



C.C. Tatham & Associates Ltd.
Consulting Engineers

BLUE VISTA

Town of The Blue Mountains

Preliminary Stormwater Management Report

prepared by:

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prepared for

Royalton Homes Inc.

February 27, 2019

CCTA File 117159

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1 Introduction

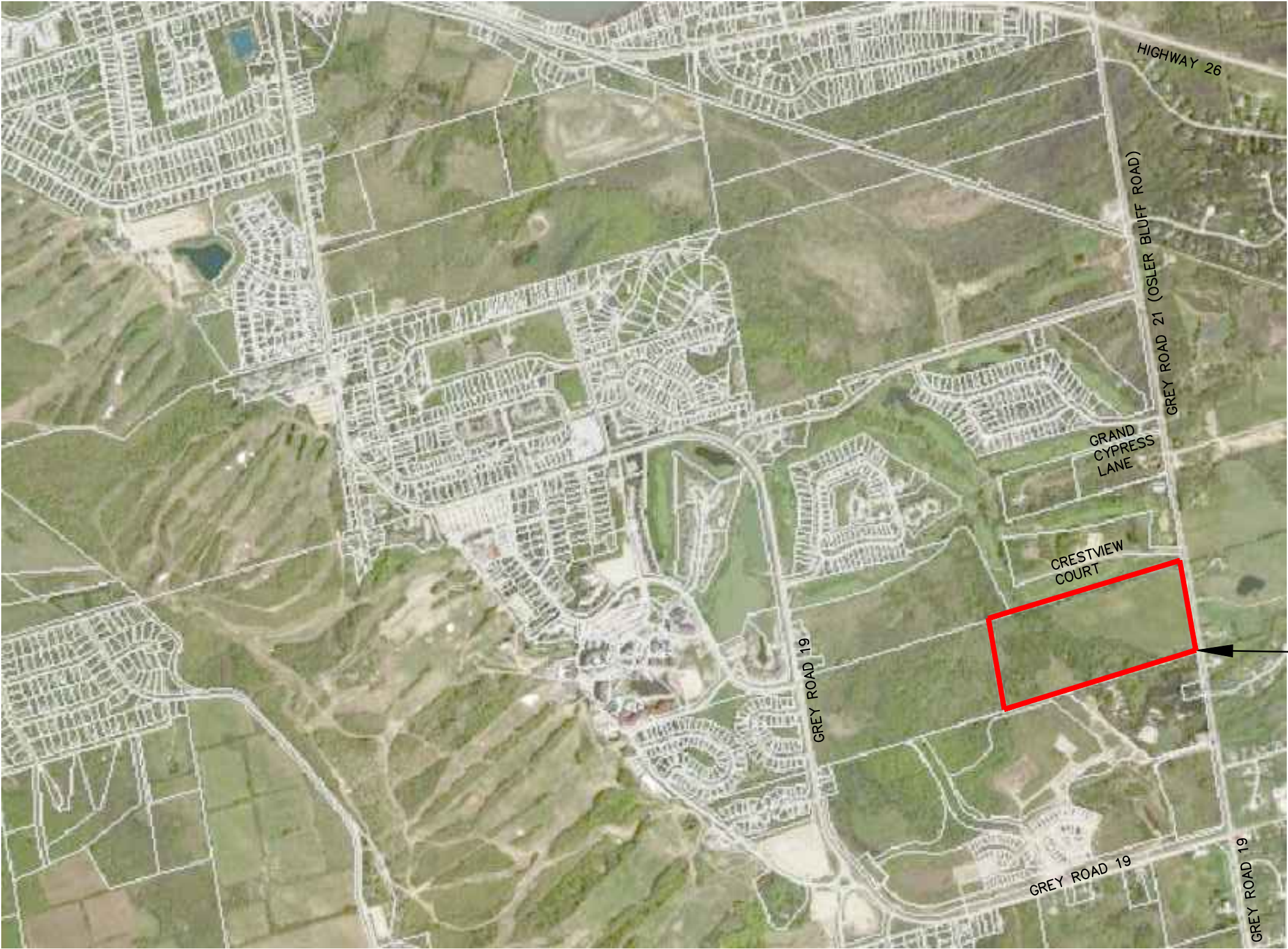
This preliminary stormwater management report has been prepared in support of the Blue Vista residential development located on the west side of Grey Road 21 (Osler Bluff Road), north of Grey Road 19/Mountain Road, in the Town of The Blue Mountains, as illustrated in Figure 1 overleaf.

The purpose of this report is to address the requirements of the Town of The Blue Mountains (The Town), Grey Sauble Conservation Authority (GSCA), and Nottawasaga Valley Conservation Authority (NVCA) with respect to internal and external servicing to achieve the relevant stormwater management (SWM) design criteria and ultimately ensure that the project is appropriately developed to minimize the impact on the downstream drainage systems.

The proposed SWM Plan was developed recognizing the pertinent Municipal and Provincial guidelines on municipal design, water resources, and the environment, as well as other reports prepared in support of the proposed development including the following:

- *Design Guidelines for Sewage Works*. Ministry of the Environment, Conservation and Parks (2008);
- *Engineering Standards*. Town of The Blue Mountains (April 2009);
- *Stormwater Management Practices Planning and Design Manual*. Ministry of the Environment, Conservation and Parks (2003); and
- *Preliminary Infiltration Assessment*. Peto MacCallum Ltd. (August 20, 2018).

Chapter 2 of this report addresses the existing site conditions, detailing the existing topography, soils, drainage outlets and specific peak flow characteristics. Chapter 3 discusses the design criteria for the stormwater management plan with respect to the Town, GSCA, NVCA, and the Ministry of Environment, Conservation and Parks (MECP). The proposed drainage conditions and proposed SWM plan are addressed in Chapter 4 including the proposed stormwater quantity and quality controls. Erosion Hazard are discussed in Chapter 4, and Chapter 4 addresses the erosion and sediment control plan for construction activities. Lastly, Chapter 5 summarizes the report and the key findings.



				BLUE VISTA TOWN OF THE BLUE MOUNTAINS	 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie Ottawa		
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	1.	DRAFT PLAN APPROVAL	FEB/19		DESIGN: JPA	CHECKED: RS	DWG. FIG-1
	NO.	REVISIONS	DATE		DRAWN: RD	DATE: NOV/18	

2 Blue Vista Development

2.1 Site Location and Description

The Blue Vista property is bordered by Grey Road 21 (Osler Bluff Road) to the east, the Scandinave Spa and the Windfall Development Lands to the south, the Second Nature Phase 2 and 3 Development Lands to the west, and the Monterra golf course to the north. The legal description of the site refers to Part Lot 17, Concession 1, Town of The Blue Mountains (formerly the Township of Collingwood), in the County of Grey. The Blue Vista property consists of approximately 20.4 ha of undeveloped land.

Existing site topography, ground cover, land use and drainage patterns were established through site visitation, interpretation of topographic maps, aerial photography and a site survey. The development site generally slopes from southwest to the northeast with approximately 15 m of fall across the property. An intermittent tributary watercourse wetland feature bisects the property into a west and east portion. The central and west portions have predominantly woodland ground cover and the east portion has predominantly pasture ground cover. Ontario Soil Survey Report No. 17 (Grey County North) defines the site to be a mix of Kemble silty clay (Ksc) and Brighton sand (Brs).

2.2 Proposed Land Use

Residential Units

The proposed development is for 133 single detached residential dwellings units. The proposed units will have a minimum lot depth of 30 m with 15 m of frontage. A secondary development plan, to increase the unit count to 180 residential units (accomplished through changing select single-detached units to semi-detached units), will be considered should the Town require an increased lot density.

Other Amenities

The proposed development will also include park areas, an open space area, two stormwater management blocks, and community trails with connection to the existing Town community trail system. As noted in the site plan, a 5.2 m widening along Grey Road 21 (Osler Bluff Road) has been dedicated to Grey County for future development and expansion of Grey Road 21.

Area Land Uses

Historically, land use in the surrounding area has been a mix of woodland, residential as well as recreational and agricultural activities. Residential development of the surrounding areas has increased in recent years resulting in required upgrades to municipal infrastructure to service the area appropriately.

3 Existing Drainage Conditions

A Pre-Development Drainage Plan (Drawing DP-1) has been prepared illustrating the pre-development drainage patterns of the site. Under existing conditions, drainage is conveyed as overland flow to two outlet locations described below:

1. Outlet 1 is the Grey Road 21 (Osler Bluff Road) roadside ditch located at the northeast corner of the property. Approximately 7.6 ha of drainage from the site (Catchment 101) discharges to this roadside ditch and continues flowing north to an unnamed tributary watercourse (referred to as Watercourse 1). This outlet is within the GSCA watershed.
2. Outlet 2 is an intermittent watercourse that bisects the property and drains to the southeast corner of the property. Approximately 12.8 ha of drainage from the development lands and 0.02 ha of external lands drain overland as sheet flow into the watercourse (Catchment 102). The watercourse also receives drainage from the Second Nature, Windfall and Le Scandinave spa development lands (Catchments 501 and 502). The watercourse drains to an existing 600 mm diameter culvert that crosses under Grey Road 21 (Osler Bluff Road) and continues to flow in an eastwardly direction to Silver Creek. This outlet is within the NVCA watershed.

To quantify the pre-development flow rates at the site's two drainage outlets, a Visual OTTHYMO hydrologic model was prepared encompassing the entirety of the Blue Vista property and external areas. The catchment area delineation and hydrologic model input parameters utilized in the model are illustrated on the Pre Development Drainage Plan (Drawing DP-1) enclosed. The model was run using the Town standard Owen Sound 4-hour Chicago and 24-hour SCS design storm events. The hydrologic model results are included in Appendix A and summarized in Table 1.

Table 1: Pre-Development Peak Flow Summary

Storm Event	Outlet 1		Outlet 2	
	Peak Flow Rates (m ³ /s)		Peak Flow Rates (m ³ /s)	
	Chicago Design Storm	SCS Design Storm	Chicago Design Storm	SCS Design Storm
25 mm	0.01	-	0.03	-
2 Year	0.02	0.03	0.07	0.10
5 Year	0.04	0.05	0.13	0.17
10 Year	0.05	0.06	0.18	0.22
25 Year	0.07	0.09	0.24	0.30
50 Year	0.09	0.11	0.31	0.36
100 Year	0.11	0.13	0.37	0.42
Regional	0.25	-	0.72	-

The existing 600 mm diameter culvert crossing at Grey Road 21 (Osler Bluff Road) is considered a point of interest as it is also the discharge outlet for adjacent properties. The hydrologic model results for this point of interest are summarized in Table 2.

Table 2: Point of Interest 1 Pre-Development Peak Flow Summary

Storm Event	Point of Interest 1 Peak Flow Rates (m ³ /s)	
	Chicago Design Storm	SCS Design Storm
25 mm	0.09	-
2 Year	0.22	0.33
5 Year	0.42	0.55
10 Year	0.58	0.72
25 Year	0.80	0.94
50 Year	0.98	1.12
100 Year	1.17	1.30
Regional	1.96	-

A HY-8 hydraulic model was prepared to determine the maximum capacity of the existing culvert crossing and the extent of flooding over Grey Road 21 (Osler Bluff Road) during storms which exceeded the conveyance capacity of the culvert. The modelling results are included in Appendix B and summarized in Table 3.

Table 3: Grey Road 21 (Osler Bluff Road) Culvert Crossing Hydraulic Summary

Storm Event	Peak Flow Rate (m ³ /s)	Culvert Discharge (m ³ /s)	Discharge over Roadway (m ³ /s)	Depth of Overtopping (m)
25 mm	0.09	0.09	0.00	0.00
2 Year	0.33	0.33	0.00	0.00
5 Year	0.55	0.55	0.00	0.00
10 Year	0.72	0.72	0.00	0.00
25 Year	0.94	0.94	0.00	0.00
50 Year	1.12	1.07	0.04	0.01
100 Year	1.30	1.07	0.22	0.02
Regional	1.96	1.08	0.88	0.05

Note: Calculations ignore available floodplain storage upstream of Grey Road 21 (Osler Bluff Road).

4 Proposed Stormwater Management Plan

4.1 Design Criteria

As discussed, to achieve the relevant stormwater management (SWM) design requirements and ultimately ensure that the project is appropriately developed to minimize the impact on the downstream drainage systems, the following design criteria will be addressed in subsequent sections:

- the stormwater management plan will maintain existing stormwater runoff rates at all site outlets by restricting post development peak flow rates to pre-development levels for the 2 through 100-year design storms;
- the stormwater management plan will achieve the required Level 1 “Enhanced” water quality treatment to Provincial standards in the form of 80% total suspended solids (TSS) removal for the site effluent;
- safe conveyance of the Regulatory storm event peak flows through the site to the downstream drainage system will be provided for surface runoff generated within the development;
- the proposed storm sewer system for the newly developed areas will be designed to collect and convey the peak flow generated by the 5-year storm as a minimum objective; and
- the appropriate erosion hazard setback from the watercourse will be maintained.

4.2 Proposed Drainage Conditions

A Post Development Drainage Plan (Drawing DP-2) illustrating the drainage conditions of the proposed development is enclosed and should be referenced in conjunction with this report.

Under proposed conditions, the residential development will drain internally via a combination of storm sewers, drainage swales and the internal road network to the proposed off-line SWM facilities. The storm sewers will be sized to convey the minor storm (5-year design storm) peak flows underground to the end of pipe SWM facilities. The road network will be designed to convey the major storm (100-year design storm) peak flows to the SWM facilities overland. The design of the internal roadways will limit surface ponding during major storm events to depths of 0.30 m or less providing safe access/egress throughout the proposed development.

The drainage directed to Outlet 1 has been minimized as much as possible. However, due to site grading constraints, approximately 2.9 ha (Catchments 201, 203 and 204) will continue to discharge to this outlet. The remainder of the proposed development, approximately 20.5 ha (Catchments 202 and 205), will discharge to Outlet 2.

Flows from Catchment 201 will be conveyed to the northeast SWM Block. A proposed dry pond SWM facility has been designed to provide quantity control to reduce post development peak flows to pre-

development levels at Outlet 1. Water quality control will be provided through a combination of Best Management Practices (dry SWMF, oil grit separator and grassed swales) to achieve the requisite water quality controls.

Catchment 205 will be conveyed to the southeast SWM Block. A proposed wet pond SWM facility has been designed to provide quality and quantity control to provide Level 1 “Enhanced” water quality treatment and reduce post development peak flows to pre-development levels at Outlet 2.

Catchments 203 and 204 will drain directly to Outlet 1, by-passing the dry pond SWMF. Similarly, Catchment 202 will drain directly to the watercourse and Outlet 2, by-passing the wet pond SWMF. These catchments consist of primarily rear yards and open space blocks. As such, the drainage from these catchments is considered clean and treatment is not required. However, these catchments were included in the hydrologic analysis to confirm post development peak flows are attenuated to pre-development levels.

4.3 Water Quantity Control

Post development peak flows to the site outlets must match or be less than the pre-development rates for the 2 through 100-year design storms. This will be achieved on site by storing the surface water runoff within two proposed SWM facilities; a dry pond in the northeast SWM Block discharging to Outlet 1, and a wet pond in the southeast SWM Block discharging to Outlet 2. These ponds will release runoff to the respective outlets at attenuated rates via controlled outlets. The two SWMFs are described in the following sections.

Dry Pond

The dry pond has been designed and sized to provide the requisite water quantity control to limit discharges to Outlet 1 at or below pre-development levels, accounting for the uncontrolled runoff release from Catchments 203 and 204. The dry pond will have approximately 950 m³ of active storage including 500 m³ of extended detention storage. Discharge from the pond will be controlled by a series of engineered outlets as follows:

- a primary low flow outlet consisting of a 55 mm diameter orifice and a 450 mm diameter outlet pipe designed to attenuate the 2 through 100-year design storms; and
- a trapezoidal spillway with a 5 m wide sill that will convey the Regional storm event with sufficient capacity to convey the uncontrolled pond inflow to Outlet 1 during emergency conditions (obstruction of the primary outlet).

Preliminary details of the proposed dry pond are illustrated on the Dry Pond SWMF Conceptual Design (Figure SWM-1) enclosed.

Wet Pond

The wet pond has been designed and sized to provide the requisite water quantity control to limit discharges to Outlet 2 at or below pre-development levels, accounting for the uncontrolled runoff release from Catchment 202. The wet pond will have approximately 8,180 m³ of active storage including 4,660 m³ of extended detention storage. Discharge from the pond will be controlled by a series of engineered outlets as follows:

- a primary low flow outlet consisting of a 120 mm diameter orifice and a 450 mm diameter outlet pipe;
- a secondary outlet consisting of a 600 mm x 600 mm ditch inlet catchbasin; and
- a trapezoidal spillway with a 10 m wide sill that will convey the Regional storm event with sufficient capacity to convey the uncontrolled pond inflow to Outlet 2 during emergency conditions (obstruction of the primary and secondary outlets).

Preliminary details of the proposed wet pond are illustrated on the Wet Pond SWMF Conceptual Design (Figure SWM-2) enclosed.

To quantify the post development flows to Outlet 1 and Outlet 2 under proposed conditions, a hydrologic analysis was completed using the Visual OTTHYMO hydrologic modelling software. The catchment area delineation and hydrologic model input parameters utilized in the model are illustrated on the Post Development Drainage Plan (Drawing DP-2) enclosed. The hydrologic model results are included in Appendix C and summarized in Table 4.

Table 4: Post Development Peak Flow Summary

Storm Event	Outlet 1 Peak Flow Rates (m ³ /s)		Outlet 2 Peak Flow Rates (m ³ /s)	
	Chicago Design Storm	SCS Design Storm	Chicago Design Storm	SCS Design Storm
25 mm	0.01 (0.01)	-	0.03 (0.03)	-
2 Year	0.02 (0.02)	0.02 (0.03)	0.06 (0.07)	0.08 (0.10)
5 Year	0.02 (0.04)	0.02 (0.05)	0.10 (0.13)	0.13 (0.17)
10 Year	0.03 (0.05)	0.03 (0.06)	0.14 (0.18)	0.16 (0.22)
25 Year	0.03 (0.07)	0.04 (0.09)	0.18 (0.24)	0.21 (0.30)
50 Year	0.04 (0.09)	0.04 (0.11)	0.22 (0.31)	0.29 (0.36)
100 Year	0.05 (0.11)	0.05 (0.13)	0.30 (0.37)	0.38 (0.42)
Regional	0.18 (0.25)	-	1.27(0.72)	-

Note: (0.01) – Pre-development peak flow rates

A comparison of the post development to pre-development peak flow rates confirms that the proposed SWM plan for the development provides the requisite water quantity control.

Preliminary design details for the SWM facilities are provided in Appendix D. The post development peak flow rates at Point of Interest 1 were tabulated considering the ultimate build-out of the Second Nature development lands and the Windfall development lands and are summarized in Table 5.

A post development HY-8 hydraulic model was prepared to determine the maximum capacity of the existing culvert crossing and the extent of flooding over Grey Road 21 (Osler Bluff Road) under proposed conditions. The hydraulic model results are included in Appendix E and summarized in Table 6. Additional conveyance calculations for the proposed 600 mm diameter CSP crossing the intermittent tributary watercourse as well as for the conveyance swales are also provided in Appendix E.

Table 5: Point of Interest 1 Post Development Peak Flow Summary

Storm Event	Point of Interest 1 Peak Flow Rates (m ³ /s)	
	Chicago Design Storm	SCS Design Storm
25 mm	0.05 (0.09)	-
2 Year	0.08 (0.22)	0.10 (0.33)
5 Year	0.16 (0.42)	0.25 (0.55)
10 Year	0.27 (0.58)	0.39 (0.72)
25 Year	0.47 (0.80)	0.62 (0.94)
50 Year	0.66 (0.98)	0.85 (1.12)
100 Year	0.88 (1.17)	1.07 (1.30)
Regional	2.27 (1.96)	-

Note: (0.09) – Pre-development peak flow rates

Table 6: Grey Road 21 (Osler Bluff Road) Culvert Crossing Hydraulic Summary (Proposed Conditions)

Storm Event	Peak Flow Rate (m ³ /s)	Culvert Discharge (m ³ /s)	Discharge over Roadway (m ³ /s)	Depth of Overtopping (m)
25 mm	0.05	0.05	0.00	0.00
2 Year	0.10	0.10	0.00	0.00
5 Year	0.25	0.25	0.00	0.00
10 Year	0.39	0.39	0.00	0.00
25 Year	0.62	0.62	0.00	0.00
50 Year	0.85	0.85	0.00	0.00
100 Year	1.07	1.07	0.00	0.00
Regional	2.27	1.08	1.18	0.07

Note: Calculations ignore available floodplain storage upstream of Grey Road 21 (Osler Bluff Road)

4.4 Water Quality Control

As previously discussed in Section 4.1, “Enhanced” or Level 1 water quality treatment in the form of 80% total suspended solids (TSS) removal is required for the development. The proposed dry pond in combination with an oil-grit separator (OGS) unit will provide the requisite water quality treatment for effluent to Outlet 1 and the proposed wet pond will provide the requisite treatment for its tributary area to Outlet 2.

Outlet 1

Under proposed conditions, approximately 1.6 ha will drain to the dry pond SWM facility. The imperviousness of the catchment area has been calculated to be approximately 50%. An oil-grit separator (OGS) will be installed upstream of the dry pond within the minor drainage system to provide pre-treatment for the runoff from the roadway.

The required extended detention storage volume for the dry pond was determined to be 136 m³/ha, equating to approximately 212 m³. The sizing of the SWM facility also considered the erosion control requirements for the receiving roadside ditch. The simplified approach was used to determine the erosion control storage volume requirement. The dry pond requires 351 m³ of extended detention storage for erosion control. The design extended detention volume for the pond is 500 m³, exceeding both the requirements. In combination, the dry SWM pond and oil-grit separator will provide 80% TSS removal. Water quality calculations and a preliminary OGS sizing report are provided in Appendix F.

Outlet 2

Under proposed conditions, approximately 11.1 ha will drain to the wet pond SWM facility. The imperviousness of the catchment area has been calculated to be approximately 50%. For Level 1 water quality treatment, the required permanent pool volume is 1,515 m³. The required extended detention storage volume for the wet pond was taken as the greater of 40 m³/ha or the runoff volume from the 25 mm event which are 446 m³ and 1,321 m³ respectively. The design permanent pool and extended detention volumes are approximately 3,110 m³ and 3,960 m³ respectively; both exceeding the requirements. As such, the wet pond SWMF will provide 80% TSS removal.

The sizing of the SWM facility also considered the erosion control requirements for the receiving watercourse. The simplified approach was used to determine the erosion control storage volume requirement. For the simplified approach, the wet pond requires 2,507 m³ of extended detention storage for erosion control. The design extended detention volume for the pond is 3,960 m³. As such, the proposed SWM facility provides the requisite level of erosion control. Refer to Appendix F for supporting calculations.

4.5 Natural Erosion Hazard Limit

A natural hazards assessment was conducted to determine the appropriate erosion hazard setback from the watercourse/banks for development. The erosion hazard limit was established with reference to the *Adaptive Management of Stream Corridors in Ontario Natural Hazards Technical Guides* produced by the Ministry of Natural Resources and Forestry and the Institute of Watershed Science. The erosion hazard limit is illustrated on the Natural Hazards Plan (Drawing HAZ-1) enclosed.

The erosion hazard limit was derived by the summation of the following:

- the toe erosion allowance which is taken as a 5 m horizontal setback from the natural toe of slope along the watercourse.
- the stable slope allowance is defined by a 3:1 (horizontal:vertical) slope from the toe erosion allowance to existing grade; and
- the erosion access allowance is a 6 m horizontal setback from the stable slope allowance where slopes are less than 3:1.

The proposed development concept has been developed respecting the erosion hazard limit. As such, the development is located outside the natural hazards on-site.

4.6 Erosion and Sediment Control

Erosion and sediment control (ESC) will be implemented for all construction activities within the development site, including vegetation clearing, topsoil stripping, road construction and stockpiling of

materials. The basic principles considered to minimize erosion and sedimentation and the resultant negative environmental impacts include:

- minimize disturbance activities where possible;
- expose the smallest possible land area to erosion for the shortest possible time;
- institute erosion control measures as-required immediately;
- implement sediment control measures before the onset of construction activities; and
- carry out regular inspections of erosion/sediment control measures and repair or maintain as necessary.

The proposed grading, servicing and building construction should be carried out in such a manner that a minimum amount of erosion occurs and such that sedimentation facilities control any erosion that does occur.

Sediment control basins are proposed in the locations of the dry pond and wet pond SWM facilities to settle out sediment in the surface runoff from the disturbed areas on-site before it is released at Outlet 1 or Outlet 2. Temporary drainage swales will be constructed to intercept surface runoff and direct it into the sediment basins. Additional siltation and erosion control measures should include the following:

- erecting silt fence around all construction sites;
- constructing mud mats to prevent off-site tracking of material at all construction access points; and
- providing sediment traps (e.g. berms, geotextile and stone/straw bale barriers in swales).

5 Summary

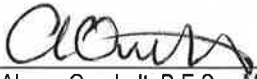
The proposed Stormwater Management Plan has been prepared considering correspondence and input from all approval agencies while recognizing the pertinent Conservation Authority and Provincial guidelines on water resources and the environment. The SWM Plan ensures that the development can be constructed in accordance with all applicable Municipal, Regional and Provincial guidelines while minimizing the impact of the development on the local drainage systems.

The SWM facilities proposed on site will provide the requisite water quantity and quality controls in the form of post to pre-development peak flow matching and 80% TSS removal. The SWM facilities also provide the requisite extended detention storage volumes to satisfy the erosion control criteria for the development. The proposed development plan was also prepared respecting the natural hazards on-site.

Construction and maintenance of siltation and erosion control facilities and implementation of erosion and sediment control best management practices during site servicing and building construction will reduce the transportation of sediment from the site, improving stormwater quality and mitigation environmental impacts during construction.

