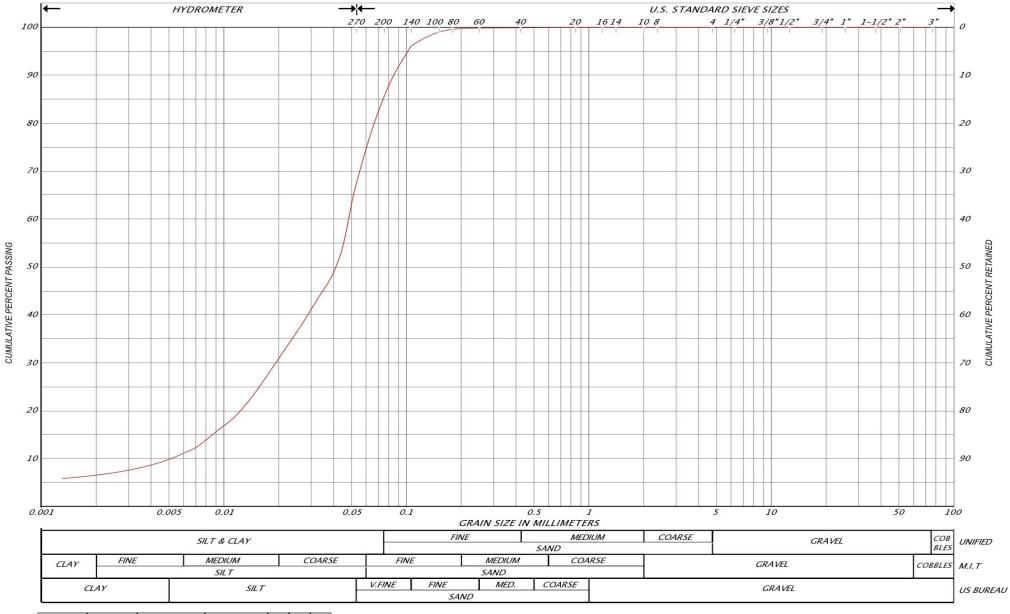




SYMBOL	BH No.	SAMPLE No.	DEPTH (ft)	WL	WP	PI
•	TP5	GS3	2.0-2.9			

REMARKS: Test Pit 5, GS 3, 2.0 to 2.9 m depth; Clayey Sandy Silt Till, Trace Gravel; Plastic Limit: 11%; Liquid Limit: 19%;

PARTICLE SIZE DISTRIBUTION CHART



SYMBOL	BH No.	SAMPLE No.	DEPTH (ft)	WL	WP	PI
•	3	5	10-12			

REMARKS: Borehole 3, SS 5, 3.1 to 3.5 m depth; SILT, Some Sand, Trace Clay; Non-Plastic

LIST OF ABBREVIATIONS



PENETRATION RESISTANCE

Standard Penetration Resistance N: - The number of blows required to advance a standard split spoon sampler 0.3 m into the subsoil. Driven by means of a 63.5 kg hammer falling freely a distance of 0.76 m.

Dynamic Penetration Resistance: - The number of blows required to advance a 51 mm, 60 degree cone, fitted to the end of drill rods, 0.3 m into the subsoil. The driving energy being 475 J per blow.

DESCRIPTION OF SOIL

The consistency of cohesive soils and the relative density or denseness of cohesionless soils are described in the following terms:

CONSISTE	NCY N (blows/0.3 m)	<u>c (kPa)</u>	<u>DENSENESS</u>	N (blows/0.3 m)
Very Soft	0 - 2	0 - 12	Very Loose	0 - 4
Soft	2 - 4	12 - 25	Loose	4 - 10
Firm	4 - 8	25 - 50	Compact	10 - 30
Stiff	8 - 15	50 - 100	Dense	30 - 50
Very Stiff	15 - 30	100 - 200	Very Dense	> 50
Hard	> 30	> 200		
WTLL	Wetter Than Liquid Limit			
WTPL	Wetter Than Plastic Limit			
APL	About Plastic Limit			
DTPL	Drier Than Plastic Limit			

TYPE OF SAMPLE

SS	Split Spoon	ST	Slotted Tube Sample
WS	Washed Sample	TW	Thinwall Open
SB	Scraper Bucket Sample	TP	Thinwall Piston
AS	Auger Sample	OS	Oesterberg Sample
CS	Chunk Sample	FS	Foil Sample
GS	Grab Sample	RC	Rock Core
	PH Sample Advanced	l Hydraulica	lly

PH Sample Advanced Hydraulically
PM Sample Advanced Manually

SOIL TESTS

Qu	Unconfined Compression	LV	Laboratory Vane
Q	Undrained Triaxial	FV	Field Vane
Qcu	Consolidated Undrained Triaxial	С	Consolidation
Qd	Drained Triaxial		