In conclusion, the proposed stormwater management plan supports the concept of an environmentally sustainable development. The proposed plan will mitigate anticipated stormwater impacts associated with the development of the proposed residential subdivision.



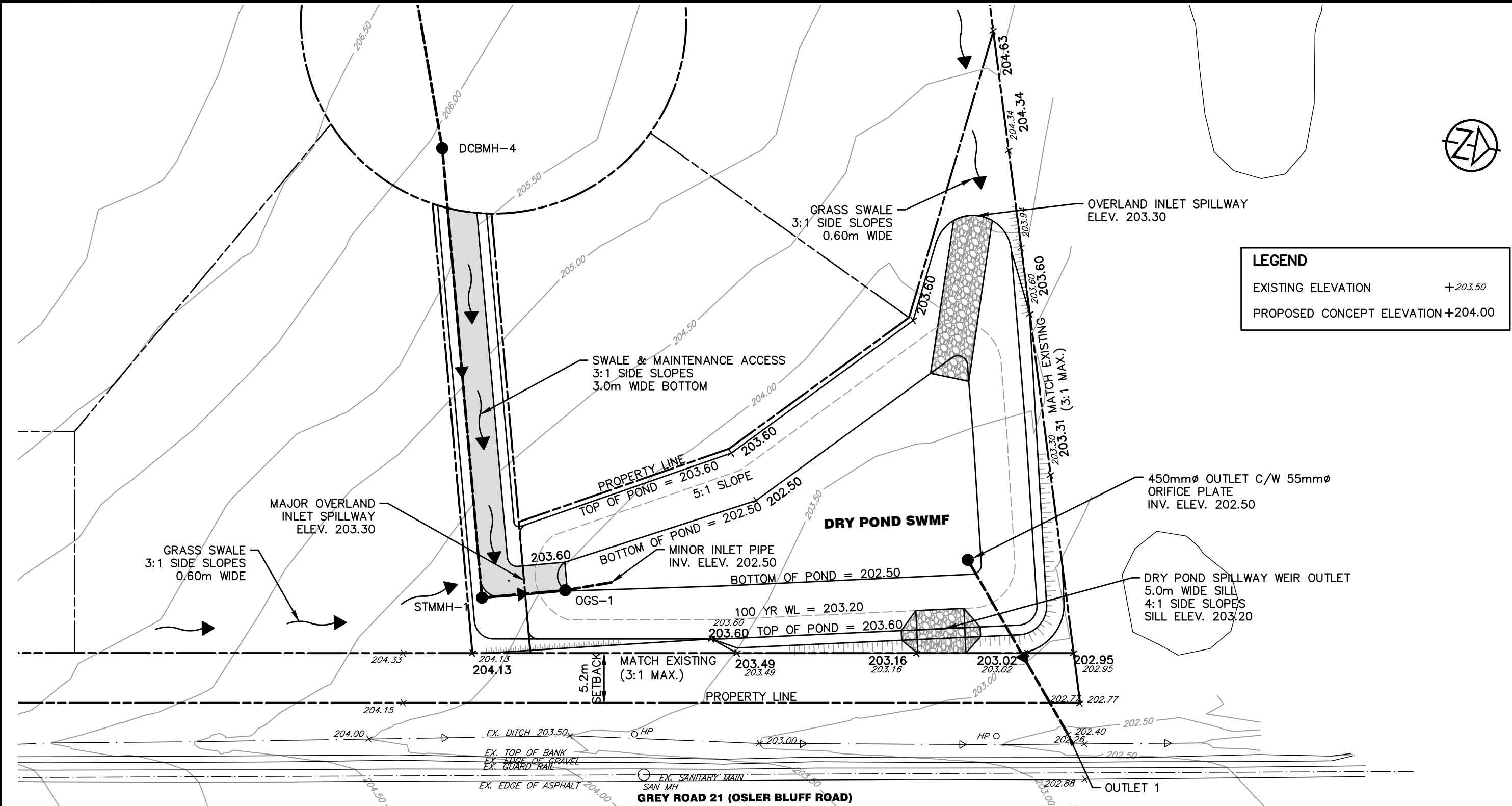

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Senior Engineer, Group Leader

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1.

DRAFT PLAN APPROVAL

FEB/19

NO.

REVISIONS

DATE

**BLUE VISTA
TOWN OF THE BLUE MOUNTAINS**

**DRY POND SWMF
CONCEPTUAL DESIGN**



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie Ottawa

SCALE: 1 : 400

JOB NO. 117159

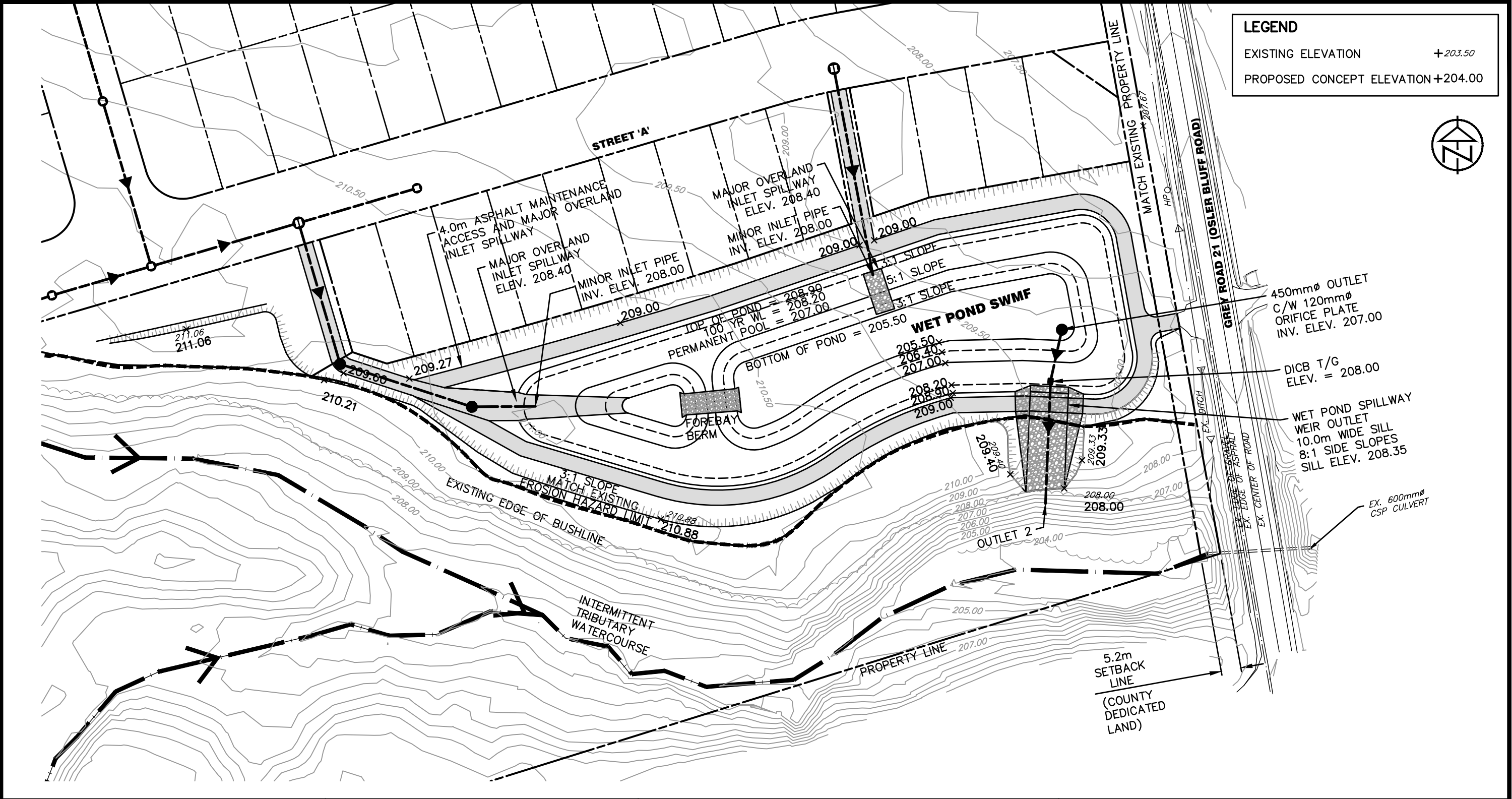
DESIGN: ARO

CHECKED: RS

DRAWN: RD

DATE: NOV/18

DWG. SWM-1



LEGEND

EXISTING ELEVATION +203.50

PROPOSED CONCEPT ELEVATION +204.00



PRELIMINARY

BLUE VISTA
TOWN OF THE BLUE MOUNTAINS



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie Ottawa

WET POND SWMF
CONCEPTUAL DESIGN

SCALE:	1 : 1000	JOB NO.	117159
DESIGN:	ARO	CHECKED:	RS
DRAWN:	RD	DATE:	NOV/18
DWG. SWM-2			

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1.	DRAFT PLAN APPROVAL	FEB/19
NO.	REVISIONS	DATE

APPENDIX A:
EXISTING CONDITION HYDROLOGIC ANALYSIS

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Pre Development

Catchment 101 Area 7.57 ha

WEIGHTED CN VALUE																			
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics			Forest/Woodland			Pasture/Lawns			Meadows			Cultivated		
					Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN
BRS	BRIGHTON	A	Sand	1	7.57	1	32	0	0	49	7.57	1	38	0	0	62	0	0	100
	#N/A	#N/A	#N/A	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A
	#N/A	#N/A	#N/A	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A
	#N/A	#N/A	#N/A	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A
	#N/A	#N/A	#N/A	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A
Totals					7.57	1	0	0	0	0	7.57	1	0	0	0	0	0.757	0.1	43.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 211 m
 Minimum Catchment Elevation 203 m
 Catchment length 307 m
 Catchment Slope 3%
 Catchment Area 7.57 ha

Time of Concentration (Minutes) 11.80
 Time of Concentration (Hours) 0.20
 Time to Peak (2/3 x Time of Concentration) 0.13

Time to Peak 0.80 hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 211 m
 Minimum Catchment Elevation 203 m
 Catchment length 307 m
 Catchment Slope 1%
 Catchment Area 7.57 ha

Time of Concentration (Minutes) 72.16
 Time of Concentration (Hours) 1.20
 Time to Peak (2/3 x Time of Concentration) 0.80

Initial Abstraction 8 mm

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient 0.10

Landuse Type	Soil Series				
	BRS	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Cultivated	0.22	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.095	#N/A	#N/A	#N/A	#N/A

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Pre Development

Catchment 102 Area 12.96 ha

WEIGHTED CN VALUE																			
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics			Forest/Woodland			Pasture/Lawns			Meadows			Cultivated		
					Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN
BRS	BRIGHTON	A	Sand	1	3.1104	0.24	2.4883	0.8	32	0	49	0.4355	0.14	38	0	62	0	100	0.1866
kc-sh	KEMBLE	D	Clay Loam or Clay	3	9.8496	0.76	8.0767	0.82	79	0	84	1.3789	0.14	81	0	86	0	100	0.394
	#N/A	#N/A	#N/A	#N/A	0	0	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0
Totals					12.96	1	10.565	0.8152	0	0	1.8144	0.14	0	0	0	0	0.58061	0.0448	67.5

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 210.75 m
 Minimum Catchment Elevation 203.5 m
 Catchment length 575.5 m
 Catchment Slope 1%
 Catchment Area 12.96 ha

Time of Concentration (Minutes) 24.24
 Time of Concentration (Hours) 0.40
 Time to Peak (2/3 x Time of Concentration) 0.27

Time to Peak 0.90 hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 210.75 m
 Minimum Catchment Elevation 203.5 m
 Catchment length 575.5 m
 Catchment Slope 1%
 Catchment Area 12.96 ha

Time of Concentration (Minutes) 81.19
 Time of Concentration (Hours) 1.35
 Time to Peak (2/3 x Time of Concentration) 0.90

Initial Abstraction 9.272 mm

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient 0.27

Landuse Type	Soil Series				
	BRS	kc-sh	0	0	0
Forest/Woodland	0.08	0.35	#N/A	#N/A	#N/A
Cultivated	0.22	0.55	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	0.4	#N/A	#N/A	#N/A
Impervious	0.95	0.95	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	0.05	#N/A	#N/A	#N/A
Meadows	0.09	0.38	#N/A	#N/A	#N/A
Soil Series Total	0.0796	0.3355	#N/A	#N/A	#N/A

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Pre Development

Catchment 501 Area 15.30 ha

WEIGHTED CN VALUE																										
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics			Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent		Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
kc-sh	KEMBLE	D	Clay Loam or Clay		3	15.3	1	15.3	1	79	0		84	0		81	0		86	0		100	0		50	79
	#N/A	#N/A	#N/A	#N/A		0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0
	#N/A	#N/A	#N/A	#N/A		0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0
	#N/A	#N/A	#N/A	#N/A		0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0
	#N/A	#N/A	#N/A	#N/A		0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0
Totals						15.3	1	15.3	1		0	0		0	0		0	0		0	0		0	0		79.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 220 m
 Minimum Catchment Elevation 217.5 m
 Catchment length 425 m
 Catchment Slope 1%
 Catchment Area 15.3 ha

Time of Concentration (Minutes) 20.51
 Time of Concentration (Hours) 0.34
 Time to Peak (2/3 x Time of Concentration) 0.23

Time to Peak	0.67 hrs
---------------------	-----------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 220 m
 Minimum Catchment Elevation 217.5 m
 Catchment length 425 m
 Catchment Slope 1%
 Catchment Area 15.3 ha

Time of Concentration (Minutes) 60.05
 Time of Concentration (Hours) 1.00
 Time to Peak (2/3 x Time of Concentration) 0.67

Initial Abstraction	10 mm
----------------------------	--------------

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient	0.35
---------------------------	-------------

Landuse Type	Soil Series				
	kc-sh	0	0	0	0
Forest/Woodland	0.35	#N/A	#N/A	#N/A	#N/A
Cultivated	0.55	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.4	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.38	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.35	#N/A	#N/A	#N/A	#N/A

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Pre Development

Catchment 502 Area 1.13 ha

WEIGHTED CN VALUE																										
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics			Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
kc-sh	KEMBLE	D	Clay Loam or Clay	3	1.13	1	1.13	1	79	0		84	0		81	0		86	0		100	0		50	79	
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0	
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0	
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0	
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0	
Totals					1.13	1	1.13	1		0	0		0	0		0	0		0	0		0	0		79.0	

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 220 m
 Minimum Catchment Elevation 217.5 m
 Catchment length 285 m
 Catchment Slope 1%
 Catchment Area 1.13 ha

Time of Concentration (Minutes) 16.47
 Time of Concentration (Hours) 0.27
 Time to Peak (2/3 x Time of Concentration) 0.18

Time to Peak	0.48 hrs
---------------------	-----------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 220 m
 Minimum Catchment Elevation 217.5 m
 Catchment length 285 m
 Catchment Slope 1%
 Catchment Area 1.13 ha

Time of Concentration (Minutes) 43.10
 Time of Concentration (Hours) 0.72
 Time to Peak (2/3 x Time of Concentration) 0.48

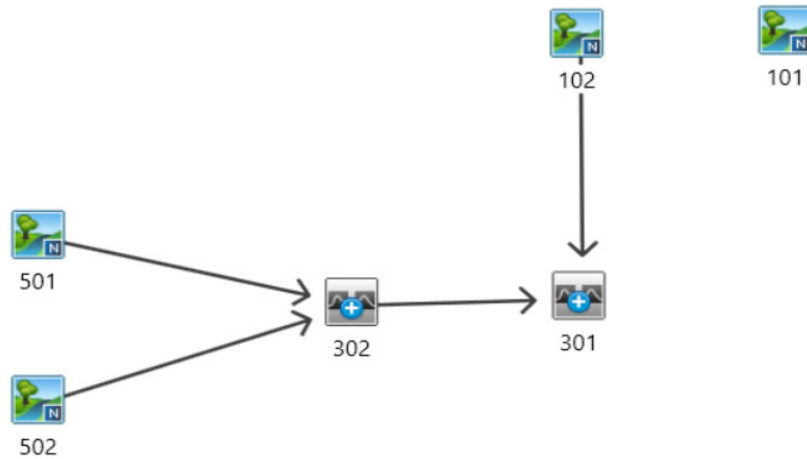
Initial Abstraction	10 mm
----------------------------	--------------

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient	0.35
---------------------------	-------------

Landuse Type	Soil Series				
	kc-sh	0	0	0	0
Forest/Woodland	0.35	#N/A	#N/A	#N/A	#N/A
Cultivated	0.55	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.4	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.38	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.35	#N/A	#N/A	#N/A	#N/A

BLUEVISTA SUBDIVISION
PRE-DEVELOPMENT CONDITIONS



Nashyd



Route Pipe



Duhyd



Standhyd



Route Channel



Diverthyd



Addhyd



Route Reservoir



C.C. TATHAM & ASSOCIATES LTD.
Consulting Engineers

Project: BLUEVISTA

File No.: 117159

Subject: Otthymo Flow Schematic

Date: Dec-18 **Figure:** 1

PRE DEVELOPMENT 4-HR CHICAGO

=====

```
V  V  I  SSSS  U  U  A  L
V  V  I  SS   U  U  A A  L
V  V  I  SS   U  U  AAAAA L
V  V  I  SS   U  U  A  A  L
VV   I  SSSS  UUUUU A  A  LLLLL

000  TTTT  TTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y  Y  MM MM  O  O
O  O  T  T  H  H  Y  Y  M  M  O  O
000  T  T  H  H  Y  Y  M  M  000
```

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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\25b5b42f-bcaf-460b-9416-4ebbf6a0d582\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\25b5b42f-bcaf-460b-9416-4ebbf6a0d582\s

DATE: 01-15-2019 TIME: 09:27:26

USER:

COMMENTS: _____

** SIMULATION : Run 01 ** 25 mm STORM

W/E COMMAND	HYD ID	DT	AREA	'	Qpeak	Tpeak	R.V.	R.C.	Qbase
		min	ha		cms	hrs	mm		cms
START @ 0.00 hrs									

READ STORM	6.0								
[Ptot= 24.97 mm]									
fname :	C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\7f39c85b-08fa-4363-a172-								
remark: CHIC25MM									
** CALIB NASHYD	0101	1	5.0	7.57	0.01	3.00	0.81	0.03	0.000
[CN=43.0									
[N = 3.0:Tp 0.80]									
* READ STORM	6.0								
[Ptot= 24.97 mm]									
fname :	C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\7f39c85b-08fa-4363-a172-								
remark: CHIC25MM									
* ** CALIB NASHYD	0102	1	5.0	12.96	0.03	3.17	1.79	0.07	0.000
[CN=67.5									
]									

```
[ N = 3.0:Tp 0.90]
* READ STORM 6.0
[ Ptot= 24.97 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\7f39c85b-08fa-4363-a172-
remark: CHIC25MM
* ** CALIB NASHYD 0501 1 5.0 15.30 0.06 2.83 2.68 0.11 0.000
[CN=78.7 ]
[ N = 3.0:Tp 0.67]
* READ STORM 6.0
[ Ptot= 24.97 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\7f39c85b-08fa-4363-a172-
remark: CHIC25MM
* ** CALIB NASHYD 0502 1 5.0 1.13 0.01 2.58 2.72 0.11 0.000
[CN=79.0 ]
[ N = 3.0:Tp 0.48]
* ADD [ 0501+ 0502] 0302 3 5.0 16.43 0.06 2.83 2.68 n/a 0.000
* ADD [ 0102+ 0302] 0301 3 5.0 29.39 0.09 2.92 2.29 n/a 0.000
*
=====
```

```
V  V  I  SSSS  U  U  A  L
V  V  I  SS   U  U  A A  L
V  V  I  SS   U  U  AAAAA L
V  V  I  SS   U  U  A  A  L
VV   I  SSSS  UUUUU A  A  LLLLL

000  TTTT  TTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y  Y  MM MM  O  O
O  O  T  T  H  H  Y  Y  M  M  O  O
000  T  T  H  H  Y  Y  M  M  000
```

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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\287941d-3243-4ce3-91c3-3f8b9a51346e\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\287941d-3243-4ce3-91c3-3f8b9a51346e\s

DATE: 01-15-2019 TIME: 09:27:25

USER:

COMMENTS: _____

** SIMULATION : Run 02 ** 2 YEAR STORM

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms

START @ 0.00 hrs

READ STORM 6.0
[Ptot= 33.75 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\afd99867-183a-4a73-a02e-remark: OSCHI2-4hr

* ** CALIB NASHYD 0101 1 5.0 7.57 0.02 2.92 1.83 0.05 0.000
[CN=43.0]
[N = 3.0:Tp 0.80]

* READ STORM 6.0
[Ptot= 33.75 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\afd99867-183a-4a73-a02e-remark: OSCHI2-4hr

* ** CALIB NASHYD 0102 1 5.0 12.96 0.07 3.08 4.08 0.12 0.000
[CN=67.5]
[N = 3.0:Tp 0.90]

* READ STORM 6.0
[Ptot= 33.75 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\afd99867-183a-4a73-a02e-remark: OSCHI2-4hr

* ** CALIB NASHYD 0501 1 5.0 15.30 0.14 2.75 6.10 0.18 0.000
[CN=78.7]
[N = 3.0:Tp 0.67]

* READ STORM 6.0
[Ptot= 33.75 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\afd99867-183a-4a73-a02e-remark: OSCHI2-4hr

* ** CALIB NASHYD 0502 1 5.0 1.13 0.01 2.50 6.18 0.18 0.000
[CN=79.0]
[N = 3.0:Tp 0.48]

* ADD [0501+ 0502] 0302 3 5.0 16.43 0.16 2.75 6.11 n/a 0.000

* ADD [0102+ 0302] 0301 3 5.0 29.39 0.22 2.83 5.21 n/a 0.000

=====

V	V	I	SSSSS	U	U	A	L
V	V	I	SS	U	U	A A	L
V	V	I	SS	U	U	AAAAA	L
V	V	I	SS	U	U	A A	L
VV	I	SSSSS	UUUUU	A	A	LLLLL	

000	TTTTT	TTTTT	H	H	Y	Y	M	M	000	TM
O	O	T	T	H	H	Y Y	MM	MM	O O	

O O T T H H Y M M O O
000 T T H H Y M M 000
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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voim.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\322b3340-a0ec-44a4-8894-5068f9e05eac\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\322b3340-a0ec-44a4-8894-5068f9e05eac\s

DATE: 01-15-2019

TIME: 09:27:26

USER:

COMMENTS: _____

***** SIMULATION : Run 03 ** 5 YEAR STORM *****

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms

START @ 0.00 hrs

READ STORM 6.0
[Ptot= 44.07 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr

* ** CALIB NASHYD 0101 1 5.0 7.57 0.04 2.92 3.49 0.08 0.000
[CN=43.0]
[N = 3.0:Tp 0.80]

* READ STORM 6.0
[Ptot= 44.07 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr

* ** CALIB NASHYD 0102 1 5.0 12.96 0.13 3.00 7.71 0.17 0.000
[CN=67.5]
[N = 3.0:Tp 0.90]

* READ STORM 6.0
[Ptot= 44.07 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr

* ** CALIB NASHYD 0501 1 5.0 15.30 0.28 2.75 11.29 0.26 0.000
[CN=78.7]
[N = 3.0:Tp 0.67]

*

READ STORM 6.0
[Ptot= 44.07 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr

* ** CALIB NASHYD 0502 1 5.0 1.13 0.03 2.50 11.42 0.26 0.000
[CN=79.0]
[N = 3.0:Tp 0.48]

* ADD [0501+ 0502] 0302 3 5.0 16.43 0.30 2.67 11.30 n/a 0.000

* ADD [0102+ 0302] 0301 3 5.0 29.39 0.42 2.75 9.71 n/a 0.000

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5\3212affb-35da-4852-9d0b-9c8922c19c40\5a085746-ead8-4a88-a647-d5ba9e518e4a\summary
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5\3212affb-35da-4852-9d0b-9c8922c19c40\5a085746-ead8-4a88-a647-d5ba9e518e4a\summary

DATE: 01-15-2019 TIME: 09:27:26

USER: _____

COMMENTS: _____

** SIMULATION : Run 04 ** 10 YEAR STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								

READ STORM 6.0								
[Ptot= 50.59 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\4c712121-ba98-4156-a793-								

remark: OSCHI10-4hr

* ** CALIB NASHYD 0101 1 5.0 7.57 0.05 2.83 4.78 0.09 0.000
[CN=43.0]
[N = 3.0:Tp 0.80]

* READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\4c712121-ba98-4156-a793-remark: OSCHI10-4hr

* ** CALIB NASHYD 0102 1 5.0 12.96 0.18 3.00 10.43 0.21 0.000
[CN=67.5]
[N = 3.0:Tp 0.90]

* READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\4c712121-ba98-4156-a793-remark: OSCHI10-4hr

* ** CALIB NASHYD 0501 1 5.0 15.30 0.38 2.67 15.07 0.30 0.000
[CN=78.7]
[N = 3.0:Tp 0.67]

* READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-b3aa-487fc45de076\4c712121-ba98-4156-a793-remark: OSCHI10-4hr

* ** CALIB NASHYD 0502 1 5.0 1.13 0.04 2.42 15.24 0.30 0.000
[CN=79.0]
[N = 3.0:Tp 0.48]

* ADD [0501+ 0502] 0302 3 5.0 16.43 0.41 2.67 15.08 n/a 0.000

* ADD [0102+ 0302] 0301 3 5.0 29.39 0.58 2.75 13.03 n/a 0.000

=====

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V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5

\\3212affb-35da-4852-9d0b-9c8922c19c40\\f8d7234b-cf7b-4e7c-8081-47b57a1cff4f\\s
Summary filename: C:\\Users\\ALOverholt\\AppData\\Local\\Civica\\VH5
\\3212affb-35da-4852-9d0b-9c8922c19c40\\f8d7234b-cf7b-4e7c-8081-47b57a1cff4f\\s

DATE: 01-15-2019 TIME: 09:27:26

USER:

COMMENTS: _____

** SIMULATION : Run 05 ** 25 YEAR STORM

W/E	COMMAND	HYD	ID	DT	AREA	'	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	'	cms	hrs	mm		cms
	START @ 0.00 hrs										

	READ STORM				6.0						
	[Ptot= 59.08 mm]										
	fname :				C:\\Users\\ALOverholt\\AppData\\Local\\Temp\\1b283559-8e56-4c72-						
	b3aa-487fc45de076\\55c9d0c9-46d9-4f05-8d32-										
	remark: OSCHI25-4hr										
*											
**	CALIB NASHYD	0101	1	5.0	7.57		0.07	2.83	6.73	0.11	0.000
	[CN=43.0]										
	[N = 3.0:Tp 0.80]										
*											
	READ STORM				6.0						
	[Ptot= 59.08 mm]										
	fname :				C:\\Users\\ALOverholt\\AppData\\Local\\Temp\\1b283559-8e56-4c72-						
	b3aa-487fc45de076\\55c9d0c9-46d9-4f05-8d32-										
	remark: OSCHI25-4hr										
*											
**	CALIB NASHYD	0102	1	5.0	12.96		0.25	3.00	14.41	0.24	0.000
	[CN=67.5]										
	[N = 3.0:Tp 0.90]										
*											
	READ STORM				6.0						
	[Ptot= 59.08 mm]										
	fname :				C:\\Users\\ALOverholt\\AppData\\Local\\Temp\\1b283559-8e56-4c72-						
	b3aa-487fc45de076\\55c9d0c9-46d9-4f05-8d32-										
	remark: OSCHI25-4hr										
*											
**	CALIB NASHYD	0501	1	5.0	15.30		0.52	2.67	20.44	0.35	0.000
	[CN=78.7]										
	[N = 3.0:Tp 0.67]										
*											
	READ STORM				6.0						
	[Ptot= 59.08 mm]										
	fname :				C:\\Users\\ALOverholt\\AppData\\Local\\Temp\\1b283559-8e56-4c72-						
	b3aa-487fc45de076\\55c9d0c9-46d9-4f05-8d32-										
	remark: OSCHI25-4hr										
*											
**	CALIB NASHYD	0502	1	5.0	1.13		0.05	2.42	20.65	0.35	0.000
	[CN=79.0]										
	[N = 3.0:Tp 0.48]										
*											
	ADD [0501+ 0502]	0302	3	5.0	16.43		0.57	2.67	20.46	n/a	0.000
*											

ADD [0102+ 0302] 0301 3 5.0 29.39 0.80 2.75 17.79 n/a 0.000
*
FINISH

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V V I SSSS U U A L
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O O T T H H Y Y MM MM O O
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***** S U M M A R Y O U T P U T *****

Input filename: C:\\Program Files (x86)\\Visual OTTHYMO 5.0\\vo2\\voin.dat
Output filename: C:\\Users\\ALOverholt\\AppData\\Local\\Civica\\VH5
\\3212affb-35da-4852-9d0b-9c8922c19c40\\1bb3af0e-f885-4e05-8845-e83899ceb8bd\\s
Summary filename: C:\\Users\\ALOverholt\\AppData\\Local\\Civica\\VH5
\\3212affb-35da-4852-9d0b-9c8922c19c40\\1bb3af0e-f885-4e05-8845-e83899ceb8bd\\s

DATE: 01-15-2019 TIME: 09:27:25

USER:

COMMENTS: _____

** SIMULATION : Run 06 ** 50 YEAR STORM

W/E	COMMAND	HYD	ID	DT	AREA	'	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	'	cms	hrs	mm		cms
	START @ 0.00 hrs										

	READ STORM				6.0						
	[Ptot= 65.65 mm]										
	fname :				C:\\Users\\ALOverholt\\AppData\\Local\\Temp\\1b283559-8e56-4c72-						
	b3aa-487fc45de076\\7b698a1b-1f1a-4102-9080-										
	remark: OSCHI50-4hr										
*											
**	CALIB NASHYD	0101	1	5.0	7.57		0.09	2.83	8.43	0.13	0.000
	[CN=43.0]										
	[N = 3.0:Tp 0.80]										
*											
	READ STORM				6.0						

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0 0	T	T	H	H	Y	Y	MM	MM	0 0	
0 0	T	T	H	H	Y	Y	M	M	0 0	
000	T	T	H	H	Y		M	M	000	

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***** S U M M A R Y O U T P U T *****

```

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\WH5
\3212affb-35da-4852-9d0b-9c8922c19c40\01992cbd-5d70-45d1-a3ac-b0f0c3925fda\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\WH5
\3212affb-35da-4852-9d0b-9c8922c19c40\01992cbd-5d70-45d1-a3ac-b0f0c3925fda\s

```

DATE: 01-15-2019

TIME: 09:27:25

USER:

COMMENTS: _____

```

*****
** SIMULATION : Run 08                               **
*****

```

REGIONAL STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
-------------	--------	-----------	------------	--------------	--------------	------------	------	--------------

START @ 0.00 hrs

READ STORM	12.0
------------	------

[Ptot=193.00 mm]

```
fname      : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-a-487fc45de076\3d0c981b-df6b-4723-97f6-remark: TIMMINS
```

```

** CALIB NASHYD      0101  1  5.0      7.57      0.25  7.58  65.60 0.34      0.000
   [CN=43.0]
   [ N = 3.0:Tp 0.80]

```

READ STORM	12.0
------------	------

READ STORM	12.0
------------	------

[Ptot=193.00 mm]

```
fname      : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-a-487fc45de076\3d0c981b-df6b-4723-97f6-remark: TIMMINS
```

```

** CALIB NASHYD      0102  1  5.0   12.96    0.72  7.67 110.30 0.57   0.000
   [CN=67.5]
   [N = 3.0:Tp 0.90]

```

READ STORM	12.0
------------	------

[Ptot=193.00 mm]

```
fname      : C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-
```

b3aa-487fc45de076\3d0c981b-df6b-4723-97f6-remark: TIMMINS

```

** CALIB NASHYD      0501  1  5.0   15.30    1.18  7.33 133.03 0.69   0.000
   [CN=78.7          ]
   [ N = 3.0:Tp 0.67]

```

```
* [ N = 1.000 p = 0.000 ]
      READ STORM                      12.0
      [ Ptot=193.00 mm ]
      fname      :      C:\Users\ALOverholt\AppData\Local\Temp\1b283559-8e56-4c72-
b3aa-487fc45de076\3d0c981b-df6b-4723-97f6-
      remark: TIMMINS
```

```

** CALIB NASHYD      0502  1  5.0      1.13      0.10  7.17 133.67 0.69   0.000
  [CN=79.0]
  [ N = 3.0:Tp 0.48]

```

ADD [0501+ 0502]	0302	3	5.0	16.43	1.27	7.33	133.07	n/a	0.000
-------------------	------	---	-----	-------	------	------	--------	-----	-------

ADD [0102+ 0302]	0301	3	5.0	29.39	1.96	7.42	123.03	n/a	0.000
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[illegible]

PRE DEVELOPMENT 24-HR SCS

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O O T T H H Y Y MM MM O O
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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\46d65693-d244-4788-b1ee-2df4f945002e\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\46d65693-d244-4788-b1ee-2df4f945002e\s

DATE: 01-15-2019 TIME: 09:27:21

USER:

COMMENTS: _____

** SIMULATION : Run 01 ** 2 YEAR STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								
MASS STORM [Ptot= 48.70 mm]	5.0							
** CALIB NASHYD [CN=79.0 [N = 3.0:Tp 0.48]	0502	1 5.0	1.13	0.02	12.42	14.10	0.29	0.000
MASS STORM [Ptot= 48.70 mm]	5.0							
** CALIB NASHYD [CN=78.7 [N = 3.0:Tp 0.67]	0501	1 5.0	15.30	0.22	12.67	13.94	0.29	0.000
ADD [0501+ 0502]	0302	3 5.0	16.43	0.23	12.58	13.95	n/a	0.000
MASS STORM [Ptot= 48.70 mm]	5.0							

*
** CALIB NASHYD 0102 1 5.0 12.96 0.10 12.92 9.61 0.20 0.000
[CN=67.5
[N = 3.0:Tp 0.90]
*
ADD [0102+ 0302] 0301 3 5.0 29.39 0.33 12.67 12.04 n/a 0.000
*
MASS STORM 5.0
[Ptot= 48.70 mm]
*
** CALIB NASHYD 0101 1 5.0 7.57 0.03 12.83 4.39 0.09 0.000
[CN=43.0
[N = 3.0:Tp 0.80]
*

=====

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\428fe02-5452-495f-9b9e-9a6e9dd8617b\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
3212affb-35da-4852-9d0b-9c8922c19c40\428fe02-5452-495f-9b9e-9a6e9dd8617b\s

DATE: 01-15-2019 TIME: 09:27:22

USER:

COMMENTS: _____

** SIMULATION : Run 02 ** 5 YEAR STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								
MASS STORM [Ptot= 62.00 mm]	5.0							
** CALIB NASHYD	0502	1 5.0	1.13	0.03	12.42	22.62	0.36	0.000

```

[CN=79.0
[ N = 3.0:Tp 0.48]
*
MASS STORM          5.0
[ Ptot= 62.00 mm ]
*
** CALIB NASHYD      0501  1  5.0   15.30   0.36 12.58  22.39 0.36   0.000
[CN=78.7
[ N = 3.0:Tp 0.67]
*
* ADD [ 0501+ 0502] 0302  3  5.0   16.43   0.39 12.58  22.41 n/a   0.000
*
MASS STORM          5.0
[ Ptot= 62.00 mm ]
*
** CALIB NASHYD      0102  1  5.0   12.96   0.17 12.92  15.88 0.26   0.000
[CN=67.5
[ N = 3.0:Tp 0.90]
*
* ADD [ 0102+ 0302] 0301  3  5.0   29.39   0.55 12.67  19.53 n/a   0.000
*
MASS STORM          5.0
[ Ptot= 62.00 mm ]
*
** CALIB NASHYD      0101  1  5.0    7.57   0.05 12.75   7.46 0.12   0.000
[CN=43.0
[ N = 3.0:Tp 0.80]
*
=====
=====
```

```

V  V  I  SSSSS  U  U  A  L
V  V  I  SS    U  U  A A  L
V  V  I  SS    U  U  A A A A L
V  V  I  SS    U  U  A  A  L
VV    I  SSSSS  UUUUU  A  A  LLLLL

000  TTTT  TTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y Y  MM MM  O  O
O  O  T  T  H  H  Y  M  M  O  O
000  T  T  H  H  Y  M  M  000
```

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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\0595769c-6944-4456-aef4-949709215c72\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\0595769c-6944-4456-aef4-949709215c72\s

DATE: 01-15-2019 TIME: 09:27:21

USER:

COMMENTS: _____

** SIMULATION : Run 03 ** 10 YEAR STORM

```

W/E COMMAND          HYD ID  DT  AREA  Qpeak Tpeak  R.V. R.C.  Qbase
                        min    ha    cms  hrs    mm
START @ 0.00 hrs
-----
MASS STORM          5.0
[ Ptot= 70.90 mm ]
*
** CALIB NASHYD      0502  1  5.0   1.13   0.04 12.33  28.88 0.41   0.000
[CN=79.0
[ N = 3.0:Tp 0.48]
*
MASS STORM          5.0
[ Ptot= 70.90 mm ]
*
** CALIB NASHYD      0501  1  5.0   15.30   0.47 12.58  28.61 0.40   0.000
[CN=78.7
[ N = 3.0:Tp 0.67]
*
* ADD [ 0501+ 0502] 0302  3  5.0   16.43   0.51 12.58  28.63 n/a   0.000
*
MASS STORM          5.0
[ Ptot= 70.90 mm ]
*
** CALIB NASHYD      0102  1  5.0   12.96   0.22 12.92  20.65 0.29   0.000
[CN=67.5
[ N = 3.0:Tp 0.90]
*
* ADD [ 0102+ 0302] 0301  3  5.0   29.39   0.72 12.67  25.11 n/a   0.000
*
MASS STORM          5.0
[ Ptot= 70.90 mm ]
*
** CALIB NASHYD      0101  1  5.0    7.57   0.07 12.75   9.90 0.14   0.000
[CN=43.0
[ N = 3.0:Tp 0.80]
*
=====
=====
```

```

V  V  I  SSSSS  U  U  A  L
V  V  I  SS    U  U  A A  L
V  V  I  SS    U  U  A A A A L
V  V  I  SS    U  U  A  A  L
VV    I  SSSSS  UUUUU  A  A  LLLLL

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O  O  T  T  H  H  Y  M  M  O  O
000  T  T  H  H  Y  M  M  000
```

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***** S U M M A R Y O U T P U T *****

W/E	COMMAND	HYD	ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
	START @ 0.00 hrs									
	MASS STORM [Ptot= 90.30 mm]			5.0						
**	CALIB NASHYD [CN=79.0] [N = 3.0:Tp 0.48]	0502	1	5.0	1.13	0.07	12.33	43.62	0.48	0.000
	MASS STORM [Ptot= 90.30 mm]			5.0						
**	CALIB NASHYD [CN=78.7] [N = 3.0:Tp 0.67]	0501	1	5.0	15.30	0.73	12.58	43.26	0.48	0.000
	ADD [0501+ 0502]	0302	3	5.0	16.43	0.79	12.58	43.29	n/a	0.000
	MASS STORM [Ptot= 90.30 mm]			5.0						
**	CALIB NASHYD [CN=67.5] [N = 3.0:Tp 0.90]	0102	1	5.0	12.96	0.36	12.83	32.29	0.36	0.000
	ADD [0102+ 0302]	0301	3	5.0	29.39	1.12	12.67	38.44	n/a	0.000
	MASS STORM			5.0						

=====

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=====

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000	TTTT	TTTT	H	H	Y	Y	M	M	000	TM
0 0	T	T	H	H	Y	Y	MM	MM	0 0	
0 0	T	T	H	H	Y	Y	M	M	0 0	
000	T	T	H	H	Y		M	M	000	

***** S U M M A R Y O U T P U T *****

COMMENTS: _____

```

*
** CALIB NASHYD      0502  1  5.0      1.13      0.08 12.33  50.20 0.51      0.000
   [CN=79.0]
   [ N = 3.0:Tp 0.48]

```

[illegible]

APPENDIX B:
EXISTING CONDITION HYDRAULIC ANALYSIS

HY-8 Culvert Analysis Report

E. 600 mm Diameter Culvert Crossing at County Road 21 (Existing Flows)

Crossing Discharge Data

Discharge Selection Method: User Defined

Table 1 - Summary of Culvert Flows at Crossing: EX. 600 mm CULVERT (PreDev)

Headwater Elevation (m)	Discharge Names	Total Discharge (cms)	Culvert 1 Discharge (cms)	Roadway Discharge (cms)	Iterations
203.56	25mm	0.09	0.09	0.00	1
203.94	2YR-SCS	0.33	0.33	0.00	1
204.54	5YR-SCS	0.55	0.55	0.00	1
205.37	10YR-SCS	0.72	0.72	0.00	1
206.75	25YR-SCS	0.94	0.94	0.00	1
207.74	50YR-SCS	1.12	1.07	0.04	30
207.75	100YR-SCS	1.30	1.07	0.22	5
207.78	REGIONAL	1.96	1.08	0.88	4
207.73	Overtopping	1.07	1.07	0.00	Overtopping

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cms)	Culvert Discharge (cms)	Headwater Elevation (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	Flow Type	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwater Depth (m)	Outlet Velocity (m/s)	Tailwater Velocity (m/s)
25mm	0.09	0.09	203.56	0.280	0.0*	1-S2n	0.188	0.190	0.188	0.030	1.144	0.215
2YR-SCS	0.33	0.33	203.94	0.630	0.661	7-M2c	0.404	0.374	0.374	0.066	1.783	0.360
5YR-SCS	0.55	0.55	204.54	1.045	1.255	7-M2c	0.600	0.484	0.484	0.090	2.252	0.440
10YR-SCS	0.72	0.72	205.37	1.525	2.092	7-M2c	0.600	0.539	0.539	0.105	2.690	0.489
25YR-SCS	0.94	0.94	206.75	2.380	3.468	7-M2c	0.600	0.561	0.561	0.123	3.419	0.543
50YR-SCS	1.12	1.07	207.74	3.009	4.459	6-FFc	0.600	0.600	0.600	0.137	3.794	0.582
100YR-SCS	1.30	1.07	207.75	3.017	4.471	6-FFc	0.600	0.600	0.600	0.150	3.800	0.616
REGIONAL	1.96	1.08	207.78	3.037	4.504	6-FFc	0.600	0.600	0.600	0.192	3.814	0.723

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

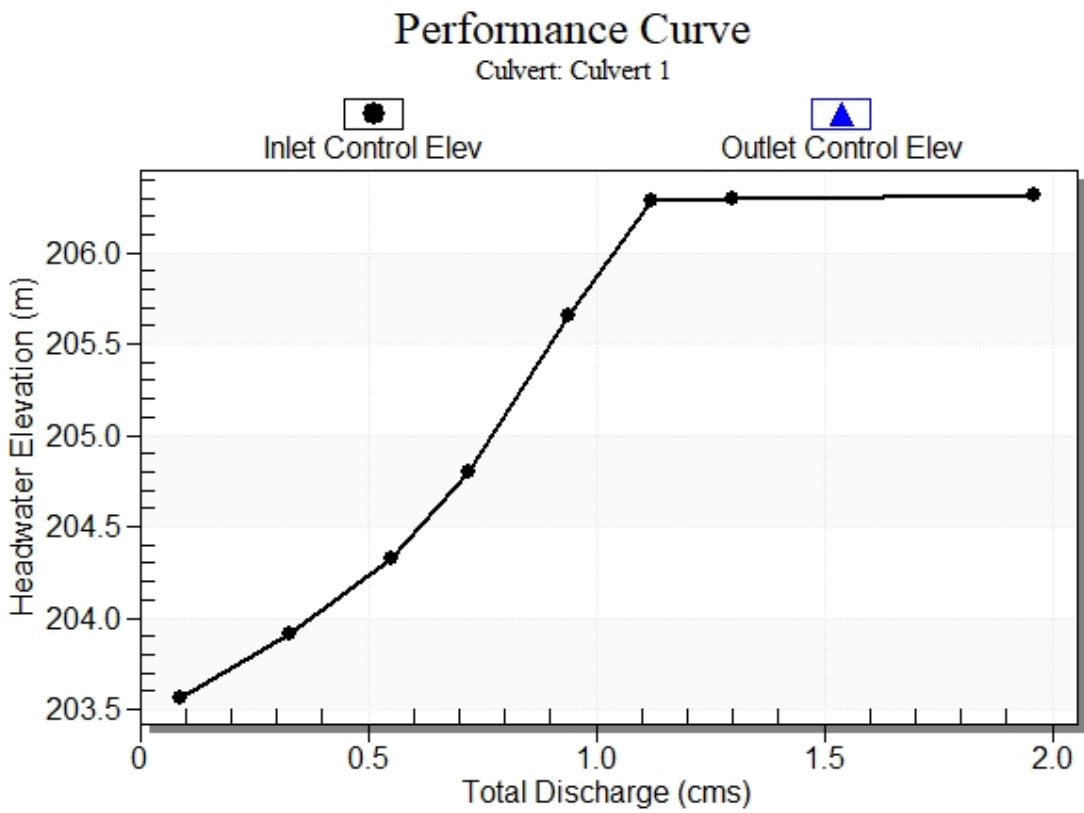
Inlet Elevation (invert): 203.28 m, Outlet Elevation (invert): 202.88 m

Culvert Length: 27.70 m, Culvert Slope: 0.0144

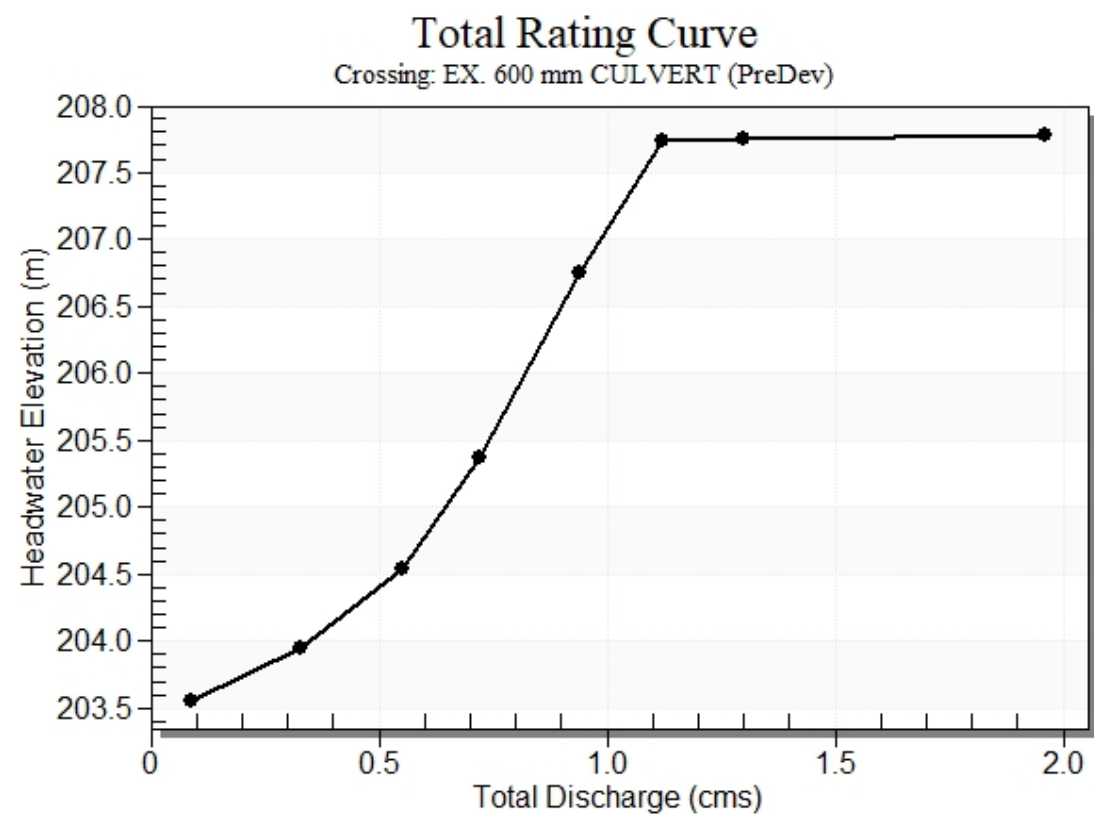
Table 3 - Downstream Channel Rating Curve (Crossing: EX. 600 mm CULVERT (PreDev))

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.09	202.91	0.03	0.22	2.97	0.40
0.33	202.95	0.07	0.36	6.46	0.45
0.55	202.97	0.09	0.44	8.78	0.47
0.72	202.99	0.11	0.49	10.32	0.48
0.94	203.00	0.12	0.54	12.10	0.50
1.12	203.02	0.14	0.58	13.44	0.51
1.30	203.03	0.15	0.62	14.70	0.51
1.96	203.07	0.19	0.72	18.78	0.53

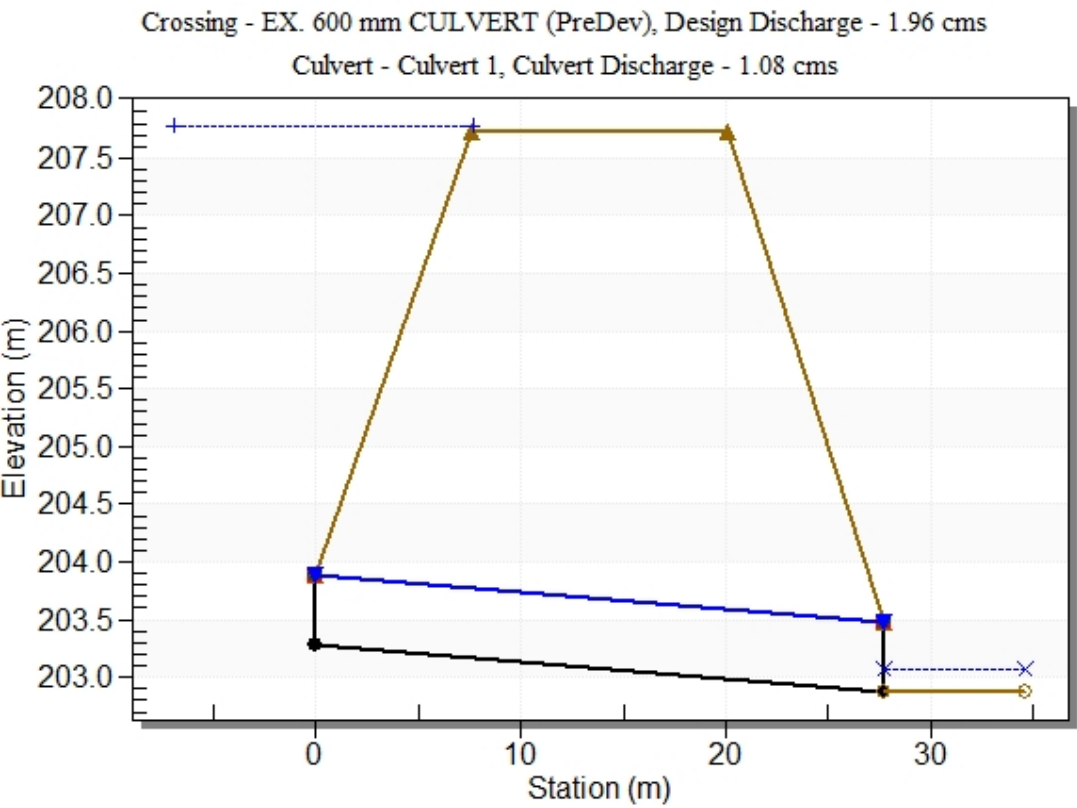
Culvert Performance Curve Plot: Culvert 1



Rating Curve Plot for Crossing: EX. 600 mm CULVERT (PreDev)



Water Surface Profile Plot for Culvert: Culvert 1



Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 203.28 m

Outlet Station: 27.70 m

Outlet Elevation: 202.88 m

Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Circular

Barrel Diameter: 600.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

Tailwater Channel Data - EX. 600 mm CULVERT (PreDev)

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 13.77 m

Side Slope (H:V): 2.00 (2:1)

Channel Slope: 0.0100

Channel Manning's n: 0.0450

Channel Invert Elevation: 202.88 m

Roadway Data for Crossing: EX. 600 mm CULVERT (PreDev)

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 43.28 m

Crest Elevation: 207.73 m

Roadway Surface: Paved

Roadway Top Width: 12.50 m

APPENDIX C:
POST DEVELOPMENT HYDROLOGIC ANALYSIS

BLUEVISTA DEVELOPMENT - 117159
PERCENT IMPERVIOUS CALCULATIONS
November 2018

Catchment : 201

Landuse Designation	Area (ha)	% Impervious	Impervious Area (ha)	% Impervious Area that is Directly Connected	Directed Connected Area (ha)	% Impervious Area that is Directly Connected
Single Family Residential	1.18	45.6%	0.54	5.3%	0.03	5.3%
Semi-detached Residential	0.00	50.2%	0.00	18.4%	0.00	0.0%
Road R.O.W.	0.29	55.0%	0.16	85.0%	0.14	85.0%
Park Block	0.00	6.5%	0.00	0.0%	0.00	0.0%
SWM Block	0.09	60.0%	0.05	100.0%	0.05	100.0%
Total	1.56	48.2%	0.75	28.8%	0.22	28.8%

- Notes: 1) Average impervious percentages based on Windfall Development as-built statistics.
2) Roof leaders are to be directed to grassed areas and not connected to storm sewer.
3) Includes an allowance (30 sq.m per lot/180 lots) for driveways for single residential, semi detached and street townhouse lots.