PML-GEO-508A Rev. 2018-05



LOG OF TEST PIT NO. 1

17T 556100E 4926096N

PROJECT Proposed Residential Subdivision

LOCATION Grey Road 21, Town of Blue Mountains, Ontario

BORING DATE May 11, 2018

PML REF. 18CF004

ENGINEER GW

1 of 1

EXCAVATION METHOD Excavator TECHNICIAN AT

E	XCAV	ATION METHOD Excavator				100 100 100	_	_						-			CHNIC	CIAN	AT
	_	SOIL PROFILE	Γ.		SAM	PLES	CALE	SHE +F	EAR STR IELD VAN OCKET P	ENGTI E ATO	H (kPa) RVANE	○ Qu	PLAS	TIC N	ATUR/ DISTU	AL L	JQUID LIMIT	눞	GROUND WATER
DEF EL (met	EV	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES	ELEVATION SCALE	DYN STA	50 1 IAMIC CO	00 1	50 2	00	W _P ⊢	ATER			W _L	UNIT WEIGHT	OBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION (%) GR SA SI&CL
0.0		JRFACE ELEVATION 212.70	XX855.0				ш					30	1	0 2	0 3	0 4	40	kN/m ³	GR SA SI&CL
	30 TC	DPSOIL: Black, silty sand, trace gravel,	~~~																
212	40 100	ry moist AND AND SILT: Loose, brown to grey,		1	GS								1	h					
0.8	80 sil	ty fine sand to fine sandy silt, trace			0.5		212	-	+	-	-	-	-					1	
1.0 - 211	.90 Cla	ay, moist to very moist																	
đ	ha	AYEY SANDY SILT TILL: Very stiff to											1						
7	gra	rd, brown, clayey sandy silt, tráce avel, cobbles and boulders, DTPL		2	GS	-	044						l	Þ					
.]							211												
2.0 - 2.	.2							6											
210	0.5 Be	ecoming grey, APL, wet layers																4	
=				3	GS	-	210		-	-	-		_	0					
3.0	.0	OT DIT TEDMINATED AT CO.	9/12																
209	9.7 TE	ST PIT TERMINATED AT 3.0 m											i						Upon completion of test pit Seepage at 2.9 m
-1																			No sidewall sloughing
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LOG OF BOREHOLE NO. 2 1 of 1 17T 556219E 4928139N PROJECT Proposed Residential Subdivision PML REF. 18CF004 LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE April 23, 2018 **ENGINEER** GW BORING METHOD Continuous Flight Solid Stem Augers TECHNICIAN AT SHEAR STRENGTH (kPa) SOIL PROFILE SAMPLES PLASTIC NATURAL LIQUID LIMIT CONTENT LIMIT +FIELD VANE △TORVANE ○ Qu **GROUND WATER** UNIT WEIGHT ▲ POCKET PENETROMETER O Q STRAT PLOT VALUES **OBSERVATIONS** NUMBER w 100 DEPTH 150 200 TYPE DESCRIPTION AND REMARKS ELEV DYNAMIC CONE PENETRATION STANDARD PENETRATION TEST GRAIN SIZE DISTRIBUTION (%) ž WATER CONTENT (%) 40 10 20 30 SURFACE ELEVATION 210.95 N/m GR SA SI&CL 0.10 TOPSOIL: Dark brown, sand, trace silt, Stick-up casing trace gravel, wet 11 SS 8 0 Concrete SAND AND SILT: Loose to very dense, brown, silty fine sand to fine sandy silt, 1.0 2 SS 25 210 First water strike at 1.2 m 3 Bentonite Seal SS 41 0 209 2.0 74/290mm SS 3.0 CLAYEY SANDY SILT TILL: Hard, grey, SS 50/140mm 0 clayey sandy silt, trace gravel, cobbles and boulders, DTPL 19 mm slotted pipe 207 4.0 Filter sand SS 92/270mm 0 206 5.0 6.0 SS 50/140mm 0 204.8 BOREHOLE TERMINATED AT 6.2 m Upon completion of augering Water at 0.1 m Cave at 4.9 m Date Depth Elev. 2018-05-04 -1.0 212.0 7.0 2018-06-11 -0.6 211.6 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 NOTES 1 - Sample submitted for chemical testing. PML - BH LOG GEO/ENV WITH MWS 18CF004 2018-06-19 BH LOGS.GPJ ON_MOT.GDT 19/06/2018 11:14:10 AM



LOG OF BOREHOLE NO. 3 1 of 1 17T 556392E 4928194N PROJECT Proposed Residential Subdivision PML REF. 18CF004 LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE April 23, 2018 **ENGINEER** GW BORING METHOD Continuous Flight Solid Stem Augers TECHNICIAN AT SHEAR STRENGTH (kPa) SOIL PROFILE SAMPLES PLASTIC NATURAL MOISTURE LIMIT CONTENT LIQUID LIMIT +FIELD VANE △TORVANE ○ Qu UNIT WEIGHT GROUND WATER ▲ POCKET PENETROMETER O Q STRAT PLOT VALUES **OBSERVATIONS** NUMBER W 100 150 200 DEPTH AND REMARKS DESCRIPTION ELEV DYNAMIC CONE PENETRATION STANDARD PENETRATION TEST GRAIN SIZE DISTRIBUTION (%) GR SA SI&CL z WATER CONTENT (%) 40 60 10 20 30 SURFACE ELEVATION 209.55 0.16 TOPSOIL: Black to dark brown, silty sand, trace gravel, very moist SAND AND SILT: Loose to dense, brown to grey, silty fine sand to fine sandy silt, SS 1 0 trace clay, very moist to wet 2 SS 40 1.0 First water strike at 0.9 m. 3 SS 34 Non plastic 2.0 207.5 SILT: Very dense, grey, silt, some sand, trace clay, very moist to moist 4 SS 68 3.0 5 SS 65 Non plastic 206 4.0 77/295mm 0 5.0 204 6.0 7 95/290mm SS 203.2 BOREHOLE TERMINATED AT 6.4 m Upon completion of augering Cave at 3.3 m 7.0 8.0 9.0 10.0 12.0 13.0 14.0 NOTES PML - BH LOG GEO/ENV WITH MWS 18CF004 2018-06-19 BH LOGS.GPJ ON_MOT.GDT 19/06/2018 11:14:11 AM