BLUEVISTA DEVELOPMENT - 117159
PERCENT IMPERVIOUS CALCULATIONS
November 2018

Catchment : 202

Landuse Designation	Area (ha)	% Impervious	Impervious Area (ha)
Single Family Residential	1.23	39.7%	0.49
Semi-detached Residential	0.00	50.2%	0.00
Road R.O.W.	0.00	55.0%	0.00
Park Block	0.12	6.5%	0.01
Open Space	5.13	5.0%	0.26
Total	6.48	11.6%	0.75

- Notes: 1) Average impervious percentages based on Windfall Development as-built statistics.
2) Roof leaders are to be directed to grassed areas and not connected to storm sewer.
3) Includes an allowance (30 sq.m per lot/180 lots) for driveways for single residential, semi detached and street townhouse lots.

BLUEVISTA DEVELOPMENT - 117159
PERCENT IMPERVIOUS CALCULATIONS
November 2018

Catchment : 203

Landuse Designation	Area (ha)	% Impervious	Impervious Area (ha)	% Impervious Area that is Directly Connected	Directed Connected Area (ha)	% Impervious Area that is Directly Connected
Single Family Residential	0.29	43.0%	0.12	5.3%	0.01	5.3%
Semi-detached Residential	0.00	50.2%	0.00	18.4%	0.00	0.0%
Road R.O.W.	0.04	55.0%	0.02	85.0%	0.02	85.0%
Park Block	0.00	6.5%	0.00	0.0%	0.00	0.0%
SWM Block	0.00	60.0%	0.00	100.0%	0.00	0.0%
Total	0.33	44.4%	0.15	17.0%	0.02	17.0%

Notes: 1) Average impervious percentages based on Windfall Development as-built statistics.
2) Roof leaders are to be directed to grassed areas and not connected to storm sewer.
3) Includes an allowance (30 sq.m per lot/180 lots) for driveways for single residential, semi detached and street townhouse lots.

BLUEVISTA DEVELOPMENT - 117159
PERCENT IMPERVIOUS CALCULATIONS
November 2018

Catchment : 204

Landuse Designation	Area (ha)	% Impervious	Impervious Area (ha)
Single Family Residential	0.99	39.7%	0.39
Semi-detached Residential	0.00	50.2%	0.00
Road R.O.W.	0.00	55.0%	0.00
Park Block	0.00	6.5%	0.00
SWM Block	0.00	60.0%	0.00
Total	0.99	39.7%	0.39

- Notes: 1) Average impervious percentages based on Windfall Development as-built statistics.
2) Roof leaders are to be directed to grassed areas and not connected to storm sewer.
3) Includes an allowance (30 sq.m per lot/180 lots) for driveways for single residential, semi detached and street townhouse lots.

BLUEVISTA DEVELOPMENT - 117159
PERCENT IMPERVIOUS CALCULATIONS
November 2018

Catchment : 205

Landuse Designation	Area (ha)	% Impervious	Impervious Area (ha)	% Impervious Area that is Directly Connected	Directed Connected Area (ha)	% Impervious Area that is Directly Connected
Single Family Residential	4.97	48.8%	2.43	5.3%	0.13	5.3%
Semi-detached Residential	1.42	50.2%	0.71	18.4%	0.13	20.0%
Road R.O.W.	2.89	55.0%	1.59	85.0%	1.35	85.0%
Park Block	1.00	6.5%	0.06	0.0%	0.00	0.0%
SWM Block	0.86	80.0%	0.69	100.0%	0.69	100.0%
Total	11.14	49.2%	5.48	41.9%	2.30	41.9%

- Notes: 1) Average impervious percentages based on Windfall Development as-built statistics.
2) Roof leaders are to be directed to grassed areas and not connected to storm sewer.
3) Includes an allowance (30 sq.m per lot/180 lots) for driveways for single residential, semi detached and street townhouse lots.

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Post Development

Catchment 201 Area 1.56 ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
BRS	BRIGHTON	A	Sand	1	1.56	1	0		32	1.56	1	49	0		38	0		62	0		100	0		50	49
Totals					1.56	1	0	0		1.56	1		0	0		0	0		0	0		0	0		49.0

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
Subject:		CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Post Development

Catchment 202 **Area** 6.48 ha

WEIGHTED CN VALUE																											
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type		
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN			
BRS	BRIGHTON	A	Sand	1	1.5552	0.24	1.2753	0.82	32	0			49	0			38	0		62	0.1866	0.12	100	0.0933	0.06	50	41.24
kc-sh	KEMBLE	D	Clay Loam or Clay	3	4.9248	0.76	4.1368	0.84	79	0			84	0			81	0		86	0.591	0.12	100	0.197	0.04	50	80.36
Totals					6.48	1	5.4121	0.8352		0	0	0	0	0	0	0	0	0	0	0	0.7776	0.12		0.2903	0.0448		71.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 210.75 m
 Minimum Catchment Elevation 203.5 m
 Catchment length 575.5 m
 Catchment Slope 1%
 Catchment Area 6.48 ha

Time of Concentration (Minutes) 25.98
 Time of Concentration (Hours) 0.43
 Time to Peak (2/3 x Time of Concentration) 0.29

Time to Peak 0.82 hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 210.75 m
 Minimum Catchment Elevation 203.5 m
 Catchment length 575.5 m
 Catchment Slope 1%
 Catchment Area 6.48 ha

Time of Concentration (Minutes) 73.64
 Time of Concentration (Hours) 1.23
 Time to Peak (2/3 x Time of Concentration) 0.82

Initial Abstraction 8.59 mm

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient 0.35

Landuse Type	Soil Series				
	BRS	kc-sh	0	0	0
Forest/Woodland	0.08	0.35	#N/A	#N/A	#N/A
Cultivated	0.22	0.55	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	0.4	#N/A	#N/A	#N/A
Impervious	0.95	0.95	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	0.05	#N/A	#N/A	#N/A
Meadows	0.09	0.38	#N/A	#N/A	#N/A
Soil Series Total	0.1826	0.404	#N/A	#N/A	#N/A

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
	Designed By:	ARO
	Checked By:	DRT
	Subject:	CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Post Development

Catchment 203 Area 0.33 ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
BRS	BRIGHTON	A	Sand	1	0.33	1	0		32	0.33	1	49	0		38	0		62	0		100	0		50	49
Totals					0.33	1	0	0		0.33	1		0	0		0	0		0	0		0	0		49.0

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
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	Checked By:	DRT
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CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Post Development

Catchment 204 Area 0.99 ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
BRS	BRIGHTON	A	Sand	1	0.99	1	0		32	0.99	1	49	0		38	0		62	0		100	0		50	49
Totals					0.99	1	0	0		0.99	1		0	0		0	0		0	0		0	0		49.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation 212 m
 Minimum Catchment Elevation 207.5 m
 Catchment length 210 m
 Catchment Slope 2%
 Catchment Area 0.99 ha

Time of Concentration (Minutes) 10.29
 Time of Concentration (Hours) 0.17
 Time to Peak (2/3 x Time of Concentration) 0.11

Time to Peak	0.66 hrs
--------------	----------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation 212 m
 Minimum Catchment Elevation 207.5 m
 Catchment length 210 m
 Catchment Slope 1%
 Catchment Area 0.99 ha

Time of Concentration (Minutes) 59.38
 Time of Concentration (Hours) 0.99
 Time to Peak (2/3 x Time of Concentration) 0.66

Initial Abstraction	5.00 mm
---------------------	---------

Woods	10
Meadows	8
Cultivated	7
Lawns	5
Impervious	2

Runoff Coefficient	0.10
--------------------	------

Landuse Type	Soil Series				
	BRS	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Cultivated	0.22	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.1	#N/A	#N/A	#N/A	#N/A

 C.C. Tatham & Associates Ltd. Consulting Engineers Collingwood Bracebridge Orillia Barrie	Project:	BlueVista Subdivision
	File No.:	117159
	Date:	November 2018
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	Subject:	CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

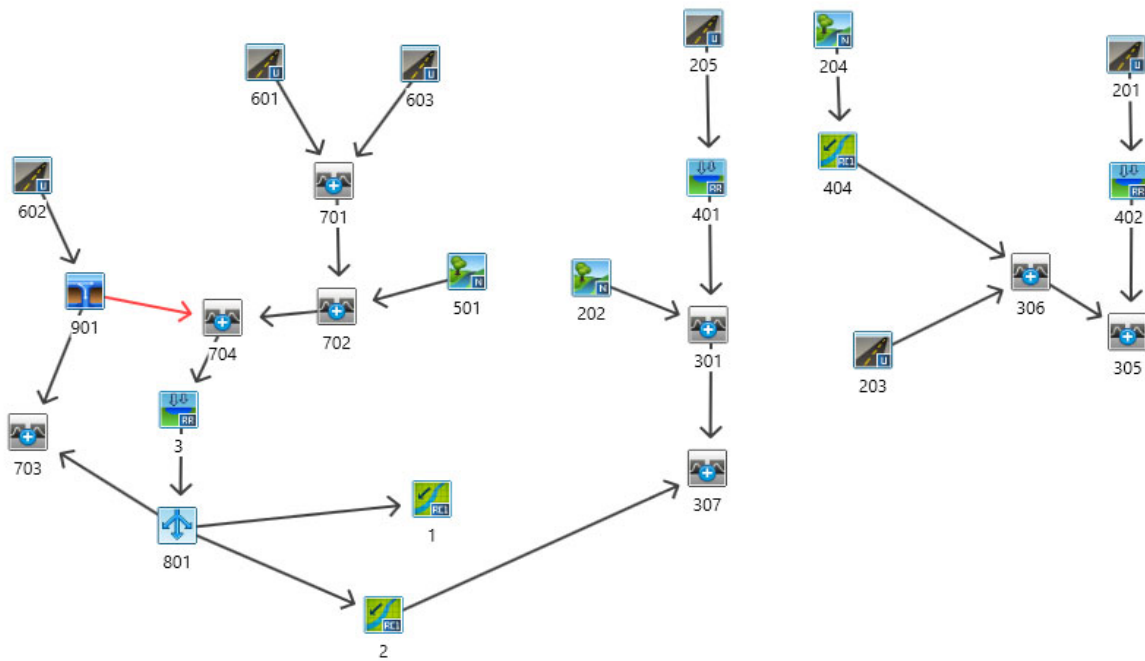
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

Post Development

Catchment 205 Area 11.14 ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Cultivated			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
BRS	BRIGHTON	A	Sand	1	5.7928	0.52	0		32	5.7928	1	49	0		38	0		62	0		100	0		49	
kc-sh	KEMBLE	D	Clay Loam or Clay	3	5.3472	0.48	0		79	5.3472	1	84	0		81	0		86	0		100	0		84	
Totals					11.14	1.00	0	0		11.14	1		0	0		0	0		0	0		0	0		65.8

BLUEVISTA SUBDIVISION PROPOSED CONDITIONS



Nashyd



Standhyd



Addhyd



Route Pipe



Route Channel



Route Reservoir



Duhyd



Diverthyd



C.C. TATHAM & ASSOCIATES LTD.
Consulting Engineers

Project: BLUEVISTA

File No.: 117159

Subject: Otthymo Flow Schematic

Date: Dec-18 **Figure:** 2

POST DEVELOPMENT 4-HR CHICAGO

=====

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTT TTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\914d8941-296f-4848-9247-906c5d323249\s
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DATE: 01-15-2019 TIME: 11:41:06

USER:

COMMENTS: _____

** SIMULATION : Run 01 ** 25 mm STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								

READ STORM 6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM								
** CALIB NASHYD	0204	1	5.0	0.99	0.00	2.75	1.40	0.06 0.000
[CN=49.0] [N = 3.0:Tp 0.66]								
* CHANNEL[2: 0204]	0404	1	5.0	0.99	0.00	2.83	1.40	n/a 0.000
READ STORM 6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM								
*								

* CALIB STANDHYD	0203	1	5.0	0.33	0.01	1.92	5.98	0.24 0.000
[I%=17.0:S%= 2.00]								
* ADD [0203+ 0404]	0306	3	5.0	1.32	0.01	1.92	2.55	n/a 0.000
READ STORM 6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM								
* CALIB STANDHYD	0201	1	5.0	1.56	0.07	1.92	8.41	0.34 0.000
[I%=28.8:S%= 2.00]								
* RESRVR [2: 0201]	0402	1	5.0	1.56	0.00	4.00	7.70	n/a 0.000
{ST= 0.01 ha.m }								
* ADD [0306+ 0402]	0305	3	5.0	2.88	0.01	1.92	5.34	n/a 0.000
READ STORM 6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM								
* CALIB NASHYD	0501	1	1.0	4.80	0.03	2.68	3.27	0.13 0.000
[CN=79.9] [N = 3.0:Tp 0.56]								
* READ STORM	6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM							
* CALIB STANDHYD	0601	1	1.0	20.90	0.63	2.22	12.45	0.50 0.000
[I%=25.0:S%= 2.00]								
* READ STORM	6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM							
* CALIB STANDHYD	0603	1	1.0	2.60	0.26	1.93	16.69	0.67 0.000
[I%=60.0:S%= 2.00]								
* ADD [0601+ 0603]	0701	3	1.0	23.50	0.72	2.12	12.92	n/a 0.000
* ADD [0501+ 0701]	0702	3	1.0	28.30	0.73	2.13	11.28	n/a 0.000
READ STORM 6.0 [Ptot= 24.97 mm] fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\7f39c85b-08fa-4363-a172-remark: CHIC25MM								
* CALIB STANDHYD	0602	1	1.0	15.80	0.47	2.22	12.31	0.49 0.000
[I%=25.0:S%= 2.00]								
* DUHYD	0901	1	1.0	15.80	0.47	2.22	12.31	n/a 0.000
MAJOR SYSTEM: 0901 2 1.0 0.00 0.00 0.00 n/a 0.000								
MINOR SYSTEM: 0901 3 1.0 15.80 0.47 2.22 12.31 n/a 0.000								
*								

```

*   ADD [ 0702+ 0901] 0704 3 1.0 44.10 1.20 2.13 11.65 n/a 0.000
*   RESRVR [ 2: 0704] 0003 1 1.0 44.10 0.08 4.37 9.82 n/a 0.000
*   {ST= 0.44 ha.m }
*   DIVERT HYD 0801 1 1.0 44.10 0.08 4.37 9.82 n/a 0.000
*   Outflow 0003 2 1.0 31.84 0.06 4.37 9.82 n/a 0.000
*   Outflow 0003 3 1.0 4.39 0.01 4.37 9.82 n/a 0.000
*   Outflow 0003 4 1.0 7.88 0.01 4.37 9.82 n/a 0.000
*   Outflow 0003 5 1.0 0.00 0.00 0.00 0.00 n/a 0.000
*   Outflow 0003 6 1.0 0.00 0.00 0.00 0.00 n/a 0.000
*   CHANNEL[ 2: 0801] 0001 1 1.0 4.39 0.01 4.37 9.82 n/a 0.000
*   ADD [ 0801+ 0901] 0703 3 1.0 31.84 0.06 4.37 9.82 n/a 0.000
*   CHANNEL[ 2: 0801] 0002 1 1.0 7.88 0.01 4.37 9.82 n/a 0.000
*   READ STORM 6.0
*   [ Ptot= 24.97 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7f39c85b-08fa-4363-a172-
*   remark: CHIC25MM
*   * CALIB NASHYD 0202 1 5.0 6.48 0.02 3.00 2.23 0.09 0.000
*   [CN=71.0 ]
*   [ N = 3.0:Tp 0.82]
*   READ STORM 6.0
*   [ Ptot= 24.97 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7f39c85b-08fa-4363-a172-
*   remark: CHIC25MM
*   * CALIB STANDHYD 0205 1 5.0 11.14 0.67 1.92 11.85 0.47 0.000
*   [I%=41.9:S%= 2.00]
*   RESRVR [ 2: 0205] 0401 1 5.0 11.14 0.02 4.08 11.68 n/a 0.000
*   {ST= 0.12 ha.m }
*   ADD [ 0202+ 0401] 0301 3 5.0 17.62 0.03 3.08 8.20 n/a 0.000
*   ADD [ 0002+ 0301] 0307 3 1.0 25.50 0.05 3.17 7.57 n/a 0.000

```

=====

```

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U A A A A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

```

```

000 TTTT TTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y Y M M O O
000 T T H H Y Y M M 000

```

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***** S U M M A R Y O U T P U T *****

```

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\9048fc08-1dc1-4886-85d7-9d1dd498100a\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\9048fc08-1dc1-4886-85d7-9d1dd498100a\s

```

DATE: 01-15-2019

TIME: 11:41:05

USER:

COMMENTS: _____

** SIMULATION : Run 02 ** 2 YEAR STORM

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs									

READ STORM 6.0									
[Ptot= 33.75 mm]									
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\afd99867-183a-4a73-a02e-									
remark: OSCHI2-4hr									
**	CALIB NASHYD	0204	1	5.0	0.99	0.00	2.67	2.82	0.08 0.000
[CN=49.0]									
[N = 3.0:Tp 0.66]									
*	CHANNEL[2: 0204]	0404	1	5.0	0.99	0.00	2.83	2.82	n/a 0.000
READ STORM 6.0									
[Ptot= 33.75 mm]									
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\afd99867-183a-4a73-a02e-									
remark: OSCHI2-4hr									
*	CALIB STANDHYD	0203	1	5.0	0.33	0.01	1.92	9.24	0.27 0.000
[I%=17.0:S%= 2.00]									
*	ADD [0203+ 0404]	0306	3	5.0	1.32	0.01	1.92	4.42	n/a 0.000
READ STORM 6.0									
[Ptot= 33.75 mm]									
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\afd99867-183a-4a73-a02e-									
remark: OSCHI2-4hr									
*	CALIB STANDHYD	0201	1	5.0	1.56	0.10	1.92	12.33	0.37 0.000
[I%=28.8:S%= 2.00]									
*	RESRVR [2: 0201]	0402	1	5.0	1.56	0.00	4.00	11.63	n/a 0.000
{ST= 0.02 ha.m }									
*	ADD [0306+ 0402]	0305	3	5.0	2.88	0.02	1.92	8.32	n/a 0.000
READ STORM 6.0									

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs -----								
READ STORM			6.0					
[Ptot= 44.07 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-								
remark: OSCHI5-4hr								
* CALIB NASHYD	0204	1	5.0	0.99	0.01	2.67	5.03 0.11	0.000
[CN=49.0]								
[N = 3.0:Tp 0.66]								
* CHANNEL[2: 0204]	0404	1	5.0	0.99	0.01	2.83	5.03 n/a	0.000
READ STORM			6.0					
[Ptot= 44.07 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-								
remark: OSCHI5-4hr								
* CALIB STANDHYD	0203	1	5.0	0.33	0.02	1.92	13.61 0.31	0.000
[I%=17.0:S%= 2.00]								
* ADD [0203+ 0404]	0306	3	5.0	1.32	0.02	1.92	7.17 n/a	0.000
READ STORM			6.0					
[Ptot= 44.07 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-								
remark: OSCHI5-4hr								
* CALIB STANDHYD	0201	1	5.0	1.56	0.14	1.92	17.40 0.39	0.000
[I%=28.8:S%= 2.00]								
* RESRVR [2: 0201]	0402	1	5.0	1.56	0.00	4.08	16.69 n/a	0.000
{ST= 0.02 ha.m }								
* ADD [0306+ 0402]	0305	3	5.0	2.88	0.02	1.92	12.33 n/a	0.000
READ STORM			6.0					
[Ptot= 44.07 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-								
remark: OSCHI5-4hr								
* CALIB NASHYD	0501	1	1.0	4.80	0.11	2.60	12.54 0.28	0.000
[CN=79.9]								
[N = 3.0:Tp 0.56]								
READ STORM			6.0					
[Ptot= 44.07 mm]								
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-								
remark: OSCHI5-4hr								
* CALIB STANDHYD	0601	1	1.0	20.90	1.72	2.17	27.71 0.63	0.000
[I%=25.0:S%= 2.00]								
READ STORM			6.0					
[Ptot= 44.07 mm]								

fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr											
*	CALIB STANDHYD	0603	1	1.0	2.60	0.51	1.93	32.76	0.74	0.000	
	[I%=60.0:S%= 2.00]										
*	ADD [0601+ 0603]	0701	3	1.0	23.50	1.90	2.13	28.26	n/a	0.000	
*	ADD [0501+ 0701]	0702	3	1.0	28.30	1.95	2.15	25.60	n/a	0.000	
	READ STORM 6.0										
	[Ptot= 44.07 mm]										
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr											
*	CALIB STANDHYD	0602	1	1.0	15.80	1.29	2.17	27.43	0.62	0.000	
	[I%=25.0:S%= 2.00]										
	DUHYD	0901	1	1.0	15.80	1.29	2.17	27.43	n/a	0.000	
	MAJOR SYSTEM:	0901	2	1.0	0.00	0.00	0.00	0.00	n/a	0.000	
	MINOR SYSTEM:	0901	3	1.0	15.80	1.29	2.17	27.43	n/a	0.000	
*	ADD [0702+ 0901]	0704	3	1.0	44.10	3.24	2.15	26.25	n/a	0.000	
*	RESRVR [2: 0704]	0003	1	1.0	44.10	0.40	3.58	23.62	n/a	0.000	
	{ST= 0.93 ha.m }										
	DIVERT HYD	0801	1	1.0	44.10	0.40	3.58	23.62	n/a	0.000	
	Outflow	0003	2	1.0	32.21	0.29	3.58	23.62	n/a	0.000	
	Outflow	0003	3	1.0	4.52	0.04	3.58	23.62	n/a	0.000	
	Outflow	0003	4	1.0	7.37	0.07	3.58	23.62	n/a	0.000	
	Outflow	0003	5	1.0	0.00	0.00	0.00	0.00	n/a	0.000	
	Outflow	0003	6	1.0	0.00	0.00	0.00	0.00	n/a	0.000	
*	CHANNEL[2: 0801]	0001	1	1.0	4.52	0.04	3.58	23.62	n/a	0.000	
*	ADD [0801+ 0901]	0703	3	1.0	32.21	0.29	3.58	23.62	n/a	0.000	
*	CHANNEL[2: 0801]	0002	1	1.0	7.37	0.07	3.58	23.62	n/a	0.000	
	READ STORM 6.0										
	[Ptot= 44.07 mm]										
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr											
*	CALIB NASHYD	0202	1	5.0	6.48	0.08	2.92	9.04	0.21	0.000	
	[CN=71.0]										
	[N = 3.0:Tp 0.82]										
	READ STORM 6.0										
	[Ptot= 44.07 mm]										
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\86dfcc95-9290-4299-a86a-remark: OSCHI5-4hr											
*	CALIB STANDHYD	0205	1	5.0	11.14	1.31	1.92	23.95	0.54	0.000	
	[I%=41.9:S%= 2.00]										
*	RESRVR [2: 0205]	0401	1	5.0	11.14	0.02	4.08	23.77	n/a	0.000	
	{ST= 0.25 ha.m }										

* ADD [0202+ 0401] 0301 3 5.0 17.62 0.10 2.92 18.35 n/a 0.000
* ADD [0002+ 0301] 0307 3 1.0 24.99 0.16 3.27 17.23 n/a 0.000

=====

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

OOO TTTT TTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y Y M M O O
OOO T T H H Y Y M M OOO

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\3b9e2c6-e478-4207-80c9-ee3563bfa419\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\3b9e2c6-e478-4207-80c9-ee3563bfa419\s

DATE: 01-15-2019 TIME: 11:41:07

USER:

COMMENTS: _____

** SIMULATION : Run 04 ** 10 YEAR STORM

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
	START @ 0.00 hrs								

	READ STORM	6.0							
	[Ptot= 50.59 mm]								
a3b01d897221\4c712121-ba98-4156-a793-	fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-								
	remark: OSCHI10-4hr								
*									
**	CALIB NASHYD	0204 1 5.0		0.99	0.01	2.67	6.70	0.13	0.000
	[CN=49.0]								
	[N = 3.0:Tp 0.66]								
*									
*	CHANNEL[2: 0204]	0404 1 5.0		0.99	0.01	2.83	6.70	n/a	0.000
	READ STORM	6.0							
	[Ptot= 50.59 mm]								

fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr

* CALIB STANDHYD 0203 1 5.0 0.33 0.02 1.92 16.67 0.33 0.000
[I%=17.0:S%= 2.00]
* ADD [0203+ 0404] 0306 3 5.0 1.32 0.02 1.92 9.19 n/a 0.000

READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr

* CALIB STANDHYD 0201 1 5.0 1.56 0.17 1.92 20.84 0.41 0.000
[I%=28.8:S%= 2.00]
* RESRVR [2: 0201] 0402 1 5.0 1.56 0.00 4.08 20.13 n/a 0.000
{ST= 0.03 ha.m }
* ADD [0306+ 0402] 0305 3 5.0 2.88 0.03 1.92 15.12 n/a 0.000

READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr

* CALIB NASHYD 0501 1 1.0 4.80 0.15 2.58 16.52 0.33 0.000
[CN=79.9]
[N = 3.0:Tp 0.56]
* READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr

* CALIB STANDHYD 0601 1 1.0 20.90 2.21 2.15 33.34 0.66 0.000
[I%=25.0:S%= 2.00]
* READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr

* CALIB STANDHYD 0603 1 1.0 2.60 0.62 1.93 38.53 0.76 0.000
[I%=60.0:S%= 2.00]
* ADD [0601+ 0603] 0701 3 1.0 23.50 2.45 2.12 33.91 n/a 0.000
* ADD [0501+ 0701] 0702 3 1.0 28.30 2.52 2.12 30.96 n/a 0.000

READ STORM 6.0
[Ptot= 50.59 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\4c712121-ba98-4156-a793-
remark: OSCHI10-4hr
* CALIB STANDHYD 0602 1 1.0 15.80 1.66 2.15 33.02 0.65 0.000
[I%=25.0:S%= 2.00]
*

```

    DUHYD      0901  1  1.0  15.80  1.66  2.15  33.02  n/a  0.000
    MAJOR SYSTEM: 0901  2  1.0   0.00  0.00  0.00  0.00  n/a  0.000
    MINOR SYSTEM: 0901  3  1.0  15.80  1.66  2.15  33.02  n/a  0.000
*
* ADD [ 0702+ 0901] 0704  3  1.0  44.10  4.17  2.13  31.70  n/a  0.000
*
* RESRVR [ 2: 0704] 0003  1  1.0  44.10  0.65  3.25  29.01  n/a  0.000
*   {ST= 1.06 ha.m }
*
* DIVERT HYD      0801  1  1.0  44.10  0.65  3.25  29.01  n/a  0.000
*   Outflow      0003  2  1.0  32.14  0.47  3.25  29.01  n/a  0.000
*   Outflow      0003  3  1.0   4.05  0.04  3.25  29.01  n/a  0.000
*   Outflow      0003  4  1.0   7.91  0.15  3.25  29.01  n/a  0.000
*   Outflow      0003  5  1.0   0.00  0.00  0.00  0.00  n/a  0.000
*   Outflow      0003  6  1.0   0.00  0.00  0.00  0.00  n/a  0.000
*
* CHANNEL[ 2: 0801] 0001  1  1.0   4.05  0.04  3.25  29.01  n/a  0.000
*
* ADD [ 0801+ 0901] 0703  3  1.0  32.14  0.47  3.25  29.01  n/a  0.000
*
* CHANNEL[ 2: 0801] 0002  1  1.0   7.91  0.15  3.25  29.01  n/a  0.000
*
* READ STORM      6.0
*   [ Ptot= 50.59 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\4c712121-ba98-4156-a793-
*   remark: OSCHI10-4hr
*
* CALIB NASHYD      0202  1  5.0   6.48  0.11  2.92  12.10  0.24  0.000
*   [CN=71.0 ]
*   [ N = 3.0:Tp 0.82]
*
* READ STORM      6.0
*   [ Ptot= 50.59 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\4c712121-ba98-4156-a793-
*   remark: OSCHI10-4hr
*
* CALIB STANDHYD      0205  1  5.0  11.14  1.55  1.92  28.45  0.56  0.000
*   [I%=41.9:S%= 2.00]
*
* RESRVR [ 2: 0205] 0401  1  5.0  11.14  0.03  4.17  28.28  n/a  0.000
*   {ST= 0.29 ha.m }
*
* ADD [ 0202+ 0401] 0301  3  5.0  17.62  0.14  2.92  22.33  n/a  0.000
*
* ADD [ 0002+ 0301] 0307  3  1.0  25.53  0.27  3.12  21.02  n/a  0.000
*
=====
=====

V  V  I  SSSSS  U  U  A  L
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
VV    I  SSSSS  UUUUU  A  A  LLLLL

    OOO  TTTT  TTTT  H  H  Y  Y  M  M  OOO  TM
    O  O  T  T  T  H  H  Y  Y  MM  MM  O  O
    O  O  T  T  H  H  Y  Y  M  M  O  O
    OOO  T  T  H  H  Y  Y  M  M  OOO

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***** S U M M A R Y   O U T P U T   *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\eeefed17c-962b-4659-bf65-70e7f9682ced\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\eeefed17c-962b-4659-bf65-70e7f9682ced\s

DATE: 01-15-2019                                TIME: 11:41:08

USER:

COMMENTS: _____

*****
** SIMULATION : Run 05                                ** 25 YEAR STORM
*****

W/E COMMAND      HYD ID  DT      AREA  '  Qpeak  Tpeak      R.V.  R.C.  Qbase
                  min    ha    '  cms    hrs    mm    cms

START @ 0.00 hrs
-----
READ STORM      6.0
[ Ptot= 59.08 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
* ** CALIB NASHYD      0204  1  5.0   0.99   0.02  2.67   9.18  0.16   0.000
*   [CN=49.0 ]
*   [ N = 3.0:Tp 0.66]
*
* CHANNEL[ 2: 0204] 0404  1  5.0   0.99   0.01  2.83   9.18  n/a   0.000
*
* READ STORM      6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
* * CALIB STANDHYD      0203  1  5.0   0.33   0.03  1.92  20.93  0.35   0.000
*   [I%=17.0:S%= 2.00]
*
* ADD [ 0203+ 0404] 0306  3  5.0   1.32   0.03  1.92  12.12  n/a   0.000
*
* READ STORM      6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
* * CALIB STANDHYD      0201  1  5.0   1.56   0.20  1.92  25.55  0.43   0.000
*   [I%=28.8:S%= 2.00]
*
* RESRVR [ 2: 0201] 0402  1  5.0   1.56   0.00  4.08  24.85  n/a   0.000
*   {ST= 0.04 ha.m }
```

```

*
*   ADD [ 0306+ 0402] 0305 3 5.0 2.88 0.03 1.92 19.01 n/a 0.000
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB NASHYD 0501 1 1.0 4.80 0.21 2.57 22.14 0.37 0.000
*   [CN=79.9 ]
*   [ N = 3.0:Tp 0.56]
*
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB STANDHYD 0601 1 1.0 20.90 2.84 2.13 40.86 0.69 0.000
*   [I%=25.0:S%= 2.00]
*
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB STANDHYD 0603 1 1.0 2.60 0.75 1.93 46.18 0.78 0.000
*   [I%=60.0:S%= 2.00]
*
*   ADD [ 0601+ 0603] 0701 3 1.0 23.50 3.14 2.10 41.45 n/a 0.000
*
*   ADD [ 0501+ 0701] 0702 3 1.0 28.30 3.23 2.12 38.17 n/a 0.000
*
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB STANDHYD 0602 1 1.0 15.80 2.12 2.13 40.50 0.69 0.000
*   [I%=25.0:S%= 2.00]
*
*   DUHYD 0901 1 1.0 15.80 2.12 2.13 40.50 n/a 0.000
*   MAJOR SYSTEM: 0901 2 1.0 0.00 0.00 0.00 n/a 0.000
*   MINOR SYSTEM: 0901 3 1.0 15.80 2.12 2.13 40.50 n/a 0.000
*
*   ADD [ 0702+ 0901] 0704 3 1.0 44.10 5.36 2.12 39.01 n/a 0.000
*
*   RESRVR [ 2: 0704] 0003 1 1.0 44.10 0.93 3.10 36.25 n/a 0.000
*   {ST= 1.24 ha.m }
*
*   DIVERT HYD 0801 1 1.0 44.10 0.93 3.10 36.25 n/a 0.000
*   Outflow 0003 2 1.0 31.16 0.59 3.10 36.25 n/a 0.000
*   Outflow 0003 3 1.0 3.54 0.05 3.10 36.25 n/a 0.000
*   Outflow 0003 4 1.0 9.40 0.29 3.10 36.25 n/a 0.000
*   Outflow 0003 5 1.0 0.00 0.00 0.00 0.00 n/a 0.000
*   Outflow 0003 6 1.0 0.00 0.00 0.00 0.00 n/a 0.000
*
*   CHANNEL[ 2: 0801] 0001 1 1.0 3.54 0.05 3.10 36.25 n/a 0.000
*
*   ADD [ 0801+ 0901] 0703 3 1.0 31.16 0.59 3.10 36.25 n/a 0.000
*

```

```

*   CHANNEL[ 2: 0801] 0002 1 1.0 9.40 0.29 3.10 36.25 n/a 0.000
*
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB NASHYD 0202 1 5.0 6.48 0.15 2.83 16.52 0.28 0.000
*   [CN=71.0 ]
*   [ N = 3.0:Tp 0.82]
*
*   READ STORM 6.0
*   [ Ptot= 59.08 mm ]
*   fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\55c9d0c9-46d9-4f05-8d32-
*   remark: OSCHI25-4hr
*
*   CALIB STANDHYD 0205 1 5.0 11.14 1.92 1.92 34.55 0.58 0.000
*   [I%=41.9:S%= 2.00]
*
*   RESRVR [ 2: 0205] 0401 1 5.0 11.14 0.03 4.08 34.38 n/a 0.000
*   {ST= 0.36 ha.m }
*
*   ADD [ 0202+ 0401] 0301 3 5.0 17.62 0.18 2.83 27.81 n/a 0.000
*
*   ADD [ 0002+ 0301] 0307 3 1.0 27.02 0.47 3.03 26.39 n/a 0.000
*
*   FINISH

```

```

=====
=====
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=====

```

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V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

```

```

000 TTTT TTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

```

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***** SUMMARY OUTPUT *****

```

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\89ea8cac-d2cf-45bb-971d-d29a49142e58\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\89ea8cac-d2cf-45bb-971d-d29a49142e58\s

```

DATE: 01-15-2019

TIME: 11:41:05

USER:

COMMENTS: _____

```
*****
** SIMULATION : Run 06                               ** 50 YEAR STORM
*****

W/E COMMAND      HYD ID  DT  AREA  '  Qpeak Tpeak  R.V. R.C.  Qbase
                  min    ha   cms  hrs   mm
START @  0.00 hrs
-----
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
** CALIB NASHYD      0204  1  5.0   0.99   0.02  2.67  11.32  0.17   0.000
[CN=49.0 ]
[ N = 3.0:Tp 0.66]
*
* CHANNEL[ 2: 0204]  0404  1  5.0   0.99   0.02  2.75  11.32  n/a   0.000
*
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB STANDHYD      0203  1  5.0   0.33   0.03  1.92  24.43  0.37   0.000
[I%=17.0:S%= 2.00]
*
* ADD [ 0203+ 0404]  0306  3  5.0   1.32   0.04  1.92  14.60  n/a   0.000
*
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB STANDHYD      0201  1  5.0   1.56   0.23  1.92  29.38  0.45   0.000
[I%=28.8:S%= 2.00]
*
* RESRVR [ 2: 0201]  0402  1  5.0   1.56   0.00  4.08  28.68  n/a   0.000
{ST= 0.04 ha.m }
*
* ADD [ 0306+ 0402]  0305  3  5.0   2.88   0.04  1.92  22.23  n/a   0.000
*
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB NASHYD      0501  1  1.0   4.80   0.25  2.57  26.77  0.41   0.000
[CN=79.9 ]
[ N = 3.0:Tp 0.56]
*
* READ STORM              6.0
[ Ptot= 65.65 mm ]
```

```
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB STANDHYD      0601  1  1.0   20.90   3.38  2.12  46.81  0.71   0.000
[I%=25.0:S%= 2.00]
*
* READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB STANDHYD      0603  1  1.0    2.60   0.84  1.93  52.20  0.80   0.000
[I%=60.0:S%= 2.00]
*
* ADD [ 0601+ 0603]  0701  3  1.0   23.50   3.74  2.08  47.40  n/a   0.000
*
* ADD [ 0501+ 0701]  0702  3  1.0   28.30   3.86  2.10  43.90  n/a   0.000
*
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB STANDHYD      0602  1  1.0   15.80   2.53  2.12  46.42  0.71   0.000
[I%=25.0:S%= 2.00]
*
* DUHYD
  MAJOR SYSTEM:      0901  2  1.0    0.10   0.14  2.12  46.42  n/a   0.000
  MINOR SYSTEM:      0901  3  1.0   15.70   2.39  2.05  46.42  n/a   0.000
*
* ADD [ 0702+ 0901]  0704  3  1.0   44.00   6.24  2.10  44.80  n/a   0.000
*
* RESRVR [ 2: 0704]  0003  1  1.0   44.00   1.18  3.02  41.99  n/a   0.000
{ST= 1.39 ha.m }
*
* DIVERT HYD
  Outflow      0801  1  1.0   44.00   1.18  3.02  41.99  n/a   0.000
  Outflow      0003  2  1.0   29.93   0.69  3.02  41.99  n/a   0.000
  Outflow      0003  3  1.0    3.22   0.05  3.02  41.99  n/a   0.000
  Outflow      0003  4  1.0   10.84   0.45  3.02  41.99  n/a   0.000
  Outflow      0003  5  1.0    0.00   0.00  0.00   0.00  n/a   0.000
  Outflow      0003  6  1.0    0.00   0.00  0.00   0.00  n/a   0.000
*
* CHANNEL[ 2: 0801]  0001  1  1.0    3.22   0.05  3.00  41.99  n/a   0.000
*
* ADD [ 0801+ 0901]  0703  3  1.0   30.04   0.69  3.02  42.00  n/a   0.000
*
* CHANNEL[ 2: 0801]  0002  1  1.0   10.84   0.45  3.00  41.99  n/a   0.000
*
READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\7b698a1b-1f1a-4102-9080-
remark: OSCHI50-4hr
*
* CALIB NASHYD      0202  1  5.0    6.48   0.19  2.83  20.25  0.31   0.000
[CN=71.0 ]
[ N = 3.0:Tp 0.82]
*
* READ STORM              6.0
[ Ptot= 65.65 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
```



```

W/E COMMAND      HYD ID      DT      AREA      Qpeak      Tpeak      R.V.      R.C.      Qbase
                  min      ha      '      cms      hrs      mm
START @ 0.00 hrs
-----
READ STORM              6.0
[ Ptot= 71.77 mm ]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b
3b01d897221\b5ab0902-e54d-49be-9d43-
remark: OSCHI100-4hr

```

**	CALIB NASHYD [CN=49.0 [N = 3.0:Tp 0.66]	0204	1	5.0	0.99	0.02	2.67	13.46	0.19	0.000
*	CHANNEL [2: 0204]	0404	1	5.0	0.99	0.02	2.75	13.46	n/a	0.000
*	READ STORM [Ptot= 71.77 mm] fname : C:\Users\AOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr			6.0						
*	CALIB STANDHYD [I%=17.0:S%= 2.00]	0203	1	5.0	0.33	0.04	1.92	27.84	0.39	0.000
*	ADD [0203+ 0404]	0306	3	5.0	1.32	0.05	1.92	17.06	n/a	0.000
*	READ STORM [Ptot= 71.77 mm] fname : C:\Users\AOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr			6.0						
*	CALIB STANDHYD [I%=28.8:S%= 2.00]	0201	1	5.0	1.56	0.26	1.92	33.07	0.46	0.000
*	RESRVR [2: 0201] {ST= 0.05 ha.m }	0402	1	5.0	1.56	0.00	4.08	32.36	n/a	0.000
*	ADD [0306+ 0402]	0305	3	5.0	2.88	0.05	1.92	25.35	n/a	0.000
*	READ STORM [Ptot= 71.77 mm] fname : C:\Users\AOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr			6.0						
*	CALIB NASHYD [CN=79.9 [N = 3.0:Tp 0.56]	0501	1	1.0	4.80	0.30	2.55	31.25	0.44	0.000
*	READ STORM [Ptot= 71.77 mm] fname : C:\Users\AOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr			6.0						
*	CALIB STANDHYD [I%=25.0:S%= 2.00]	0601	1	1.0	20.90	3.83	2.12	52.41	0.73	0.000
*	READ STORM [Ptot= 71.77 mm] fname : C:\Users\AOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr			6.0						
*	CALIB STANDHYD [I%=60.0:S%= 2.00]	0603	1	1.0	2.60	0.96	1.93	57.85	0.81	0.000
*	ADD [0601+ 0603]	0701	3	1.0	23.50	4.23	2.08	53.01	n/a	0.000
*	ADD [0501+ 0701]	0702	3	1.0	28.30	4.37	2.10	49.32	n/a	0.000

READ STORM 6.0
[Ptot= 71.77 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr

* CALIB STANDHYD	0602	1	1.0	15.80	2.87	2.12	52.00	0.72	0.000
[I%=25.0:S%= 2.00]									
DUHYD	0901	1	1.0	15.80	2.87	2.12	52.00	n/a	0.000
MAJOR SYSTEM:	0901	2	1.0	0.56	0.48	2.12	52.00	n/a	0.000
MINOR SYSTEM:	0901	3	1.0	15.24	2.39	2.00	52.00	n/a	0.000
ADD [0702+ 0901]	0704	3	1.0	43.54	6.75	2.10	50.26	n/a	0.000
RESRVR [2: 0704]	0003	1	1.0	43.54	1.48	2.93	47.39	n/a	0.000
{ST= 1.51 ha.m }									
DIVERT HYD	0801	1	1.0	43.54	1.48	2.93	47.39	n/a	0.000
Outflow	0003	2	1.0	29.00	0.85	2.93	47.39	n/a	0.000
Outflow	0003	3	1.0	2.95	0.05	2.93	47.39	n/a	0.000
Outflow	0003	4	1.0	11.59	0.57	2.93	47.39	n/a	0.000
Outflow	0003	5	1.0	0.00	0.00	0.00	0.00	n/a	0.000
Outflow	0003	6	1.0	0.00	0.00	0.00	0.00	n/a	0.000
CHANNEL[2: 0801]	0001	1	1.0	2.95	0.05	2.93	47.39	n/a	0.000
ADD [0801+ 0901]	0703	3	1.0	29.55	0.85	2.93	47.47	n/a	0.000
CHANNEL[2: 0801]	0002	1	1.0	11.59	0.57	2.93	47.39	n/a	0.000

READ STORM 6.0
[Ptot= 71.77 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr

* CALIB NASHYD	0202	1	5.0	6.48	0.22	2.83	23.91	0.33	0.000
[CN=71.0]									
[N = 3.0:Tp 0.82]									

READ STORM 6.0
[Ptot= 71.77 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\b5ab0902-e54d-49be-9d43-remark: OSCHI100-4hr

* CALIB STANDHYD	0205	1	5.0	11.14	2.44	1.92	44.09	0.61	0.000
[I%=41.9:S%= 2.00]									
RESRVR [2: 0205]	0401	1	5.0	11.14	0.10	3.58	43.91	n/a	0.000
{ST= 0.43 ha.m }									
ADD [0202+ 0401]	0301	3	5.0	17.62	0.31	3.00	36.56	n/a	0.000
ADD [0002+ 0301]	0307	3	1.0	29.21	0.88	2.93	35.76	n/a	0.000

=====

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAAA L

V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL
OOO TTTT TTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
OOO T T H H Y M M OOO

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***** SUMMARY OUTPUT *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\222da8f4-05ed-44d9-9834-56fb5165298a\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\222da8f4-05ed-44d9-9834-56fb5165298a\s

DATE: 01-15-2019 TIME: 11:41:04

USER:

COMMENTS: _____

** SIMULATION : Run 08 ** REGIONAL STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
-------------	--------	--------	---------	-----------	-----------	---------	------	-----------

START @ 0.00 hrs

READ STORM 12.0
[Ptot=193.00 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\3d0c981b-df6b-4723-97f6-remark: TIMMINS

** CALIB NASHYD	0204	1	5.0	0.99	0.04	7.33	78.13	0.40	0.000
[CN=49.0]									
[N = 3.0:Tp 0.66]									
CHANNEL[2: 0204]	0404	1	5.0	0.99	0.04	7.50	78.13	n/a	0.000

READ STORM 12.0
[Ptot=193.00 mm]
fname : C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-a3b01d897221\3d0c981b-df6b-4723-97f6-remark: TIMMINS

* CALIB STANDHYD	0203	1	5.0	0.33	0.03	7.00	114.01	0.59	0.000
[I%=17.0:S%= 2.00]									
ADD [0203+ 0404]	0306	3	5.0	1.32	0.06	7.00	87.10	n/a	0.000

READ STORM 12.0
[Ptot=193.00 mm]

```

fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB STANDHYD      0201  1  5.0    1.56    0.13    7.00 122.18 0.63    0.000
  [I%=28.8:S%= 2.00]
*
* RESRVR [ 2: 0201]    0402  1  5.0    1.56    0.13    7.00 121.48 n/a    0.000
  {ST= 0.05 ha.m }
*
* ADD [ 0306+ 0402]    0305  3  5.0    2.88    0.18    7.00 105.72 n/a    0.000
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB NASHYD      0501  1  1.0     4.80    0.40    7.23 136.76 0.71    0.000
  [CN=79.9 ]
  [ N = 3.0:Tp 0.56]
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB STANDHYD      0601  1  1.0    20.90    2.21    7.05 169.31 0.88    0.000
  [I%=25.0:S%= 2.00]
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB STANDHYD      0603  1  1.0     2.60    0.30    7.00 174.82 0.91    0.000
  [I%=60.0:S%= 2.00]
*
* ADD [ 0601+ 0603]    0701  3  1.0    23.50    2.50    7.02 169.92 n/a    0.000
*
* ADD [ 0501+ 0701]    0702  3  1.0    28.30    2.88    7.03 164.30 n/a    0.000
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB STANDHYD      0602  1  1.0    15.80    1.67    7.05 168.65 0.87    0.000
  [I%=25.0:S%= 2.00]
*
  DUHYD
    MAJOR SYSTEM:      0901  2  1.0    15.80    1.67    7.05 168.65 n/a    0.000
    MINOR SYSTEM:      0901  3  1.0    15.80    1.67    7.05 168.65 n/a    0.000
*
* ADD [ 0702+ 0901]    0704  3  1.0    44.10    4.54    7.03 165.86 n/a    0.000
*
* RESRVR [ 2: 0704]    0003  1  1.0    44.10    3.81    7.37 160.41 n/a    0.000
  {ST= 1.93 ha.m }
*
  DIVERT HYD
    Outflow      0801  1  1.0    44.10    3.81    7.37 160.41 n/a    0.000
                  0003  2  1.0    29.32    2.73    7.37 160.41 n/a    0.000

```

```

Outflow      0003  3  1.0     1.68    0.05    7.37 160.41 n/a    0.000
Outflow      0003  4  1.0    13.10    1.03    7.37 160.41 n/a    0.000
Outflow      0003  5  1.0     0.00    0.00    0.00 0.00 n/a    0.000
Outflow      0003  6  1.0     0.00    0.00    0.00 0.00 n/a    0.000
*
  CHANNEL[ 2: 0801]    0001  1  1.0     1.68    0.05    7.38 160.41 n/a    0.000
*
  ADD [ 0801+ 0901]    0703  3  1.0    29.32    2.73    7.37 160.41 n/a    0.000
*
  CHANNEL[ 2: 0801]    0002  1  1.0    13.10    1.03    7.38 160.41 n/a    0.000
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB NASHYD      0202  1  5.0     6.48    0.40    7.50 118.01 0.61    0.000
  [CN=71.0 ]
  [ N = 3.0:Tp 0.82]
*
  READ STORM      12.0
  [ Ptot=193.00 mm ]
  fname      :      C:\Users\ALOverholt\AppData\Local\Temp\93eaf720-79aa-4a47-bd4b-
a3b01d897221\3d0c981b-df6b-4723-97f6-
remark: TIMMINS
*
* CALIB STANDHYD      0205  1  5.0    11.14    1.08    7.00 148.43 0.77    0.000
  [I%=41.9:S%= 2.00]
*
* RESRVR [ 2: 0205]    0401  1  5.0    11.14    0.91    7.08 148.26 n/a    0.000
  {ST= 0.62 ha.m }
*
* ADD [ 0202+ 0401]    0301  3  5.0    17.62    1.27    7.17 137.14 n/a    0.000
*
* ADD [ 0002+ 0301]    0307  3  1.0    30.72    2.27    7.17 139.75 n/a    0.000
*

```

POST DEVELOPMENT 24-HR SCS

```

=====
=====
V      V      I      SSSSS  U      U      A      L
V      V      I      SS      U      U      A A      L
V      V      I      SS      U      U      AAAAA      L
V      V      I      SS      U      U      A      A      L
VV      I      SSSSS  UUUUU  A      A      LLLLL
000      TTTT      TTTT      H      H      Y      Y      M      M      000      TM
O      O      T      T      H      H      Y      Y      MM      MM      O      O
O      O      T      T      H      H      Y      Y      M      M      O      O
000      T      H      H      Y      Y      M      M      000
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```