LOG OF BOREHOLE NO. 4 1 of 1 17T 556543E 4928249N PROJECT Proposed Residential Subdivision PML REF. 18CF004 LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE April 20, 2018 **ENGINEER** GW BORING METHOD Continuous Flight Solid Stem Augers TECHNICIAN AT SHEAR STRENGTH (kPa) SOIL PROFILE SAMPLES +FIELD VANE △TORVANE ○ Qu PLASTIC MOISTURE LIQUID LIMIT CONTENT **GROUND WATER** UNIT WEIGH STRAT PLOT VALUES **OBSERVATIONS** NUMBER w DEPTH 100 150 200 TYPE DESCRIPTION AND REMARKS DYNAMIC CONE PENETRATION STANDARD PENETRATION TEST (metres GRAIN SIZE DISTRIBUTION (%) ż WATER CONTENT (%) SURFACE ELEVATION 207.80 40 60 10 20 30 kN/m 0.12 TOPSOIL: Black to dark brown, silty GR SA SI&CL 0.0 Stick-up casing Concrete sand, trace gravel, moist SS 1 SAND: Loose to compact, brown, sand, trace silt, trace gravel, moist to wet 207 Bentonite Seal 1.0 21 SS 5 SS 17 206 2.0 SAND AND SILT: Dense to very dense, brown, silty fine sand to fine sandy silt, First water strike at 205.7 2.0 m trace clay, very moist to wet 4 SS 33 205 19 mm slotted pipe 3.0 Filter sand 5 SS 41 204 4.0 SS 83/290mm 5.0 202 6.0 SS 72/290mm 201.4 BOREHOLE TERMINATED AT 6.4 m Upon completion of augering Wet cave at 1.8 m 7.0 Water Level Readings: Depth Elev. 2018-05-04 1.2 206.6 205.9 2018-06-11 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 NOTES 1 - Sample submitted for chemical testing. PML - BH LOG GEO/ENV WITH MWS 18CF004 2018-06-19 BH LOGS.GPJ ON_MOT.GDT 19/06/2018 11:14:12 AM



LOG OF TEST PIT NO. 5 1 of 1 17T 556151E 4927968N PROJECT Proposed Residential Subdivision PML REF. 18CF004 LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE May 11, 2018 **ENGINEER** GW **EXCAVATION METHOD** Excavator TECHNICIAN AT SHEAR STRENGTH (kPa) SAMPLES SOIL PROFILE +FIELD VANE △TORVANE ○ Qu PLASTIC MOISTURE LIMIT CONTENT LIQUID LIMIT UNIT WEIGHT **GROUND WATER** ▲ POCKET PENETROMETER OQ STRAT PLOT **OBSERVATIONS** VALUES NUMBER W ELEVATION 50 100 150 200 AND REMARKS DESCRIPTION ELEV DYNAMIC CONE PENETRATION X STANDARD PENETRATION TEST GRAIN SIZE DISTRIBUTION (%) metres WATER CONTENT (%) ż 40 10 20 30 40 60 80 SURFACE ELEVATION 215.45 kN/m GR SA SI&CL 0.0 TOPSOIL: Black to brown, silty sand, 0.30 215.15 trace gravel, very moist to wet 215 SAND AND SILT: Loose, brown, silty fine 1 GS 0.70 214.75 sand to fine sandy silt, some gravel, trace Native backfill organics, wet 1.0 CLAYEY SANDY SILT TILL: Very stiff to 21 GS hard, brown, clayey sandy silt, trace gravel, cobbles and boulders, DTPL 214 2.0 213.5 Becoming grey, wet layers 2.0 19 mm slotted pipe 3 GS 213 212.6 TEST PIT TERMINATED AT 2.9 m Upon completion of test pit Seepage at 2.9 m No sidewall sloughing 3.0 Water Level Readings: Date 2018-06-11 Depth 0.5 4.0 5.0 6.0 7.0 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 NOTES 1 - Sample submitted for chemical testing.



LOG OF TEST PIT NO. 6

17T 556249E 4927986N

PML REF.