***** S U M M A R Y O U T P U T *****

```
Input filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\3cbac376-8935-438b-a080-4fa747a0e3ad\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\3cbac376-8935-438b-a080-4fa747a0e3ad\s
```

DATE: 01-15-2019 TIME: 11:41:40

USER:

COMMENTS: _____

```
*****
** SIMULATION : Run 01                               ** 2 YEAR STORM
*****
```

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								
MASS STORM								
[Ptot= 48.70 mm]								
* ** CALIB NASHYD	0501	1 1.0	4.80	0.09	12.53	11.65	0.24	0.000
[CN=79.9								
[N = 3.0:Tp 0.56]								
* ** MASS STORM								
[Ptot= 48.70 mm]								
* ** CALIB STANDHYD	0601	1 1.0	20.90	1.12	12.18	31.69	0.65	0.000
[I%=25.0:S%= 2.00]								
* ** MASS STORM								
[Ptot= 48.70 mm]								
* ** CALIB STANDHYD	0603	1 1.0	2.60	0.27	12.00	36.85	0.76	0.000
[I%=60.0:S%= 2.00]								

*	ADD [0601+ 0603]	0701	3	1.0	23.50	1.23	12.15	32.26	n/a	0.000
*	ADD [0501+ 0701]	0702	3	1.0	28.30	1.29	12.17	29.39	n/a	0.000
	MASS STORM [Ptot= 48.70 mm]			5.0						
**	CALIB STANDHYD [I%=25.0:S%= 2.00]	0602	1	1.0	15.80	0.84	12.18	31.39	0.64	0.000
*	DUHYD	0901	1	1.0	15.80	0.84	12.18	31.39	n/a	0.000
	MAJOR SYSTEM:	0901	2	1.0	0.00	0.00	0.00	0.00	n/a	0.000
	MINOR SYSTEM:	0901	3	1.0	15.80	0.84	12.18	31.39	n/a	0.000
*	ADD [0702+ 0901]	0704	3	1.0	44.10	2.13	12.17	30.11	n/a	0.000
*	RESRVR [2: 0704] {ST= 0.83 ha.m }	0003	1	1.0	44.10	0.22	14.50	21.66	n/a	0.000
*	DIVERT HYD	0801	1	1.0	44.10	0.22	14.50	21.66	n/a	0.000
	Outflow	0003	2	1.0	32.50	0.16	14.50	21.66	n/a	0.000
	Outflow	0003	3	1.0	4.64	0.03	14.50	21.66	n/a	0.000
	Outflow	0003	4	1.0	6.96	0.03	14.50	21.66	n/a	0.000
	Outflow	0003	5	1.0	0.00	0.00	0.00	0.00	n/a	0.000
	Outflow	0003	6	1.0	0.00	0.00	0.00	0.00	n/a	0.000
*	CHANNEL[2: 0801]	0001	1	1.0	4.64	0.03	14.50	21.66	n/a	0.000
*	ADD [0801+ 0901]	0703	3	1.0	32.50	0.16	14.50	21.66	n/a	0.000
	MASS STORM [Ptot= 48.70 mm]			5.0						
**	CALIB NASHYD [CN=49.0 [N = 3.0:Tp 0.66]	0204	1	5.0	0.99	0.01	12.58	6.20	0.13	0.000
*	CHANNEL[2: 0204]	0404	1	5.0	0.99	0.01	12.75	6.20	n/a	0.000
*	MASS STORM [Ptot= 48.70 mm]			5.0						
*	CALIB STANDHYD [I%=17.0:S%= 2.00]	0203	1	5.0	0.33	0.01	12.00	15.75	0.32	0.000
*	ADD [0203+ 0404]	0306	3	5.0	1.32	0.01	12.00	8.59	n/a	0.000
	MASS STORM [Ptot= 48.70 mm]			5.0						
*	CALIB STANDHYD [I%=28.8:S%= 2.00]	0201	1	5.0	1.56	0.08	12.00	19.82	0.41	0.000
*	RESRVR [2: 0201] {ST= 0.02 ha.m }	0402	1	5.0	1.56	0.00	14.75	19.12	n/a	0.000
*	ADD [0306+ 0402]	0305	3	5.0	2.88	0.02	12.00	14.29	n/a	0.000
*	CHANNEL[2: 0801]	0002	1	1.0	6.96	0.03	14.50	21.66	n/a	0.000
*	MASS STORM [Ptot= 48.70 mm]			5.0						

=====

=====

000	TTTT	TTTT	H	H	Y	Y	M	M	000	TM
0 0	T	T	H	H	Y	Y	MM	MM	0 0	
0 0	T	T	H	H	Y		M	M	0 0	
000	T	T	H	H	Y		M	M	000	

***** SUMMARY OUTPUT *****

COMMENTS: _____

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								

MASS STORM		5.0						

*	[Ptot= 62.00 mm]									
**	CALIB NASHYD [CN=79.9 [N = 3.0:Tp 0.56]	0501	1	1.0	4.80	0.14	12.50	18.82	0.30	0.000
*										
*	MASS STORM [Ptot= 62.00 mm]	5.0								
**	CALIB STANDHYD [I%=25.0:S%= 2.00]	0601	1	1.0	20.90	1.67	12.17	43.49	0.70	0.000
*										
*	MASS STORM [Ptot= 62.00 mm]	5.0								
**	CALIB STANDHYD [I%=60.0:S%= 2.00]	0603	1	1.0	2.60	0.36	12.00	48.85	0.79	0.000
*										
*	ADD [0601+ 0603]	0701	3	1.0	23.50	1.84	12.12	44.08	n/a	0.000
*	ADD [0501+ 0701]	0702	3	1.0	28.30	1.93	12.13	40.71	n/a	0.000
*										
*	MASS STORM [Ptot= 62.00 mm]	5.0								
**	CALIB STANDHYD [I%=25.0:S%= 2.00]	0602	1	1.0	15.80	1.25	12.17	43.12	0.70	0.000
*										
*	DUHYD	0901	1	1.0	15.80	1.25	12.17	43.12	n/a	0.000
	MAJOR SYSTEM:	0901	2	1.0	0.00	0.00	0.00	0.00	n/a	0.000
	MINOR SYSTEM:	0901	3	1.0	15.80	1.25	12.17	43.12	n/a	0.000
*										
*	ADD [0702+ 0901]	0704	3	1.0	44.10	3.17	12.15	41.57	n/a	0.000
*	RESRVR [2: 0704] {ST= 1.03 ha.m }	0003	1	1.0	44.10	0.59	13.22	32.32	n/a	0.000
*										
*	DIVERT HYD	0801	1	1.0	44.10	0.59	13.22	32.32	n/a	0.000
	Outflow	0003	2	1.0	32.22	0.43	13.22	32.32	n/a	0.000
	Outflow	0003	3	1.0	4.39	0.04	13.22	32.32	n/a	0.000
	Outflow	0003	4	1.0	7.50	0.12	13.22	32.32	n/a	0.000
	Outflow	0003	5	1.0	0.00	0.00	0.00	0.00	n/a	0.000
	Outflow	0003	6	1.0	0.00	0.00	0.00	0.00	n/a	0.000
*										
*	CHANNEL[2: 0801]	0001	1	1.0	4.39	0.04	13.22	32.32	n/a	0.000
*	ADD [0801+ 0901]	0703	3	1.0	32.22	0.43	13.22	32.32	n/a	0.000
*										
*	MASS STORM [Ptot= 62.00 mm]	5.0								
**	CALIB NASHYD [CN=49.0 [N = 3.0:Tp 0.66]	0204	1	5.0	0.99	0.01	12.58	10.11	0.16	0.000
*										
*	CHANNEL[2: 0204]	0404	1	5.0	0.99	0.01	12.75	10.11	n/a	0.000
*										
*	MASS STORM [Ptot= 62.00 mm]	5.0								
*										
*	CALIB STANDHYD [I%=17.0:S%= 2.00]	0203	1	5.0	0.33	0.02	12.00	22.45	0.36	0.000
*										
*	ADD [0203+ 0404]	0306	3	5.0	1.32	0.02	12.00	13.19	n/a	0.000

```

*
*      MASS STORM              5.0
*      [ Ptot= 62.00 mm ]
*
*      CALIB STANDHYD          0201  1  5.0    1.56    0.11 12.00  27.23 0.44  0.000
*      [I%=28.8:S%= 2.00]
*
*      RESRVR [ 2: 0201]      0402  1  5.0    1.56    0.00 16.08  26.53 n/a  0.000
*      {ST= 0.03 ha.m }
*
*      ADD [ 0306+ 0402]      0305  3  5.0    2.88    0.02 12.00  20.42 n/a  0.000
*
*      CHANNEL[ 2: 0801]      0002  1  1.0    7.50    0.12 13.22  32.32 n/a  0.000
*
*      MASS STORM              5.0
*      [ Ptot= 62.00 mm ]
*
*      CALIB NASHYD            0202  1  5.0    6.48    0.10 12.83  18.15 0.29  0.000
*      [CN=71.0
*      [ N = 3.0:Tp 0.82]
*
*      MASS STORM              5.0
*      [ Ptot= 62.00 mm ]
*
*      CALIB STANDHYD          0205  1  5.0    11.14    1.02 12.00  36.71 0.59  0.000
*      [I%=41.9:S%= 2.00]
*
*      RESRVR [ 2: 0205]      0401  1  5.0    11.14    0.03 16.58  36.53 n/a  0.000
*      {ST= 0.30 ha.m }
*
*      ADD [ 0202+ 0401]      0301  3  5.0    17.62    0.13 12.83  29.77 n/a  0.000
*
*      ADD [ 0002+ 0301]      0307  3  1.0    25.12    0.25 13.08  22.50 n/a  0.000
*
=====
=====

```

```

      V   V   I   SSSSS  U   U   A   L
      V   V   I   SS    U   U   A A  L
      V   V   I   SS    U   U   A A A A L
      V   V   I   SS    U   U   A   A  L
      VV    I   SSSSS  UUUUU  A   A  LLLLL

      000  TTTT  TTTT  H   H   Y   Y   M   M   000  TM
      O   O   T   T   H   H   Y   Y   MM  MM  O   O
      O   O   T   T   H   H   Y   Y   M   M  O   O
      000  T   T   H   H   Y   Y   M   M   000

```

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***** S U M M A R Y O U T P U T *****

```

Input  filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\voin.dat
Output filename:  C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\16bdf02e-c17e-4494-809b-e844440fe48c\s
Summary filename:  C:\Users\ALOverholt\AppData\Local\Civica\XH5
\3212affb-35da-4852-9d0b-9c8922c19c40\16bdf02e-c17e-4494-809b-e844440fe48c\s

```

DATE: 01-15-2019

TIME: 11:41:38

USER:

COMMENTS: _____

** SIMULATION : Run 03 ** 10 YEAR STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								
MASS STORM [Ptot= 70.90 mm]		5.0						
** CALIB NASHYD [CN=79.9 [N = 3.0:Tp 0.56]	0501	1	1.0	4.80	0.18	12.50	24.11 0.34	0.000
MASS STORM [Ptot= 70.90 mm]		5.0						
** CALIB STANDHYD [I%=25.0:S%= 2.00]	0601	1	1.0	20.90	2.04	12.15	51.61 0.73	0.000
MASS STORM [Ptot= 70.90 mm]		5.0						
** CALIB STANDHYD [I%=60.0:S%= 2.00]	0603	1	1.0	2.60	0.43	12.00	57.04 0.80	0.000
ADD [0601+ 0603]	0701	3	1.0	23.50	2.26	12.10	52.21 n/a	0.000
ADD [0501+ 0701]	0702	3	1.0	28.30	2.37	12.12	48.55 n/a	0.000
MASS STORM [Ptot= 70.90 mm]		5.0						
** CALIB STANDHYD [I%=25.0:S%= 2.00]	0602	1	1.0	15.80	1.53	12.15	51.20 0.72	0.000
DUHYD	0901	1	1.0	15.80	1.53	12.15	51.20 n/a	0.000
MAJOR SYSTEM:	0901	2	1.0	0.00	0.00	0.00	n/a	0.000
MINOR SYSTEM:	0901	3	1.0	15.80	1.53	12.15	51.20 n/a	0.000
ADD [0702+ 0901]	0704	3	1.0	44.10	3.90	12.13	49.50 n/a	0.000
RESRVR [2: 0704] {ST= 1.17 ha.m }	0003	1	1.0	44.10	0.84	13.10	39.91 n/a	0.000
DIVERT HYD	0801	1	1.0	44.10	0.84	13.10	39.91 n/a	0.000
Outflow	0003	2	1.0	31.75	0.56	13.10	39.91 n/a	0.000
Outflow	0003	3	1.0	3.95	0.04	13.10	39.91 n/a	0.000
Outflow	0003	4	1.0	8.40	0.23	13.10	39.91 n/a	0.000
Outflow	0003	5	1.0	0.00	0.00	0.00	n/a	0.000
Outflow	0003	6	1.0	0.00	0.00	0.00	n/a	0.000
CHANNEL[2: 0801]	0001	1	1.0	3.95	0.04	13.10	39.91 n/a	0.000
ADD [0801+ 0901]	0703	3	1.0	31.75	0.56	13.10	39.91 n/a	0.000

```

*
*   MASS STORM                5.0
*   [ Ptot= 70.90 mm ]
**
** CALIB NASHYD                0204  1  5.0    0.99    0.01 12.58 13.15 0.19  0.000
*   [CN=49.0
*   [ N = 3.0:Tp 0.66]
*
*   CHANNEL[ 2: 0204]          0404  1  5.0    0.99    0.01 12.75 13.15 n/a  0.000
*
*   MASS STORM                5.0
*   [ Ptot= 70.90 mm ]
*
*   CALIB STANDHYD            0203  1  5.0    0.33    0.02 12.00 27.34 0.39  0.000
*   [I%=17.0:S%= 2.00]
*
*   ADD [ 0203+ 0404]          0306  3  5.0    1.32    0.03 12.00 16.70 n/a  0.000
*
*   MASS STORM                5.0
*   [ Ptot= 70.90 mm ]
*
*   CALIB STANDHYD            0201  1  5.0    1.56    0.13 12.00 32.53 0.46  0.000
*   [I%=28.8:S%= 2.00]
*
*   RESRVR [ 2: 0201]          0402  1  5.0    1.56    0.00 16.08 31.83 n/a  0.000
*   {ST= 0.03 ha.m }
*
*   ADD [ 0306+ 0402]          0305  3  5.0    2.88    0.03 12.00 24.89 n/a  0.000
*
*   CHANNEL[ 2: 0801]          0002  1  1.0    8.40    0.23 13.10 39.91 n/a  0.000
*
*   MASS STORM                5.0
*   [ Ptot= 70.90 mm ]
*
*   CALIB NASHYD                0202  1  5.0    6.48    0.14 12.75 23.38 0.33  0.000
*   [CN=71.0
*   [ N = 3.0:Tp 0.82]
*
*   MASS STORM                5.0
*   [ Ptot= 70.90 mm ]
*
*   CALIB STANDHYD            0205  1  5.0    11.14    1.20 12.00 43.42 0.61  0.000
*   [I%=41.9:S%= 2.00]
*
*   RESRVR [ 2: 0205]          0401  1  5.0    11.14    0.03 20.00 43.24 n/a  0.000
*   {ST= 0.36 ha.m }
*
*   ADD [ 0202+ 0401]          0301  3  5.0    17.62    0.16 12.75 35.94 n/a  0.000
*
*   ADD [ 0002+ 0301]          0307  3  1.0    26.02    0.39 13.00 27.45 n/a  0.000
*
=====
=====

```

```

      V   V   I   SSSSS  U   U   A   L
      V   V   I   SS    U   U   A A  L
      V   V   I   SS    U   U  AAAAA L
      V   V   I   SS    U   U  A   A  L
      VV    I   SSSSS  UUUUU  A   A  LLLLL

      OOO  TTTTT  TTTTT  H   H   Y   Y   M   M   OOO  TM
      O   O   T   T   H   H   Y   Y   MM  MM  O   O
      O   O   T   T   H   H   Y   Y   M   M  O   O

```

OOO T T H H Y M M OOO
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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files (x86)\visual OTTHYMO 5.0\vo2\vojn.dat
 Output filename: C:\Users\ALOverholt\AppData\Local\Civica\vh5
 \3212affb-35da-4852-9d0b-9c8922c19c40\aa070414-f2ba-42c8-8a11-c765f160e62e\s
 Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\vh5
 \3212affb-35da-4852-9d0b-9c8922c19c40\aa070414-f2ba-42c8-8a11-c765f160e62e\s

DATE: 01-15-2019 TIME: 11:41:41

USER:

COMMENTS: _____

 ** SIMULATION : Run 04 ** 25 YEAR STORM

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs									

	MASS STORM			5.0					
	[Ptot= 82.00 mm]								
*									
**	CALIB NASHYD	0501	1	1.0	4.80	0.23	12.48	31.13	0.38 0.000
	[CN=79.9								
	[N = 3.0:Tp 0.56]								
*									
	MASS STORM			5.0					
	[Ptot= 82.00 mm]								
*									
**	CALIB STANDHYD	0601	1	1.0	20.90	2.55	12.13	61.91	0.76 0.000
	[I%=25.0:S%= 2.00]								
*									
	MASS STORM			5.0					
	[Ptot= 82.00 mm]								
*									
**	CALIB STANDHYD	0603	1	1.0	2.60	0.51	12.00	67.41	0.82 0.000
	[I%=60.0:S%= 2.00]								
*									
	ADD [0601+ 0603]	0701	3	1.0	23.50	2.82	12.08	62.52	n/a 0.000
*									
	ADD [0501+ 0701]	0702	3	1.0	28.30	2.96	12.10	58.55	n/a 0.000
*									
	MASS STORM			5.0					
	[Ptot= 82.00 mm]								
*									
**	CALIB STANDHYD	0602	1	1.0	15.80	1.91	12.13	61.46	0.75 0.000
	[I%=25.0:S%= 2.00]								
*									
	DUHYD	0901	1	1.0	15.80	1.91	12.13	61.46	n/a 0.000
	MAJOR SYSTEM:	0901	2	1.0	0.00	0.00	0.00	0.00	n/a 0.000

```

*      MINOR SYSTEM:      0901  3  1.0  15.80   1.91 12.13  61.46  n/a  0.000
*
*  ADD [ 0702+ 0901] 0704  3  1.0  44.10   4.86 12.12  59.59  n/a  0.000
*
*  RESRVR [ 2: 0704] 0003  1  1.0  44.10   1.12 13.00  49.73  n/a  0.000
*    {ST= 1.37 ha.m }
*
*  DIVERT HYD      0801  1  1.0  44.10   1.12 13.00  49.73  n/a  0.000
*    Outflow      0003  2  1.0  30.39   0.66 13.00  49.73  n/a  0.000
*    Outflow      0003  3  1.0   3.55   0.05 13.00  49.73  n/a  0.000
*    Outflow      0003  4  1.0  10.16   0.42 13.00  49.73  n/a  0.000
*    Outflow      0003  5  1.0   0.00   0.00  0.00   0.00  n/a  0.000
*    Outflow      0003  6  1.0   0.00   0.00  0.00   0.00  n/a  0.000
*
*  CHANNEL[ 2: 0801] 0001  1  1.0   3.55   0.05 13.00  49.73  n/a  0.000
*
*  ADD [ 0801+ 0901] 0703  3  1.0  30.39   0.66 13.00  49.73  n/a  0.000
*
*  MASS STORM
*    [ Ptot= 82.00 mm ]
*
*  ** CALIB NASHYD      0204  1  5.0   0.99   0.02 12.58  17.37 0.21  0.000
*    [CN=49.0 ]
*    [ N = 3.0:Tp 0.66]
*
*  CHANNEL[ 2: 0204] 0404  1  5.0   0.99   0.02 12.75  17.37  n/a  0.000
*
*  MASS STORM
*    [ Ptot= 82.00 mm ]
*
*  * CALIB STANDHYD      0203  1  5.0   0.33   0.03 12.00  33.83 0.41  0.000
*    [I%=17.0:S%= 2.00]
*
*  ADD [ 0203+ 0404] 0306  3  5.0   1.32   0.03 12.00  21.48  n/a  0.000
*
*  MASS STORM
*    [ Ptot= 82.00 mm ]
*
*  * CALIB STANDHYD      0201  1  5.0   1.56   0.16 12.00  39.47 0.48  0.000
*    [I%=28.8:S%= 2.00]
*
*  RESRVR [ 2: 0201] 0402  1  5.0   1.56   0.00 16.25  38.77  n/a  0.000
*    {ST= 0.04 ha.m }
*
*  ADD [ 0306+ 0402] 0305  3  5.0   2.88   0.04 12.00  30.85  n/a  0.000
*
*  CHANNEL[ 2: 0801] 0002  1  1.0  10.16   0.42 13.00  49.73  n/a  0.000
*
*  MASS STORM
*    [ Ptot= 82.00 mm ]
*
*  * CALIB NASHYD      0202  1  5.0   6.48   0.18 12.75  30.42 0.37  0.000
*    [CN=71.0 ]
*    [ N = 3.0:Tp 0.82]
*
*  MASS STORM
*    [ Ptot= 82.00 mm ]
*
*  * CALIB STANDHYD      0205  1  5.0  11.14   1.52 12.00  52.07 0.64  0.000
*    [I%=41.9:S%= 2.00]
*
*  RESRVR [ 2: 0205] 0401  1  5.0  11.14   0.06 16.00  51.90  n/a  0.000
*    {ST= 0.41 ha.m }
*

```

```

*      ADD [ 0202+ 0401] 0301  3  5.0  17.62   0.21 12.75  44.00  n/a  0.000
*
*      ADD [ 0002+ 0301] 0307  3  1.0  27.78   0.62 12.93  35.53  n/a  0.000
*

```

FINISH

```

=====
=====
=====
=====

      V      V      I      SSSSS      U      U      A      L
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA      L
      V      V      I      SS      U      U      A      L
      VV      I      SSSSS      UUUUU      A      A      LLLLL

      000      TTTT      TTTT      H      H      Y      Y      M      M      000      TM
      O      O      T      T      H      H      Y      Y      MM      MM      O      O
      O      O      T      T      H      H      Y      Y      M      M      O      O
      000      T      T      H      H      Y      Y      M      M      000

```

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***** S U M M A R Y O U T P U T *****

```

Input filename: C:\Program Files (x86)\visual OTTHYMO 5.0\VO2\voin.dat
Output filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\597dff5b-7c86-42e7-bad7-62209150c686\s
Summary filename: C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\597dff5b-7c86-42e7-bad7-62209150c686\s

```

DATE: 01-15-2019

TIME: 11:41:40

USER:

COMMENTS: _____

```

*****
** SIMULATION : Run 05
*****

```

50 YEAR STORM

```

W/E COMMAND      HYD ID      DT      AREA      '      Qpeak      Tpeak      R.V.      R.C.      Qbase
                  min      ha      cms      hrs      mm

START @ 0.00 hrs
-----
MASS STORM      5.0
[ Ptot= 90.30 mm ]
*
** CALIB NASHYD      0501  1  1.0   4.80   0.27 12.48  36.63 0.41  0.000
   [CN=79.9 ]
   [ N = 3.0:Tp 0.56]
*
MASS STORM      5.0
[ Ptot= 90.30 mm ]

```



```

*
** CALIB STANDHYD      0601  1  1.0   20.90   2.94 12.12  69.71 0.77   0.000
[I%=25.0:S%= 2.00]
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
** CALIB STANDHYD      0603  1  1.0    2.60   0.57 12.00  75.23 0.83   0.000
[I%=60.0:S%= 2.00]
*
  ADD [ 0601+ 0603]    0701  3  1.0   23.50   3.29 12.07  70.32 n/a   0.000
*
  ADD [ 0501+ 0701]    0702  3  1.0   28.30   3.44 12.07  66.14 n/a   0.000
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
** CALIB STANDHYD      0602  1  1.0   15.80   2.20 12.12  69.24 0.77   0.000
[I%=25.0:S%= 2.00]
*
  DUHYD                0901  1  1.0   15.80   2.20 12.12  69.24 n/a   0.000
    MAJOR SYSTEM:      0901  2  1.0    0.00   0.00 0.00  0.00 n/a   0.000
    MINOR SYSTEM:      0901  3  1.0   15.80   2.20 12.12  69.24 n/a   0.000
*
  ADD [ 0702+ 0901]    0704  3  1.0   44.10   5.63 12.10  67.25 n/a   0.000
*
  RESRVR [ 2: 0704]    0003  1  1.0   44.10   1.45 12.88  57.24 n/a   0.000
  {ST= 1.50 ha.m }
*
  DIVERT HYD           0801  1  1.0   44.10   1.45 12.88  57.24 n/a   0.000
    Outflow            0003  2  1.0   29.63   0.84 12.88  57.24 n/a   0.000
    Outflow            0003  3  1.0    3.30   0.05 12.88  57.24 n/a   0.000
    Outflow            0003  4  1.0   11.17   0.56 12.88  57.24 n/a   0.000
    Outflow            0003  5  1.0    0.00   0.00 0.00  0.00 n/a   0.000
    Outflow            0003  6  1.0    0.00   0.00 0.00  0.00 n/a   0.000
*
  CHANNEL[ 2: 0801]    0001  1  1.0    3.30   0.05 12.88  57.24 n/a   0.000
*
  ADD [ 0801+ 0901]    0703  3  1.0   29.63   0.84 12.88  57.24 n/a   0.000
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
** CALIB NASHYD        0204  1  5.0    0.99   0.02 12.58  20.81 0.23   0.000
[CN=49.0
 [ N = 3.0:Tp 0.66]
*
  CHANNEL[ 2: 0204]    0404  1  5.0    0.99   0.02 12.75  20.81 n/a   0.000
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
  CALIB STANDHYD       0203  1  5.0    0.33   0.03 12.00  38.93 0.43   0.000
[I%=17.0:S%= 2.00]
*
  ADD [ 0203+ 0404]    0306  3  5.0    1.32   0.04 12.00  25.34 n/a   0.000
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
  CALIB STANDHYD       0201  1  5.0    1.56   0.18 12.00  44.88 0.50   0.000
[I%=28.8:S%= 2.00]
*
  RESRVR [ 2: 0201]    0402  1  5.0    1.56   0.00 16.42  44.18 n/a   0.000

```

```

      {ST= 0.05 ha.m }
*
  ADD [ 0306+ 0402]    0305  3  5.0    2.88   0.04 12.00  35.54 n/a   0.000
*
  CHANNEL[ 2: 0801]    0002  1  1.0   11.17   0.56 12.88  57.24 n/a   0.000
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
  CALIB NASHYD         0202  1  5.0    6.48   0.21 12.75  36.00 0.40   0.000
[CN=71.0
 [ N = 3.0:Tp 0.82]
*
  MASS STORM           5.0
  [ Ptot= 90.30 mm ]
*
  CALIB STANDHYD       0205  1  5.0   11.14   1.73 12.00  58.72 0.65   0.000
[I%=41.9:S%= 2.00]
*
  RESRVR [ 2: 0205]    0401  1  5.0   11.14   0.10 14.25  58.54 n/a   0.000
  {ST= 0.44 ha.m }
*
  ADD [ 0202+ 0401]    0301  3  5.0   17.62   0.29 13.00  50.25 n/a   0.000
*
  ADD [ 0002+ 0301]    0307  3  1.0   28.79   0.85 12.92  42.63 n/a   0.000
*
=====
=====

```

```

      V   V   I   SSSSS   U   U   A   L
      V   V   I   SS     U   U   A A   L
      V   V   I   SS     U   U   AAAAA L
      V   V   I   SS     U   U   A   A   L
      VV     I   SSSSS   UUUUU   A   A   LLLLL
      000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
      O   O   T   T   T   H   H   Y   Y   MM MM   O   O
      O   O   T   T   H   H   Y   M   M   O   O
      000   T   T   H   H   Y   M   M   000

```

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***** S U M M A R Y O U T P U T *****

```

Input  filename: C:\Program Files (x86)\Visual OTTHYMO 5.0\VO2\vojn.dat
Output filename:  C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\1cfbaf2e-00e8-4b08-887f-a0554a1a71d3\s
Summary filename:  C:\Users\ALOverholt\AppData\Local\Civica\VH5
\3212affb-35da-4852-9d0b-9c8922c19c40\1cfbaf2e-00e8-4b08-887f-a0554a1a71d3\s

```

DATE: 01-15-2019

TIME: 11:41:39

USER:

COMMENTS: _____

** SIMULATION : Run 06

** 100 YEAR STORM

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ 0.00 hrs								
MASS STORM [Ptot= 98.50 mm]	5.0							
** CALIB NASHYD [CN=79.9 [N = 3.0:Tp 0.56]	0501	1	1.0	4.80	0.32	12.48	42.24 0.43	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
** CALIB STANDHYD [I%=25.0:S%= 2.00]	0601	1	1.0	20.90	3.35	12.12	77.48 0.79	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
** CALIB STANDHYD [I%=60.0:S%= 2.00]	0603	1	1.0	2.60	0.64	12.00	83.02 0.84	0.000
ADD [0601+ 0603]	0701	3	1.0	23.50	3.76	12.07	78.10 n/a	0.000
ADD [0501+ 0701]	0702	3	1.0	28.30	3.94	12.07	73.73 n/a	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
** CALIB STANDHYD [I%=25.0:S%= 2.00]	0602	1	1.0	15.80	2.52	12.12	76.98 0.78	0.000
DUHYD	0901	1	1.0	15.80	2.52	12.12	76.98 n/a	0.000
MAJOR SYSTEM:	0901	2	1.0	0.05	0.13	12.12	76.98 n/a	0.000
MINOR SYSTEM:	0901	3	1.0	15.75	2.39	12.07	76.98 n/a	0.000
ADD [0702+ 0901]	0704	3	1.0	44.05	6.33	12.07	74.90 n/a	0.000
RESRVR [2: 0704] {ST= 1.62 ha.m }	0003	1	1.0	44.05	1.87	12.77	64.73 n/a	0.000
DIVERT HYD	0801	1	1.0	44.05	1.87	12.77	64.73 n/a	0.000
Outflow	0003	2	1.0	29.27	1.13	12.77	64.73 n/a	0.000
Outflow	0003	3	1.0	3.08	0.05	12.77	64.73 n/a	0.000
Outflow	0003	4	1.0	11.70	0.69	12.77	64.73 n/a	0.000
Outflow	0003	5	1.0	0.00	0.00	0.00	n/a	0.000
Outflow	0003	6	1.0	0.00	0.00	0.00	n/a	0.000
CHANNEL[2: 0801]	0001	1	1.0	3.08	0.05	12.77	64.73 n/a	0.000
ADD [0801+ 0901]	0703	3	1.0	29.32	1.13	12.77	64.75 n/a	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
** CALIB NASHYD [CN=49.0 [N = 3.0:Tp 0.66]	0204	1	5.0	0.99	0.02	12.58	24.43 0.25	0.000

CHANNEL[2: 0204]	0404	1	5.0	0.99	0.02	12.75	24.43 n/a	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
CALIB STANDHYD [I%=17.0:S%= 2.00]	0203	1	5.0	0.33	0.04	12.00	44.16 0.45	0.000
ADD [0203+ 0404]	0306	3	5.0	1.32	0.05	12.00	29.36 n/a	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
CALIB STANDHYD [I%=28.8:S%= 2.00]	0201	1	5.0	1.56	0.21	12.00	50.39 0.51	0.000
RESRVR [2: 0201] {ST= 0.05 ha.m }	0402	1	5.0	1.56	0.02	14.00	49.68 n/a	0.000
ADD [0306+ 0402]	0305	3	5.0	2.88	0.05	12.00	40.37 n/a	0.000
CHANNEL[2: 0801]	0002	1	1.0	11.70	0.69	12.77	64.73 n/a	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
CALIB NASHYD [CN=71.0 [N = 3.0:Tp 0.82]	0202	1	5.0	6.48	0.25	12.75	41.74 0.42	0.000
MASS STORM [Ptot= 98.50 mm]	5.0							
CALIB STANDHYD [I%=41.9:S%= 2.00]	0205	1	5.0	11.14	1.93	12.00	65.42 0.66	0.000
RESRVR [2: 0205] {ST= 0.46 ha.m }	0401	1	5.0	11.14	0.14	13.08	65.24 n/a	0.000
ADD [0202+ 0401]	0301	3	5.0	17.62	0.38	12.83	56.60 n/a	0.000
ADD [0002+ 0301]	0307	3	1.0	29.32	1.07	12.80	49.62 n/a	0.000

APPENDIX D:
PRELIMINARY SWM FACILITY DESIGN DETAILS

BlueVista Subdivision

Osler Bluff Road

117159

Dry Pond Volume Table

Active Pool

Side Slope 5 :1

Bottom Elev. 202.50

	Elev. (m)	Depth (m)	Areas		Live (m ³)	Accum. Live (m ³)
			Area (m ²)	Avg. Area (m ²)		
Bottom of Pond	202.50	0.00	425.00	0.00	0.0	0.0
	202.55	0.05	468.75	446.88	22.3	22.3
	202.60	0.10	512.50	490.63	24.5	46.9
	202.65	0.15	556.25	534.38	26.7	73.6
	202.70	0.20	600.00	578.13	28.9	102.5
	202.75	0.25	643.75	621.88	31.1	133.6
	202.80	0.30	687.50	665.63	33.3	166.9
	202.85	0.35	731.25	709.38	35.5	202.3
	202.90	0.40	775.00	753.13	37.7	240.0
	202.95	0.45	818.75	796.88	39.8	279.8
	203.00	0.50	862.50	840.63	42.0	321.9
	203.05	0.55	906.25	884.38	44.2	366.1
	203.10	0.60	950.00	928.13	46.4	412.5
	203.15	0.65	993.75	971.88	48.6	461.1
Weir	203.20	0.70	1037.50	1015.63	50.8	511.9
	203.25	0.75	1081.25	1059.38	53.0	564.8
	203.30	0.80	1125.00	1103.13	55.2	620.0
	203.35	0.85	1168.75	1146.88	57.3	677.3
	203.40	0.90	1212.50	1190.63	59.5	736.9
	203.45	0.95	1256.25	1234.38	61.7	798.6
	203.50	1.00	1300.00	1278.13	63.9	862.5
	203.55	1.05	1301.00	1300.50	65.0	927.5
Top of Pond	203.60	1.10	1302.00	1301.50	65.1	992.6

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Dry Pond Discharge Table

ORIFICE/PIPE CONTROL

Orifice Plate Outlet Pipe

diameter = 55 450 mm
area = 0.0024 0.1590 m²
Orifice C = 0.63 0.80
Invert = 202.50 202.50 m

WEIR CONTROL

Overflow

Length of Weir 5 m
Weir Sill Elevation 203.20 m
Weir constant K 1.6
Side Slope (H:V) 4

Q = flow rate (cms)

C = constant

A = area of opening(sq. m)

H = net head on the orifice

g = Acceleration due to gravity

$Q = K \times L \times H^{1.5}$

where Q = flow rate (cms)

K = constant

L = length (m)

H = head on the weir (m)

	Water Level (m)	Orifice		Outlet Pipe		Emergency Spillway		Hydraulic Control	Total Discharge (cms)
		Head (m)	Discharge (cms)	Head (m)	Discharge (cms)	Head (m)	Discharge (cms)		
Bottom of Pond	202.50	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	202.55	0.02	0.0010	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	202.60	0.07	0.0018	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	202.65	0.12	0.0023	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	202.70	0.17	0.0028	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	202.75	0.22	0.0031	0.03	0.0891	0.00	0.0000	ORIFICE	0.0031
	202.80	0.27	0.0035	0.08	0.1543	0.00	0.0000	ORIFICE	0.0035
	202.85	0.32	0.0038	0.13	0.1993	0.00	0.0000	ORIFICE	0.0038
	202.90	0.37	0.0040	0.18	0.2358	0.00	0.0000	ORIFICE	0.0040
	202.95	0.42	0.0043	0.23	0.2673	0.00	0.0000	ORIFICE	0.0043
Weir	203.00	0.47	0.0046	0.28	0.2955	0.00	0.0000	ORIFICE	0.0046
	203.05	0.52	0.0048	0.33	0.3213	0.00	0.0000	ORIFICE	0.0048
	203.10	0.57	0.0050	0.38	0.3451	0.00	0.0000	ORIFICE	0.0050
	203.15	0.62	0.0052	0.43	0.3674	0.00	0.0000	ORIFICE	0.0052
	203.20	0.67	0.0054	0.48	0.3884	0.00	0.0000	ORIFICE	0.0054
	203.25	0.72	0.0056	0.53	0.4084	0.05	0.0930	OVERFLOW	0.0987
	203.30	0.77	0.0058	0.58	0.4274	0.10	0.2732	OVERFLOW	0.2790
	203.35	0.82	0.0060	0.63	0.4455	0.15	0.5205	OVERFLOW	0.5265
	203.40	0.87	0.0062	0.68	0.4630	0.20	0.8300	OVERFLOW	0.8362
	203.45	0.92	0.0064	0.73	0.4799	0.25	1.2000	OVERFLOW	1.2064
Top of Pond	203.50	0.97	0.0065	0.78	0.4961	0.30	1.6300	OVERFLOW	1.6366
	203.55	1.02	0.0067	0.83	0.5119	0.35	2.1203	OVERFLOW	2.1270
	203.60	1.07	0.0069	0.88	0.5272	0.40	2.6715	OVERFLOW	2.6784

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Dry Pond Stage-Storage-Discharge Table

		Orifice	PIPE	Overflow			
Water Level		Orifice Plate	Outlet Pipe	Weir	Hydraulic	Total	Total Storage
(m)		Discharge (m ³ /s)	Discharge (m ³ /s)	Discharge (m ³ /s)	Control	Discharge (m ³ /s)	(ha-m)
Bottom of Pond	202.50	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0000
	202.55	0.0010	0.0000	0.0000	ORIFICE	0.000	0.0022
	202.60	0.0018	0.0000	0.0000	ORIFICE	0.000	0.0047
	202.65	0.0023	0.0000	0.0000	ORIFICE	0.000	0.0074
	202.70	0.0028	0.0000	0.0000	ORIFICE	0.000	0.0103
	202.75	0.0031	0.0250	0.0000	ORIFICE	0.003	0.0134
	202.80	0.0035	0.0750	0.0000	ORIFICE	0.003	0.0167
	202.85	0.0038	0.1250	0.0000	ORIFICE	0.004	0.0202
	202.90	0.0040	0.1750	0.0000	ORIFICE	0.004	0.0240
	202.95	0.0043	0.2250	0.0000	ORIFICE	0.004	0.0280
	203.00	0.0046	0.2750	0.0000	ORIFICE	0.005	0.0322
	203.05	0.0048	0.3250	0.0000	ORIFICE	0.005	0.0366
	203.10	0.0050	0.3750	0.0000	ORIFICE	0.005	0.0413
	203.15	0.0052	0.4250	0.0000	ORIFICE	0.005	0.0461
	203.20	0.0054	0.4750	0.0000	ORIFICE	0.005	0.0512
Weir	203.25	0.0056	0.5250	0.0930	OVERFLOW	0.099	0.0565
	203.30	0.0058	0.5750	0.2732	OVERFLOW	0.279	0.0620
	203.35	0.0060	0.6250	0.5205	OVERFLOW	0.527	0.0677
	203.40	0.0062	0.6750	0.8300	OVERFLOW	0.836	0.0737
	203.45	0.0064	0.7250	1.2000	OVERFLOW	1.206	0.0799
	203.50	0.0065	0.7750	1.6300	OVERFLOW	1.637	0.0863
	203.55	0.0067	0.8250	2.1203	OVERFLOW	2.127	0.0928
	203.60	0.0069	0.8750	2.6715	OVERFLOW	2.678	0.0993
Top of Pond							

25 mm W.L. Elev.
2-Year W.L. Elev.
5-Year W.L. Elev.
10-Year W.L. Elev.
25-Year W.L. Elev.
50-Year W.L. Elev.
100-Year W.L. Elev.
Timmins W.L. Elev.

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Wet Pond Volume Table

Active Pool
Side Slope Varies
Bottom Elev. 205.50
Permanent Pool 207.00

	Elev. (m)	Depth (m)	Areas		Storage		
			Area (m ²)	Avg. Area (m ²)	Dead (m ³)	Accum. Dead (m ³)	Live (m ³)
Bottom of Pond	205.50	0.00	1200.00	0.00	0.0	0.0	
	205.55	0.05	1258.33	1229.17	61.5	61.5	
	205.60	0.10	1316.67	1287.50	64.4	125.8	
	205.65	0.15	1375.00	1345.83	67.3	193.1	
	205.70	0.20	1433.33	1404.17	70.2	263.3	
	205.75	0.25	1491.67	1462.50	73.1	336.5	
	205.80	0.30	1550.00	1520.83	76.0	412.5	
	205.85	0.35	1608.33	1579.17	79.0	491.5	
	205.90	0.40	1666.67	1637.50	81.9	573.3	
	205.95	0.45	1725.00	1695.83	84.8	658.1	
	206.00	0.50	1783.33	1754.17	87.7	745.8	
	206.05	0.55	1841.67	1812.50	90.6	836.5	
	206.10	0.60	1900.00	1870.83	93.5	930.0	
	206.15	0.65	1958.33	1929.17	96.5	1026.5	
	206.20	0.70	2016.67	1987.50	99.4	1125.8	
	206.25	0.75	2075.00	2045.83	102.3	1228.1	
	206.30	0.80	2133.33	2104.17	105.2	1333.3	
	206.35	0.85	2191.67	2162.50	108.1	1441.5	
	206.40	0.90	2250.00	2220.83	111.0	1552.5	
	206.45	0.95	2308.33	2279.17	114.0	1666.5	
	206.50	1.00	2366.67	2337.50	116.9	1783.3	
	206.55	1.05	2425.00	2395.83	119.8	1903.1	
	206.60	1.10	2483.33	2454.17	122.7	2025.8	
	206.65	1.15	2541.67	2512.50	125.6	2151.5	
	206.70	1.20	2600.00	2570.83	128.5	2280.0	
	206.75	1.25	2658.33	2629.17	131.5	2411.5	
	206.80	1.30	2716.67	2687.50	134.4	2545.8	
Perm Pool	206.85	1.35	2775.00	2745.83	137.3	2683.1	
	206.90	1.40	2833.33	2804.17	140.2	2823.3	
	206.95	1.45	2891.67	2862.50	143.1	2966.5	
	207.00	1.50	2950.00	2920.83	146.0	3112.5	
	207.05	1.55	3265.63	3107.81			155.4
	207.10	1.60	3343.75	3304.69			165.2
	207.15	1.65	3421.88	3382.81			169.1
	207.20	1.70	3500.00	3460.94			173.0
	207.25	1.75	3578.13	3539.06			177.0
	207.30	1.80	3656.25	3617.19			180.9
	207.35	1.85	3734.38	3695.31			184.8
	207.40	1.90	3812.50	3773.44			188.7
	207.45	1.95	3890.63	3851.56			192.6
	207.50	2.00	3968.75	3929.69			196.5
	207.55	2.05	4046.88	4007.81			200.4
	207.60	2.10	4125.00	4085.94			204.3
	207.65	2.15	4203.13	4164.06			208.2
	207.70	2.20	4281.25	4242.19			212.1
	207.75	2.25	4359.38	4320.31			216.0
	207.80	2.30	4437.50	4398.44			219.9
	207.85	2.35	4515.63	4476.56			223.8
	207.90	2.40	4593.75	4554.69			227.7
	207.95	2.45	4671.88	4632.81			231.6
	208.00	2.50	4750.00	4710.94			235.5
	208.05	2.55	4828.13	4789.06			239.5
	208.10	2.60	4906.25	4867.19			243.4
	208.15	2.65	4984.38	4945.31			247.3
DICB	208.20	2.70	5062.50	5023.44			251.2
	208.25	2.75	5140.63	5101.56			255.1
	208.30	2.80	5218.75	5179.69			259.0
	208.35	2.85	5296.88	5257.81			262.9
	208.40	2.90	5375.00	5335.94			266.8
	208.45	2.95	5453.13	5414.06			270.7
	208.50	3.00	5531.25	5492.19			274.6
Overflow	208.55	3.05	5609.38	5570.31			278.5
	208.60	3.10	5687.50	5648.44			282.4
	208.65	3.15	5765.63	5726.56			286.3
	208.70	3.20	5843.75	5804.69			290.2
	208.75	3.25	5921.88	5882.81			294.1
	208.80	3.30	6000.00	5960.94			298.0
	208.85	3.35	6001.00	6000.50			300.0
Top of Pond	208.90	3.40	6002.00	6001.50			300.1

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Wet Pond Discharge Table

ORIFICE/PIPE CONTROL

Orifice Plate Outlet Pipe

diameter = 120 450 mm
area = 0.0113 0.1590 m²
Orifice C = 0.63 0.80
Invert = 207.00 207.00 m

Q = flow rate (cms)
C = constant
A = area of opening(sq. m)
H = net head on the orifice
g = Acceleration due to gravity

WEIR CONTROL

DICB Overflow

Length of Weir 0.6 7 m
Weir Sill Elevation 208.00 208.35 m
Weir constant K 1.6 1.6
Side Slope (H:V) 2 4

$$Q = K \times L \times H^{1.5}$$

where Q = flow rate (cms)

K = constant

L = length (m)

H = head on the weir (m)

	Water Level (m)	Orifice		Outlet Pipe		DICB		Emergency Spillway		Hydraulic Control	Total Discharge (cms)
		Head (m)	Discharge (cms)	Head (m)	Discharge (cms)	Head (m)	Discharge (cms)	Head (m)	Discharge (cms)		
Bottom of Pond Perm Pool	205.50	0.00	0.0000	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.00	0.00	0.0000	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.05	0.00	0.0000	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.10	0.04	0.0063	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.15	0.09	0.0095	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.20	0.14	0.0118	0.00	0.0000	0.00	0.0000	0.00	0.0000	ORIFICE	0.0000
	207.25	0.19	0.0138	0.03	0.0891	0.00	0.0000	0.00	0.0000	ORIFICE	0.0138
	207.30	0.24	0.0155	0.08	0.1543	0.00	0.0000	0.00	0.0000	ORIFICE	0.0155
	207.35	0.29	0.0170	0.13	0.1993	0.00	0.0000	0.00	0.0000	ORIFICE	0.0170
	207.40	0.34	0.0184	0.18	0.2358	0.00	0.0000	0.00	0.0000	ORIFICE	0.0184
	207.45	0.39	0.0197	0.23	0.2673	0.00	0.0000	0.00	0.0000	ORIFICE	0.0197
	207.50	0.44	0.0209	0.28	0.2955	0.00	0.0000	0.00	0.0000	ORIFICE	0.0209
	207.55	0.49	0.0221	0.33	0.3213	0.00	0.0000	0.00	0.0000	ORIFICE	0.0221
	207.60	0.54	0.0232	0.38	0.3451	0.00	0.0000	0.00	0.0000	ORIFICE	0.0232
	207.65	0.59	0.0242	0.43	0.3674	0.00	0.0000	0.00	0.0000	ORIFICE	0.0242
	207.70	0.64	0.0252	0.48	0.3884	0.00	0.0000	0.00	0.0000	ORIFICE	0.0252
	207.75	0.69	0.0262	0.53	0.4084	0.00	0.0000	0.00	0.0000	ORIFICE	0.0262
	207.80	0.74	0.0271	0.58	0.4274	0.00	0.0000	0.00	0.0000	ORIFICE	0.0271
	207.85	0.79	0.0281	0.63	0.4455	0.00	0.0000	0.00	0.0000	ORIFICE	0.0281
	207.90	0.84	0.0289	0.68	0.4630	0.00	0.0000	0.00	0.0000	ORIFICE	0.0289
	207.95	0.89	0.0298	0.73	0.4799	0.00	0.0000	0.00	0.0000	ORIFICE	0.0298
DICB	208.00	0.94	0.0306	0.78	0.4961	0.00	0.0000	0.00	0.0000	ORIFICE	0.0306
	208.05	0.99	0.0314	0.83	0.5119	0.05	0.0149	0.00	0.0000	DICB	0.0463
	208.10	1.04	0.0322	0.88	0.5272	0.10	0.0395	0.00	0.0000	DICB	0.0717
	208.15	1.09	0.0330	0.93	0.5420	0.15	0.0754	0.00	0.0000	DICB	0.1084
	208.20	1.14	0.0337	0.98	0.5565	0.20	0.1227	0.00	0.0000	DICB	0.1564
Overflow	208.25	1.19	0.0344	1.03	0.5706	0.25	0.1813	0.00	0.0000	DICB	0.2158
	208.30	1.24	0.0351	1.08	0.5843	0.30	0.2513	0.00	0.0000	DICB	0.2864
	208.35	1.29	0.0358	1.13	0.5978	0.35	0.3325	0.00	0.0000	DICB	0.3684
	208.40	1.34	0.0365	1.18	0.6109	0.40	0.4251	0.05	0.1288	Overflow	0.5904
	208.45	1.39	0.0372	1.23	0.6238	0.45	0.5290	0.10	0.3744	Overflow	0.9406
	208.50	1.44	0.0379	1.28	0.6364	0.50	0.6442	0.15	0.7064	Overflow	1.3428
	208.55	1.49	0.0385	1.33	0.6487	0.55	0.7708	0.20	1.1162	Overflow	1.7650
	208.60	1.54	0.0392	1.38	0.6609	0.60	0.9087	0.25	1.6000	Overflow	2.2609
	208.65	1.59	0.0398	1.43	0.6728	0.65	1.0579	0.30	2.1558	Overflow	2.8286
	208.70	1.64	0.0404	1.48	0.6845	0.70	1.2184	0.35	2.7829	Overflow	3.4674
Top of Pond	208.75	1.69	0.0410	1.53	0.6960	0.75	1.3903	0.40	3.4810	Overflow	4.1770
	208.80	1.74	0.0416	1.58	0.7073	0.80	1.5735	0.45	4.2503	Overflow	4.9576
	208.85	1.79	0.0422	1.63	0.7184	0.85	1.7680	0.50	5.0912	Overflow	5.8096
	208.90	1.84	0.0428	1.68	0.7294	0.90	1.9738	0.55	6.0042	Overflow	6.7335

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Wet Pond Stage-Storage-Discharge Table

		Orifice	PIPE	DICB	Overflow			
Water Level		50 mm Orifice Plate	750 mm Outlet Pipe	0.6 m DICB with 2:1 side slope	Weir	Hydraulic Control	Total Discharge	Total Storage
(m)		Discharge (m³/s)	Discharge (m³/s)	Discharge (m³/s)	Discharge (m³/s)		(m³/s)	(ha-m)
Bottom of Pond Perm Pool	205.50	0.0000	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0000
	207.00	0.0000	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0000
	207.05	0.0000	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0155
	207.10	0.0063	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0321
	207.15	0.0095	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0490
	207.20	0.0118	0.0000	0.0000	0.0000	ORIFICE	0.000	0.0663
	207.25	0.0138	0.0250	0.0000	0.0000	ORIFICE	0.014	0.0840
	207.30	0.0155	0.0750	0.0000	0.0000	ORIFICE	0.015	0.1021
	207.35	0.0170	0.1250	0.0000	0.0000	ORIFICE	0.017	0.1205
	207.40	0.0184	0.1750	0.0000	0.0000	ORIFICE	0.018	0.1394
	207.45	0.0197	0.2250	0.0000	0.0000	ORIFICE	0.020	0.1587
	207.50	0.0209	0.2750	0.0000	0.0000	ORIFICE	0.021	0.1783
	207.55	0.0221	0.3250	0.0000	0.0000	ORIFICE	0.022	0.1984
	207.60	0.0232	0.3750	0.0000	0.0000	ORIFICE	0.023	0.2188
	207.65	0.0242	0.4250	0.0000	0.0000	ORIFICE	0.024	0.2396
	207.70	0.0252	0.4750	0.0000	0.0000	ORIFICE	0.025	0.2608
	207.75	0.0262	0.5250	0.0000	0.0000	ORIFICE	0.026	0.2824
	207.80	0.0271	0.5750	0.0000	0.0000	ORIFICE	0.027	0.3044
	207.85	0.0281	0.6250	0.0000	0.0000	ORIFICE	0.028	0.3268
	207.90	0.0289	0.6750	0.0000	0.0000	ORIFICE	0.029	0.3496
DICB	207.95	0.0298	0.7250	0.0000	0.0000	ORIFICE	0.030	0.3727
	208.00	0.0306	0.7750	0.0000	0.0000	ORIFICE	0.031	0.3963
	208.05	0.0314	0.8250	0.0149	0.0000	DICB	0.046	0.4202
	208.10	0.0322	0.8750	0.0395	0.0000	DICB	0.072	0.4446
	208.15	0.0330	0.9250	0.0754	0.0000	DICB	0.108	0.4693
	208.20	0.0337	0.9750	0.1227	0.0000	DICB	0.156	0.4944
	208.25	0.0344	1.0250	0.1813	0.0000	DICB	0.216	0.5199
	208.30	0.0351	1.0750	0.2513	0.0000	DICB	0.286	0.5458
	208.35	0.0358	1.1250	0.3325	0.0000	DICB	0.368	0.5721
	208.40	0.0365	1.1750	0.4251	0.1288	Overflow	0.590	0.5988
Overflow	208.45	0.0372	1.2250	0.5290	0.3744	Overflow	0.941	0.6259
	208.50	0.0379	1.2750	0.6442	0.7064	Overflow	1.343	0.6533
	208.55	0.0385	1.3250	0.7708	1.1162	Overflow	1.765	0.6812
	208.60	0.0392	1.3750	0.9087	1.6000	Overflow	2.261	0.7094
	208.65	0.0398	1.4250	1.0579	2.1558	Overflow	2.829	0.7380
	208.70	0.0404	1.4750	1.2184	2.7829	Overflow	3.467	0.7671
	208.75	0.0410	1.5250	1.3903	3.4810	Overflow	4.177	0.7965
	208.80	0.0416	1.5750	1.5735	4.2503	Overflow	4.958	0.8263
	208.85	0.0422	1.6250	1.7680	5.0912	Overflow	5.810	0.8563
	208.90	0.0428	1.6750	1.9738	6.0042	Overflow	6.734	0.8863
Top of Pond								

25 mm W.L. Elev.