1 of 1

PROJECT Proposed Residential Subdivision LOCATION Grey Road 21, Town of Blue Mountains, Ontario

BORING DATE May 11, 2018

18CF004 **ENGINEER** GW

EXCAVATION METHOD Excavator

TECHNICIAN AT

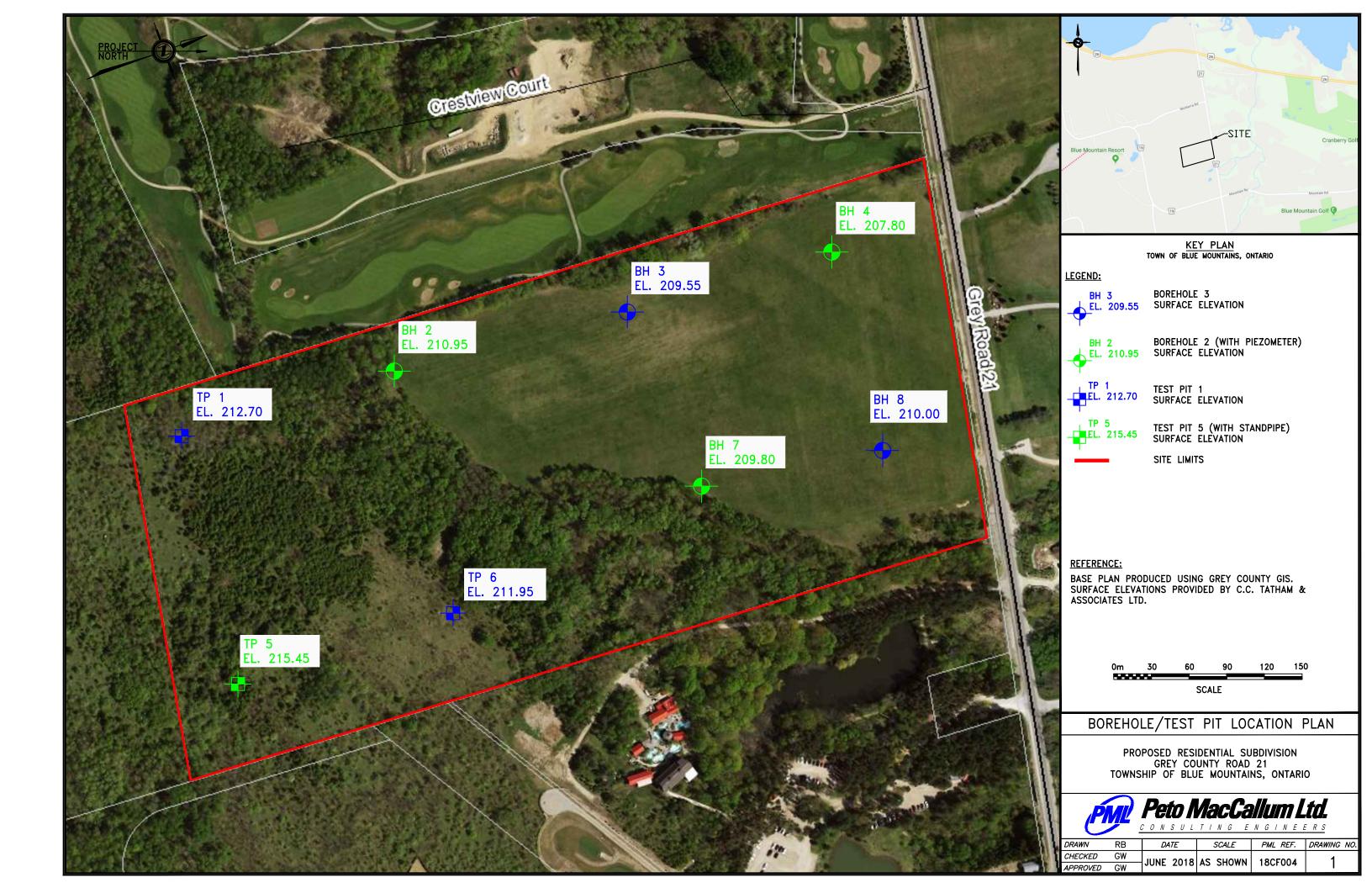
	EXCA	VATION METHOD Excavator					_	_					_			TEC	CHNIC	IAN	AT
		SOIL PROFILE			SAME	PLES	Щ	S	HEAR STR	ENGTH	(kPa)	O 0	DI AC	TIC N	ATURA	AL .	.IQUID		
	DEPTH ELEV	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES	ELEVATION SCALE	4	+FIELD VAN POCKET PI 50 1		METER 50 20		LIMIT W _P	CC	DISTU DISTU W ————	RE L	LIMIT W _L	UNIT WEIGHT	GROUND WATER OBSERVATIONS AND REMARKS
	(metres)		L A	NC	}	>	LA/	D	YNAMIC CO TANDARD P	NE PENI	ETRATION	ON ×	w	ATER	CONT	ENT (%)	N S	GRAIN SIZE
		SURFACE ELEVATION 211.95	S			۴	E	1				80		0 2				kN/m ³	GRAIN SIZE DISTRIBUTION (%) GR SA SI&CL
0.0		TOPSOIL: Black, sand, some silt, trace	~~~					+											
			~~~				-												
	0.80	gravel, very moist  SAND AND SILT: Loose, brown, silty fine sand to fine sandy silt, trace gravel, very		1	GS									0					
1.0	211.15	moist	1997				211	1	_				-						
2		CLAYEY SANDY SILT TILL: Very stiff to																	
-		hard, grey, clayey sandy silt, trace gravel, cobbles and boulders, DTPL, wet layers		- 111															
20				2	GS	198	210	ما					0						
2.0																			
_																			
=	2.9																		
3.0		TEST PIT TERMINATED AT 2.9 m																	Upon completion of augering Seepage at 1.0 m
=																			Sidewall sloughing at 1.0 m
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#### LOG OF BOREHOLE NO. 7 1 of 1 17T 556448E 4928075N PROJECT Proposed Residential Subdivision PML REF. 18CF004 LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE April 23, 2018 **ENGINEER** GW BORING METHOD Continuous Flight Solid Stem Augers TECHNICIAN AT SHEAR STRENGTH (kPa) SOIL PROFILE SAMPLES +FIELD VANE △TORVANE ○ QU PLASTIC MOISTURE A POCKET PENETROMETER ○ Q LIQUID LIMIT UNIT WEIGHT **GROUND WATER** ▲ POCKET PENETROMETER O Q STRAT PLOT VALUES **OBSERVATIONS** NUMBER w ELEVATION 150 200 AND REMARKS TYPE DESCRIPTION ELEV DYNAMIC CONE PENETRATION STANDARD PENETRATION TEST GRAIN SIZE DISTRIBUTION (%) GR SA SI&CL Z WATER CONTENT (%) 40 60 80 10 20 30 40 SURFACE ELEVATION 209.80 0.15 TOPSOIL: Dark brown, silty sand, trace Stick-up casing 209.65 gravel, moist 1 SS 4 Concrete SAND AND SILT: Loose to very dense, Bentonite seal brown, silty fine sand to fine sandy silt, trace clay, very moist to wet First water strike at 1.0 2 SS 25 0.8 m 31 SS 32 208 2.0 19 mm slotted pipe 4 SS 75/270mm 0 Filter sand 3.0 206.9 CLAYEY SANDY SILT TILL: Hard, clayey SS 50/145mm sandy silt, trace gravel, cobbles and boulders, DTPL 206 4.0 68/295mm 6 SS 5.0 SILT: Very dense, grey, silt, trace sand, 204.3 trace clay, moist 6.0 7 SS BOREHOLE TERMINATED AT 6.5 m 203.3 Upon completion of augering Water at 0.6 m 7.0 Cave at 3.3 m Water Level Readings: Depth Elev. 0.4 209.4 Date 2018-05-04 2018-06-11 12 208 6 8.0 9.0 10.0 12.0 13.0 14.0 NOTES 1 - Sample submitted for chemical testing. PML - BH LOG GEO/ENV WITH MWS 18CF004 2018-06-19 BH LOGS GPJ ON MOT GDT 19/06/2018 11:14:14 AM



#### LOG OF BOREHOLE NO. 8 1 of 1 17T 556575E 4928104N PML REF. 18CF004 PROJECT Proposed Residential Subdivision LOCATION Grey Road 21, Town of Blue Mountains, Ontario BORING DATE April 23, 2018 **ENGINEER** GW TECHNICIAN AT BORING METHOD Continuous Flight Solid Stem Augers SHEAR STRENGTH (kPa) SOIL PROFILE SAMPLES +FIELD VANE △TORVANE ○ QU PLASTIC NATURAL MOISTURE LIMIT CONTENT LIQUID LIMIT WEIGHT **GROUND WATER** ▲ POCKET PENETROMETER O Q VALUES **OBSERVATIONS** STRAT PLOT NUMBER 150 W DEPTH ELEV TYPE AND REMARKS DESCRIPTION UNIT DYNAMIC CONE PENETRATION × STANDARD PENETRATION TEST GRAIN SIZE DISTRIBUTION (%) GR SA SI&CL WATER CONTENT (%) Z 20 30 40 60 80 10 40 SURFACE ELEVATION 210.00 0.0 0.14 TOPSOIL: Brown, sand, trace silt, trace gravel, moist 1 SS 3 SAND: Very loose to compact, brown, sand, trace to some silt, trace gravel, very moist to wet 2 SS 12 1.0 First water strike at 1.5 m 3 SS 13 2.0 309 SAND AND SILT: Very dense, brown, silty fine sand to fine sandy silt, very 4 SS 56 moist to wet 3.0 5 SS 75 4.0 SS 83/270mm 5.0 6.0 0 SS 83/270mm Upon completion of augering Water at 1.8 m 203.6 BOREHOLE TERMINATED AT 6.4 m Cave at 2.7 m 7.0 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 NOTES



PML Ref.: 18CF004, Report: 1 June 19, 2018



# **APPENDIX A**

Certificates of Analyses for Chemical Testing



Final Report

C.O.C.: G75184

REPORT No. B18-10833 (i)

Rev. 1

Report To:

Peto MacCallum Ltd

19 Churchill Drive, Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18

DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

**Caduceon Environmental Laboratories** 

112 Commerce Park Drive

Barrie ON L4N 8W8

Tel: 705-252-5743

Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER:

18CF004

WATERWORKS NO.

Parameter	Qty	Site Analyzed	Analyst Initials	Date Analyzed	Lab Method	Reference Method
Cyanide	3	Kingston	US	01-May-18	A-CN s K	in house
Conductivity	3	Richmond Hill	ABL	30-Apr-18	A-COND-02 s RH	MOEE3138
рН	3	Richmond Hill	ABL	27-Apr-18	A-pH-02 (rh)	MOEE 3137
Chromium (VI)	3	Richmond Hill	ABL	01-May-18	D-CrVI-02 s RH	EPA3060A
Mercury	3	Holly Lane	PBK	27-Apr-18	D-HG-01 (o)	EPA 7471A
Sodium Adsorption Ratio	3	Holly Lane	TPR	27-Apr-18	D-ICP-01 SAR (o)	SM 3120
Metals - ICP-OES	3	Holly Lane	TPR	27-Apr-18	D-ICP-02 (o)	EPA 6010
Metals - ICP-MS	3	Holly Lane	RPE	27-Apr-18	D-ICPMS-01 (o)	EPA 6020

μg/g = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in μg/g, (F1-btex if requested)

F2 C10-C16 hydrocarbons in µg/g, (F2-napth if requested)

F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)

F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is

validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

nC6 and nC10 response factor is within 30% of response factor for toluene:

nC10,nC16 and nC34 response factors within 10% of each other:

C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

Unless otherwise noted all extraction, analysis, QC requirements and limits for holding time were met. If analyzed for F4 and F4G they are not to be summed but the greater of the two numbers are to be used in application to the CWS PHC

QC will be made available upon request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an  * 

Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie

Christine Burke Lab Manager

The analytical results reported herein refer to the samples as received. Reproduction of this analytical report in full or in part is prohibited without prior consent from Caduceon Environmental Laboratories.



Final Report

C.O.C.: G75184

REPORT No. B18-10833 (i)

Rev. 1

Report To:

Peto MacCallum Ltd 19 Churchill Drive, Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18

DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

**Caduceon Environmental Laboratories** 

112 Commerce Park Drive Barrie ON L4N 8W8 Tel: 705-252-5743 Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER:

18CF004

WATERWORKS NO.

	Client I.D.		BH 2 SS 1	BH 4 SS 2	BH 7 SS 3	O. Reg. 153
	Sample I.I	<b>)</b> .	B18-10833-1	B18-10833-2	B18-10833-3	Tbl. 1 - All
	Date Colle	cted	23-Apr-18	20-Apr-18	23-Apr-18	
Parameter	Units	R.L.				
pH @25°C	pH Units		7.37	7.86	7.95	
Conductivity @25°C	mS/cm	0.07	0.11	0.07	0.09	0.57
Cyanide (Free)	μg/g	0.05	< 0.05	< 0.05	< 0.05	0.051
Sodium Adsorption Ratio	units		0.127	0.0571	0.0877	2.4
Antimony	µg/g	0.5	< 0.5	< 0.5	< 0.5	1.3
Arsenic	µg/g	0.5	1.2	0.8	0.6	18
Barium	µg/g	1	27	9	12	220
Beryllium	µg/g	0.2	0.2	< 0.2	< 0.2	2.5
Boron	µg/g	0.5	4.1	2.9	4.4	36
Cadmium	μg/g	0.5	< 0.5	< 0.5	< 0.5	1.2
Chromium	µg/g	1	11	5	7	70
Chromium (VI)	µg/g	0.5	< 0.5	< 0.5	< 0.5	0.66
Cobalt	µg/g	1	3	2	3	21
Copper	µg/g	1	9	5	9	92
Lead	µg/g	5	12	< 5	< 5	120
Mercury	µg/g	0.005	0.028	0.005	< 0.005	0.27
Molybdenum	µg/g	1	< 1	< 1	<1	2
Nickel	μg/g	1	6	5	5	82
Selenium	μg/g	0.5	< 0.5	< 0.5	< 0.5	1.5
Silver	μg/g	0.2	< 0.2	< 0.2	< 0.2	0.5
Thallium	μg/g	0.1	< 0.1	< 0.1	< 0.1	1
Uranium	μg/g	0.1	0.5	0.3	0.4	2.5
Vanadium	μg/g	1	18	10	12	86
Zinc	μg/g	3	24	11	14	290

¹ Revised report to change guidelines as per client request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an * Site Analyzed=K-Kingston,W-Windsor,O-Ottawa,R-Richmond Hill,B-Barrie

Christine Burke Lab Manager



Final Report

C.O.C.: G75184

REPORT No. B18-10833 (i)

Rev. 1

Report To:

Peto MacCallum Ltd 19 Churchill Drive, Barrie ON L4N 8Z5 Attention: Geoff White

DATE RECEIVED: 25-Apr-18
DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories

112 Commerce Park Drive Barrie ON L4N 8W8 Tel: 705-252-5743 Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER:

18CF004

WATERWORKS NO.

**Summary of Exceedances** 

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an  *  Site Analyzed=K-Kingston,W-Windsor,O-Ottawa,R-Richmond Hill,B-Barrie

Christine Burke Lab Manager



Final Report

C.O.C.: G75184

REPORT No. B18-10833 (ii)

Rev. 1

Report To:

Peto MacCallum Ltd

19 Churchill Drive,

Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18

DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

**Caduceon Environmental Laboratories** 

112 Commerce Park Drive

Barrie ON L4N 8W8

Tel: 705-252-5743

Fax: 705-252-5746

JOB/PROJECT NO .:

P.O. NUMBER:

18CF004

WATERWORKS NO.

Parameter	Qty	Site Analyzed	Analyst Initials	Date Analyzed	Lab Method	Reference Method
% Moisture	3	Richmond Hill	FAL	26-Apr-18	A-% moisture RH	
PHC(F2-F4)	3	Kingston	KPR	26-Apr-18	C-PHC-S-001 (k)	CWS Tier 1
PHC(F1)	3	Richmond Hill	FAL	26-Apr-18	C-VPHS-01 (rh)	CWS Tier 1

μg/g = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in µg/g, (F1-btex if requested)

F2 C10-C16 hydrocarbons in μg/g, (F2-napth if requested)

F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)

F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is

validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

nC6 and nC10 response factor is within 30% of response factor for toluene:

nC10,nC16 and nC34 response factors within 10% of each other:

C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

Unless otherwise noted all extraction, analysis, QC requirements and limits for holding time were met. If analyzed for F4 and F4G they are not to be summed but the greater of the two numbers are to be used in application to the CWS PHC

QC will be made available upon request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an *

Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie

The Christine Burke

Lab Manager



Final Report

C.O.C.: G75184

REPORT No. B18-10833 (ii)

Rev. 1

Report To:

Peto MacCallum Ltd

19 Churchill Drive, Barrie ON L4N 8Z5

Attention: Geoff White

DATE RECEIVED: 25-Apr-18

DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

**Caduceon Environmental Laboratories** 

112 Commerce Park Drive

Barrie ON L4N 8W8

Tel: 705-252-5743

Fax: 705-252-5746

JOB/PROJECT NO .:

P.O. NUMBER:

18CF004

WATERWORKS NO.

	Client I.D. Sample I.D. Date Collected		BH 2 SS 1 B18-10833-1 23-Apr-18	BH 4 SS 2 B18-10833-2 20-Apr-18	BH 7 SS 3 B18-10833-3 23-Apr-18	O. Reg. 153 Tbl. 1 - All
Parameter	Units	R.L.				
PHC F1 (C6-C10)	µg/g	10	< 10	< 10	< 10	25
PHC F2 (>C10-C16)	µg/g	5	7	6	< 5	10
PHC F3 (>C16-C34)	µg/g	10	15	18	< 10	240
PHC F4 (>C34-C50)	µg/g	10	< 10	< 10	< 10	120
% moisture	%		33.1	6.8	16.0	

¹ Revised report to change guidelines as per client request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an *

Site Analyzed=K-Kingston, W-Windsor, O-Ottawa, R-Richmond Hill, B-Barrie



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**Summary of Exceedances** 

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

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Christine Burke Lab Manager

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Final Report

C.O.C.: G75186 REPORT No. B18-12842 (i)

Rev. 1

Report To:

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Barrie ON L4N 8Z5 Attention: Geoff White

DATE RECEIVED: 14-May-18

DATE REPORTED: 15-Jun-18

SAMPLE MATRIX: Soil

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Fax: 705-252-5746

JOB/PROJECT NO .:

P.O. NUMBER:

18CF004

WATERWORKS NO.

Parameter	Qty	Site Analyzed	Analyst Initials	Date Analyzed	Lab Method	Reference Method
Cyanide	1	Kingston	US	17-May-18	A-CN s K	in house
Conductivity	1	Richmond Hill	ABL	16-May-18	A-COND-02 s RH	MOEE3138
рН	1	Richmond Hill	ABL	15-May-18	A-pH-02 (rh)	MOEE 3137
Chromium (VI)	1	Holly Lane	VK	16-May-18	D-CRVI-02 (o)	EPA7196A
Mercury	1	Holly Lane	PBK	18-May-18	D-HG-01 (o)	EPA 7471A
Sodium Adsorption Ratio	1	Holly Lane	TPR	18-May-18	D-ICP-01 SAR (o)	SM 3120
Metals - ICP-OES	1	Holly Lane	TPR	18-May-18	D-ICP-02 (o)	EPA 6010
Metals - ICP-MS	1	Holly Lane	RPE	18-May-18	D-ICPMS-01 (o)	EPA 6020

μg/g = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in µg/g, (F1-btex if requested)

F2 C10-C16 hydrocarbons in µg/g, (F2-napth if requested)

F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)

F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

nC6 and nC10 response factor is within 30% of response factor for toluene:

nC10,nC16 and nC34 response factors within 10% of each other:

C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

Unless otherwise noted all extraction, analysis, QC requirements and limits for holding time were met. If analyzed for F4 and F4G they are not to be summed but the greater of the two numbers are to be used in application to the CWS PHC

QC will be made available upon request.

O. Reg. 153 - Soil, Ground Water and Sediment Standards Tbl. 1 - All - Table 1 - Res/Park/Institutional/Indus/Com/Commun

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SAMPLE MATRIX: Soil

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18CF004

WATERWORKS NO.

	Client I.D. Sample I.D. Date Collected		TP 5 GS 2 B18-12842-1 11-May-18	O. Reg. 153 Tbl. 1 - All
	Date Cone	cteu	11-iway-16	
Parameter	Units	R.L.		
pH @25°C	pH Units		7.88	MI SE
Conductivity @25°C	mS/cm	0.07	0.12	0.57
Cyanide (Free)	µg/g	0.05	< 0.05	0.051
Sodium Adsorption Ratio	units		0.144	2.4
Antimony	μg/g	0.5	< 0.5	1.3
Arsenic	μg/g	0.5	2.2	18
Barium	μg/g	1	29	220
Beryllium	µg/g	0.2	0.3	2.5
Boron	μg/g	0.5	7.5	36
Cadmium	µg/g	0.5	< 0.5	1.2
Chromium	µg/g	1	12	70
Chromium (VI)	µg/g	0.2	< 0.2	0.66
Cobalt	µg/g	1	6	21
Copper	μg/g	1	14	92
Lead	µg/g	5	< 5	120
Mercury	μg/g	0.005	0.008	0.27
Molybdenum	µg/g	1	< 1	2
Nickel	µg/g	1	14	82
Selenium	μg/g	0.5	< 0.5	1.5
Silver	μg/g	0.2	0.2	0.5
Thallium	μg/g	0.1	< 0.1	1 1
Uranium	μg/g	0.1	0.4	2.5
Vanadium	μg/g	1	16	86
Zinc	μg/g	3	22	290

¹ Revised report to change guidelines as per client request.

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JOB/PROJECT NO .:

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#### **Summary of Exceedances**

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Parameter	Qty	Site Analyzed	Analyst Initials	Date Analyzed	Lab Method	Reference Method
% Moisture	1	Richmond Hill	JE	15-May-18	A-% moisture RH	
PHC(F2-F4)	1	Kingston	KPR	15-May-18	C-PHC-S-001 (k)	CWS Tier 1
PHC(F1)	1	Richmond Hill	JE	15-May-18	C-VPHS-01 (rh)	CWS Tier 1

μg/g = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in μg/g, (F1-btex if requested)

F2 C10-C16 hydrocarbons in μg/g, (F2-napth if requested)

F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)

F4 C34-C50 hydrocarbons in μg/g

This method complies with the Reference Method for the CWS PHC and is validated for use in the laboratory.

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C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

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Parameter	Units	R.L.			
PHC F1 (C6-C10)	µg/g	10	< 10	25	
PHC F2 (>C10-C16)	µg/g	5	< 5	10	
PHC F3 (>C16-C34)	µg/g	10	14	240	
PHC F4 (>C34-C50)	µg/g	10	< 10	120	
% moisture	%		8.4	COMPANY TO THE PARTY OF THE PAR	

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Bule

Proposed Residential Subdivision, Grey Road 21, Town of Blue Mountains, Ontario PML Ref.: 18CF004, Report: 1 June 19, 2018



# **APPENDIX B**

Statement of Limitations

### STATEMENT OF LIMITATIONS



#### **STATEMENT OF LIMITATIONS**

This report is prepared for and made available for the sole use of the client named. Peto MacCallum Ltd. (PML) hereby disclaims any liability or responsibility to any person or entity, other than those for whom this report is specifically issued, for any loss, damage, expenses, or penalties that may arise or result from the use of any information or recommendations contained in this report. The contents of this report may not be used or relied upon by any other person without the express written consent and authorization of PML.

This report shall not be relied upon for any purpose other than as agreed with the client named without the written consent of PML. It shall not be used to express or imply warranty as to the fitness of the property for a particular purpose. A portion of this report may not be used as a separate entity: that is to say the report is to be read in its entirety at all times.

The report is based solely on the scope of services which are specifically referred to in this report. No physical or intrusive testing has been performed, except as specifically referenced in this report. This report is not a certification of compliance with past or present regulations, codes, guidelines and policies.

The scope of services carried out by PML is based on details of the proposed development and land use to address certain issues, purposes and objectives with respect to the specific site as identified by the client. Services not expressly set forth in writing are expressly excluded from the services provided by PML. In other words, PML has not performed any observations, investigations, study analysis, engineering evaluation or testing that is not specifically listed in the scope of services in this report. PML assumes no responsibility or duty to the client for any such services and shall not be liable for failing to discover any condition, whose discovery would require the performance of services not specifically referred to in this report.

### STATEMENT OF LIMITATIONS



# STATEMENT OF LIMITATIONS (continued)

The findings and comments made by PML in this report are based on the conditions observed at the time of PML's site reconnaissance. No assurances can be made and no assurances are given with respect to any potential changes in site conditions following the time of completion of PML's field work. Furthermore, regulations, codes and guidelines may change at any time subsequent to the date of this report and these changes may effect the validity of the findings and recommendations given in this report.

The results and conclusions with respect to site conditions are therefore in no way intended to be taken as a guarantee or representation, expressed or implied, that the site is free from any contaminants from past or current land use activities or that the conditions in all areas of the site and beneath or within structures are the same as those areas specifically sampled.

Any investigation, examination, measurements or sampling explorations at a particular location may not be representative of conditions between sampled locations. Soil, ground water, surface water, or building material conditions between and beyond the sampled locations may differ from those encountered at the sampling locations and conditions may become apparent during construction which could not be detected or anticipated at the time of the intrusive sampling investigation.

Budget estimates contained in this report are to be viewed as an engineering estimate of probable costs and provided solely for the purposes of assisting the client in its budgeting process. It is understood and agreed that PML will not in any way be held liable as a result of any budget figures provided by it.

The Client expressly waives its right to withhold PML's fees, either in whole or in part, or to make any claim or commence an action or bring any other proceedings, whether in contract, tort, or otherwise against PML in anyway connected with advice or information given by PML relating to the cost estimate or Environmental Remediation/Cleanup and Restoration or Soil and Ground Water Management Plan Cost Estimate.