2-Year W.L. Elev.

5-Year W.L. Elev.

10-Year W.L. Elev.

25-Year W.L. Elev.

50-Year W.L. Elev.

100-Year W.L. Elev.

Timmins W.L. Elev.

117159 - BlueVista Subdivision
SWM Facility Design Calculations
Using MOE SWMPD Manual / March 2003
FOREBAY SIZING CALCULATIONS

Wet Pond

1) Settling

Dist	=	$\text{SQRT}(r \cdot Q_p / V_s)$	Dist = Forebay length (m)		
			r = Length to width ratio	r	= 2.0000
			Qp = 25 mm SWM outflow - water quality (cms)	Qp	= 0.0150 cms
			Vs = settling velocity for 0.15 mm particles (m/s)	Vs	= 0.0003 m/s
Dist	=	10.00 m	Actual forebay length =	25 m	

2) Dispersion Length

Dist	=	$8 \cdot Q / d \cdot V_f$	Dist = Length of dispersion (m)		
			Q = 5 Yr max inlet flow (cms)	Q	= 1.3060 cms
			d = depth of permanent pool in forebay (m)	d	= 1.0000 m
			Vf = desired velocity in forebay (m/s)	Vf	= 0.5000 m/s
Dist	=	20.90 m	Actual forebay length =	25 m	

3) Cleanout Frequency

Table 6.3 MOE SWMPD Manual

Cleanout	=	$\text{Vol} / (\text{load} \cdot \text{Asew} \cdot \text{eff.})$	Asew = contributing sewer area (ha)	Asew	= 11.1 ha
			Actual Forebay Length	Alength	= 25.00 m
			Imp = avg. percent Impervious (%)	Imp	= 50 %
			load = sediment loading (cu.m/ha)	load	= 0.6 cu.m/ha
			eff. = removal efficiency (%)	eff.	= 80%
			Targ = cleanout Frequency Target (Years)	Targ	= 10 years
			Vol = bottom 0.5 m volume (cu.m)	Vol	= 384 cu.m
Cleanout	=	72 years			

BlueVista Subdivision
FILE No. 117159
Nov-18
DRAWDOWN TIME FOR EROSION CONTROL
(Using the falling head orifice equation)

Dry Pond

$$t = \frac{2 A_p}{C A_o (2g)^{0.5}} \quad (h_1^{0.5} - h_2^{0.5})$$

Value

where t = drawdown time in seconds

A_p = surface area of pond (m²)

666 m²

C = discharge coefficient (typically 0.63)

0.63

A_o = cross-sectional area of orifice (m²)

0.002376 m²

55 mm diameter

g = gravitational acceleration constant (9.81 m/s²)

9.81 m/s²

h₁ = starting water elevation above the orifice (m)

0.55 m

h₂ = ending water elevation above the orifice (m)

0.00 m

$$t = \frac{2 * 2717}{0.63 * 0.01131 * (2 * 9.81)^{0.5}} \quad (0.39^{0.5} - 0^{0.5})$$

t = 148,886.08 seconds

t = 41.36 hours

BlueVista Subdivision
FILE No. 117159
Nov-18
DRAWDOWN TIME FOR SURFACE STORAGE
(Using the falling head orifice equation)

Dry Pond

$$t = \frac{2 A_p}{C A_o (2g)^{0.5}}$$

$$(h_1^{0.5} - h_2^{0.5})$$

Value

where t = drawdown time in seconds

A_p = surface area of pond (m²)

731 m²

C = discharge coefficient (typically 0.63)

0.63

A_o = cross-sectional area of orifice (m²)

0.002376 m²

55 mm diameter

g = gravitational acceleration constant (9.81 m/s²)

9.81 m/s²

h₁ = starting water elevation above the orifice (m)

0.70 m

h₂ = ending water elevation above the orifice (m)

0.00 m

$$t = \frac{2 * 2717}{0.63 * 0.01131 * (2 * 9.81)^{0.5}}$$

$$(0.39^{0.5} - 0^{0.5})$$

t = 184,560.85 seconds

t = 51.27 hours

BlueVista Subdivision
FILE No. 117159
Nov-18
DRAWDOWN TIME FOR EROSION CONTROL
(Using the falling head orifice equation)

Wet Pond

$$t = \frac{2 A_p}{C A_o (2g)^{0.5}} (h_1^{0.5} - h_2^{0.5})$$

Value

where t = drawdown time in seconds

A_p = surface area of pond (m²)

3615 m²

C = discharge coefficient (typically 0.63)

0.63

A_o = cross-sectional area of orifice (m²)

0.01131 m²

120 mm diameter

g = gravitational acceleration constant (9.81 m/s²)

9.81 m/s²

h₁ = starting water elevation above the orifice (m)

0.70 m

h₂ = ending water elevation above the orifice (m)

0.00 m

$$t = \frac{2 * 2717}{0.63 * 0.01131 * (2 * 9.81)^{0.5}} (0.39^{0.5} - 0^{0.5})$$

t = 191,665.92 seconds

t = 53.24 hours

BlueVista Subdivision
FILE No. 117159
Nov-18
DRAWDOWN TIME FOR SURFACE STORAGE
(Using the falling head orifice equation)

Wet Pond

$$t = \frac{2 A_p}{C A_o (2g)^{0.5}} (h_1^{0.5} - h_2^{0.5})$$

Value

where t = drawdown time in seconds

A_p = surface area of pond (m²)

3850 m²

C = discharge coefficient (typically 0.63)

0.63

A_o = cross-sectional area of orifice (m²)

0.01131 m²

120 mm diameter

g = gravitational acceleration constant (9.81 m/s²)

9.81 m/s²

h₁ = starting water elevation above the orifice (m)

1.00 m

h₂ = ending water elevation above the orifice (m)

0.00 m

$$t = \frac{2 * 2717}{0.63 * 0.01131 * (2 * 9.81)^{0.5}} (0.39^{0.5} - 0^{0.5})$$

t = 243,976.67 seconds

t = 67.77 hours

APPENDIX E:
POST DEVELOPMENT HYDRAULIC ANALYSIS

HY-8 Culvert Analysis Report

Existing 600 mm Diameter Culvert Crossing at County Road 21

Crossing Discharge Data

Discharge Selection Method: User Defined

Table 1 - Summary of Culvert Flows at Crossing: EX. 600 mm CULVERT (PostDev)

Headwater Elevation (m)	Discharge Names	Total Discharge (cms)	Culvert 1 Discharge (cms)	Roadway Discharge (cms)	Iterations
203.49	25mm	0.05	0.05	0.00	1
203.58	2YR-SCS	0.10	0.10	0.00	1
203.85	5YR-SCS	0.25	0.25	0.00	1
204.01	10YR-SCS	0.39	0.39	0.00	1
204.86	25YR-SCS	0.62	0.62	0.00	1
206.14	50YR-SCS	0.85	0.85	0.00	1
207.72	100YR-SCS	1.07	1.07	0.00	1
207.80	Regional	2.27	1.08	1.18	4
207.73	Overtopping	1.07	1.07	0.00	Overtopping

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cms)	Culvert Discharge (cms)	Headwater Elevation (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	Flow Type	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwater Depth (m)	Outlet Velocity (m/s)	Tailwater Velocity (m/s)
25mm	0.05	0.05	203.49	0.205	0.0*	1-S2n	0.139	0.140	0.139	0.021	0.967	0.170
2YR-SCS	0.10	0.10	203.58	0.297	0.0*	1-S2n	0.199	0.200	0.199	0.032	1.180	0.224
5YR-SCS	0.25	0.25	203.85	0.515	0.565	2-M2c	0.335	0.324	0.324	0.056	1.606	0.322
10YR-SCS	0.39	0.39	204.01	0.725	0.731	7-M2c	0.466	0.408	0.408	0.073	1.905	0.384
25YR-SCS	0.62	0.62	204.86	1.223	1.580	7-M2c	0.600	0.510	0.510	0.096	2.422	0.462
50YR-SCS	0.85	0.85	206.14	2.001	2.860	7-M2c	0.600	0.563	0.563	0.116	3.084	0.522
100YR-SCS	1.07	1.07	207.72	2.995	4.437	6-FFc	0.600	0.600	0.600	0.133	3.784	0.571
Regional	2.27	1.08	207.80	3.045	4.515	6-FFc	0.600	0.600	0.600	0.209	3.819	0.765

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

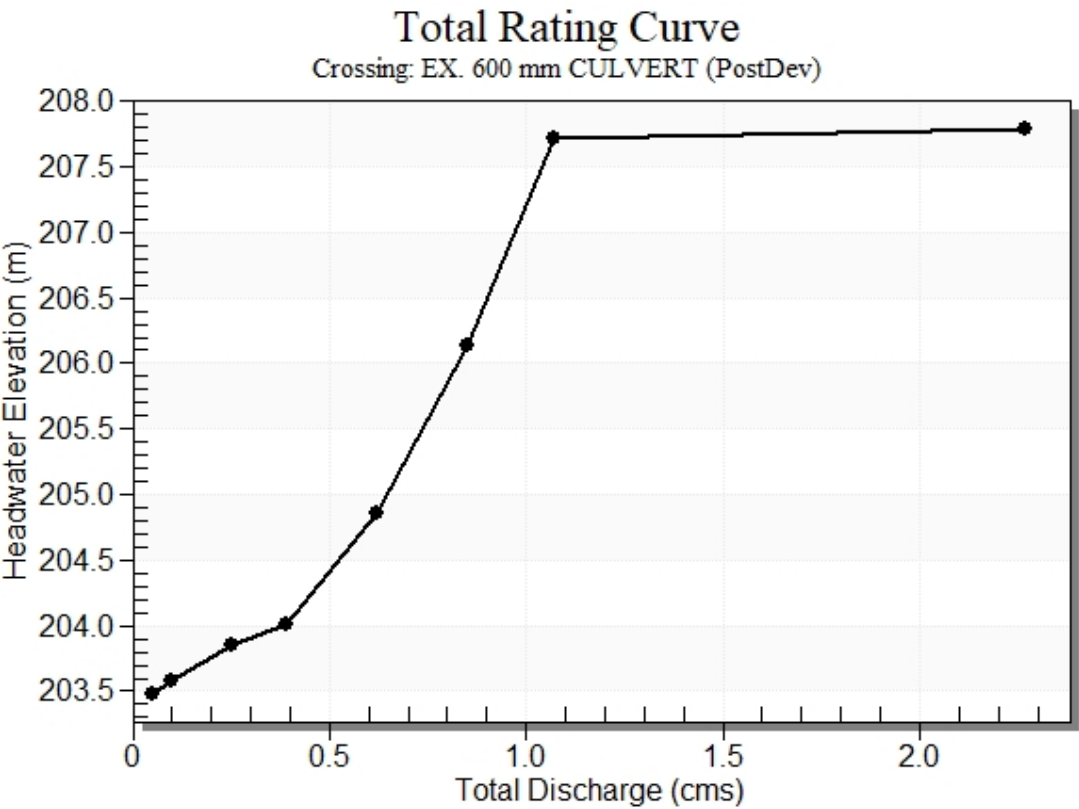
Inlet Elevation (invert): 203.28 m, Outlet Elevation (invert): 202.88 m

Culvert Length: 27.70 m, Culvert Slope: 0.0144

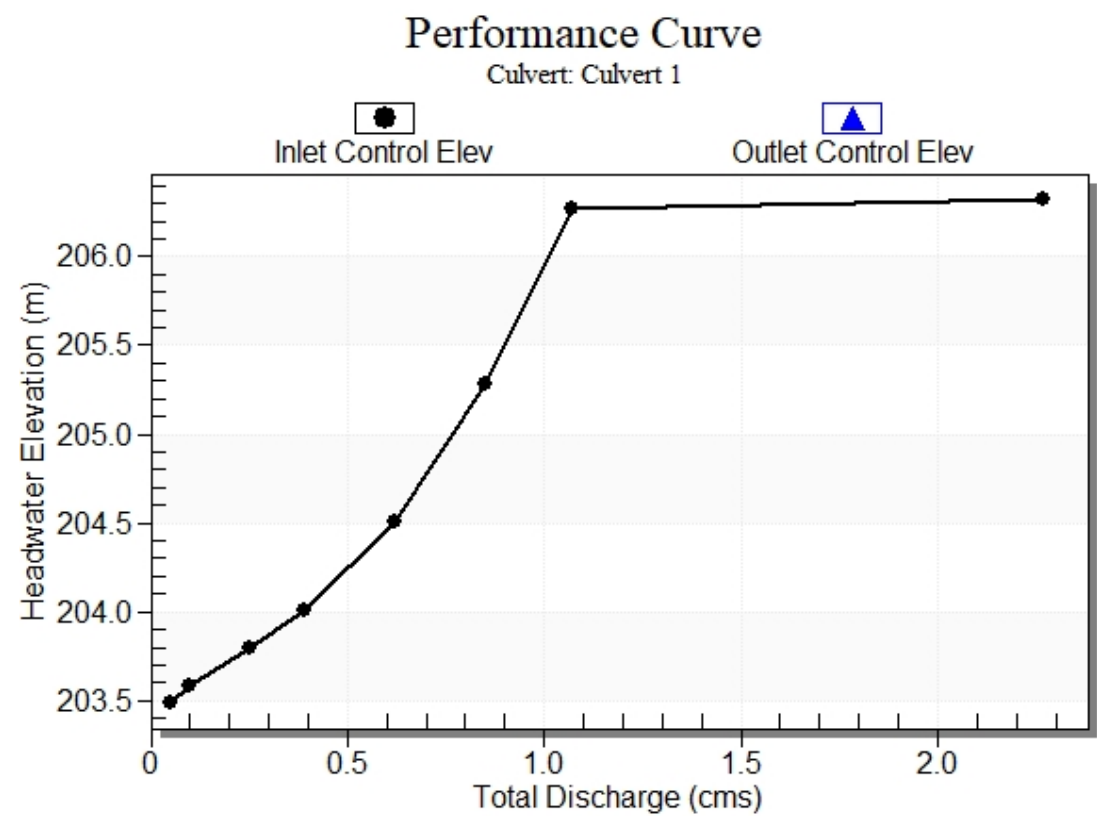
Table 3 - Downstream Channel Rating Curve (Crossing: EX. 600 mm CULVERT (PostDev))

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.05	202.90	0.02	0.17	2.09	0.37
0.10	202.91	0.03	0.22	3.16	0.40
0.25	202.94	0.06	0.32	5.47	0.44
0.39	202.95	0.07	0.38	7.15	0.46
0.62	202.98	0.10	0.46	9.43	0.48
0.85	203.00	0.12	0.52	11.39	0.49
1.07	203.01	0.13	0.57	13.08	0.50
2.27	203.09	0.21	0.76	20.51	0.54

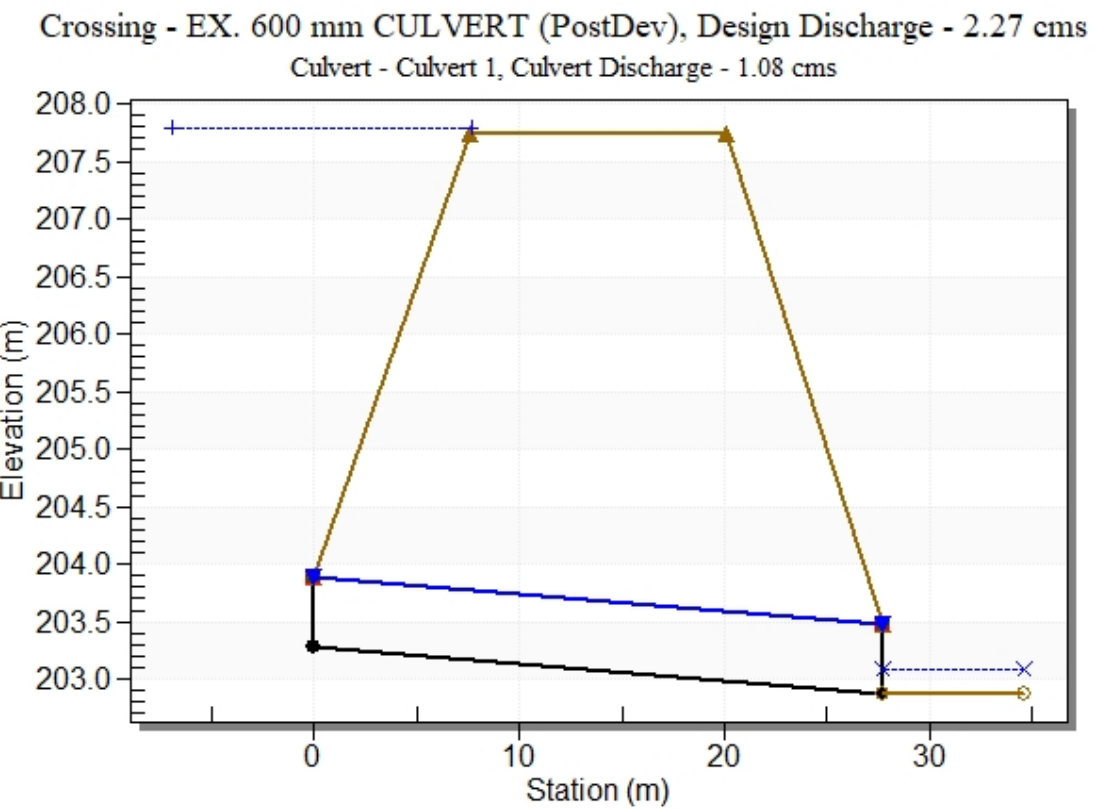
Rating Curve Plot for Crossing: EX. 600 mm CULVERT (PostDev)



Culvert Performance Curve Plot: Culvert 1



Water Surface Profile Plot for Culvert: Culvert 1



Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 203.28 m

Outlet Station: 27.70 m

Outlet Elevation: 202.88 m

Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Circular

Barrel Diameter: 600.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

Tailwater Channel Data - EX. 600 mm CULVERT (PostDev)

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 13.77 m

Side Slope (H:V): 2.00 (2:1)

Channel Slope: 0.0100

Channel Manning's n: 0.0450

Channel Invert Elevation: 202.88 m

Roadway Data for Crossing: EX. 600 mm CULVERT (PostDev)

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 43.28 m

Crest Elevation: 207.73 m

Roadway Surface: Paved

Roadway Top Width: 12.50 m

HY-8 Culvert Analysis Report

Proposed 600 mm Diameter Culvert Crossing At Street 'A'

Crossing Discharge Data

Discharge Selection Method: User Defined

Table 1 - Summary of Culvert Flows at Crossing: PROP. 600 mm CULVERT (PostDev)

Headwater Elevation (m)	Discharge Names	Total Discharge (cms)	Culvert 1 Discharge (cms)	Roadway Discharge (cms)	Iterations
209.44	25mm	0.02	0.02	0.00	1
209.51	2YR-SCS	0.04	0.04	0.00	1
209.59	5YR-SCS	0.08	0.08	0.00	1
209.65	10YR-SCS	0.11	0.11	0.00	1
209.72	25YR-SCS	0.15	0.15	0.00	1
209.78	50YR-SCS	0.19	0.19	0.00	1
209.83	100YR-SCS	0.22	0.22	0.00	1
210.23	Timmins	0.40	0.40	0.00	1
210.60	Overtopping	0.51	0.51	0.00	Overtopping

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cms)	Culvert Discharge (cms)	Headwater Elevation (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	Flow Type	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwater Depth (m)	Outlet Velocity (m/s)	Tailwater Velocity (m/s)
25mm	0.02	0.02	209.44	0.126	0.138	2-M2c	0.111	0.085	0.085	0.013	0.771	0.139
2YR-SCS	0.04	0.04	209.51	0.192	0.210	2-M2c	0.167	0.130	0.130	0.022	0.957	0.192
5YR-SCS	0.08	0.08	209.59	0.268	0.295	2-M2c	0.234	0.180	0.180	0.032	1.138	0.245
10YR-SCS	0.11	0.11	209.65	0.316	0.349	2-M2c	0.278	0.210	0.210	0.038	1.244	0.276
25YR-SCS	0.15	0.15	209.72	0.379	0.421	2-M2c	0.337	0.250	0.250	0.047	1.366	0.312
50YR-SCS	0.19	0.19	209.78	0.431	0.479	2-M2c	0.389	0.280	0.280	0.053	1.455	0.338
100YR-SCS	0.22	0.22	209.83	0.481	0.534	2-M2c	0.447	0.306	0.306	0.059	1.543	0.361
Timmins	0.40	0.40	210.23	0.750	0.926	7-M2c	0.600	0.415	0.415	0.083	1.932	0.449

Straight Culvert

Inlet Elevation (invert): 209.30 m, Outlet Elevation (invert): 209.17 m

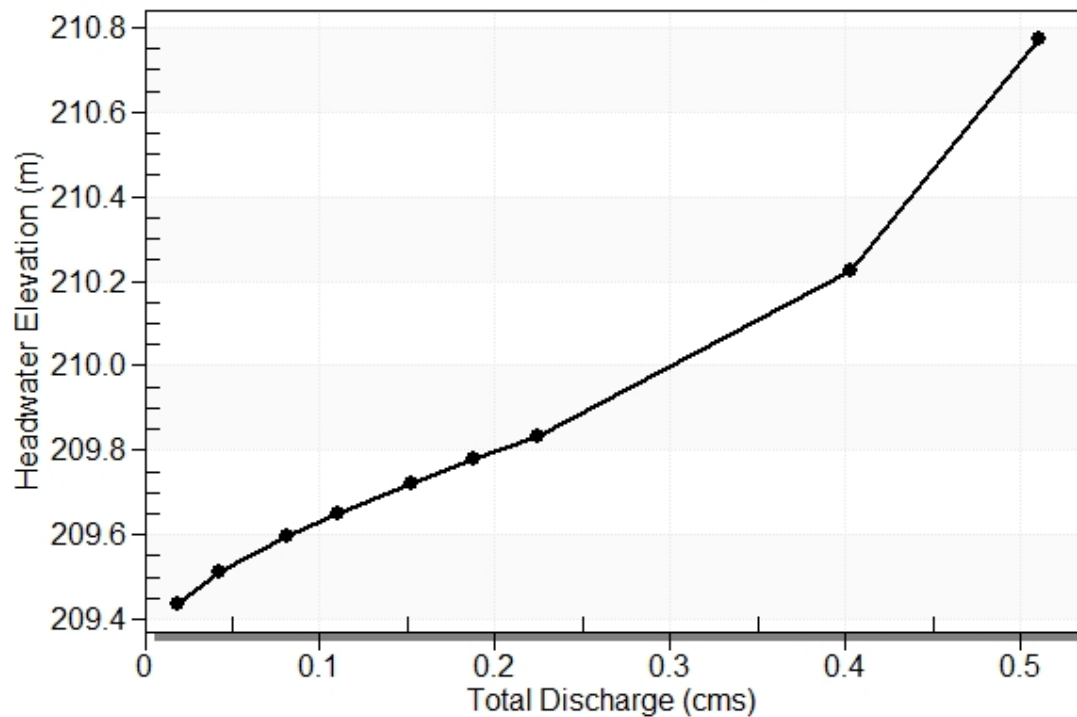
Culvert Length: 25.00 m, Culvert Slope: 0.0052

Table 3 - Downstream Channel Rating Curve (Crossing: PROP. 600 mm CULVERT (PostDev))

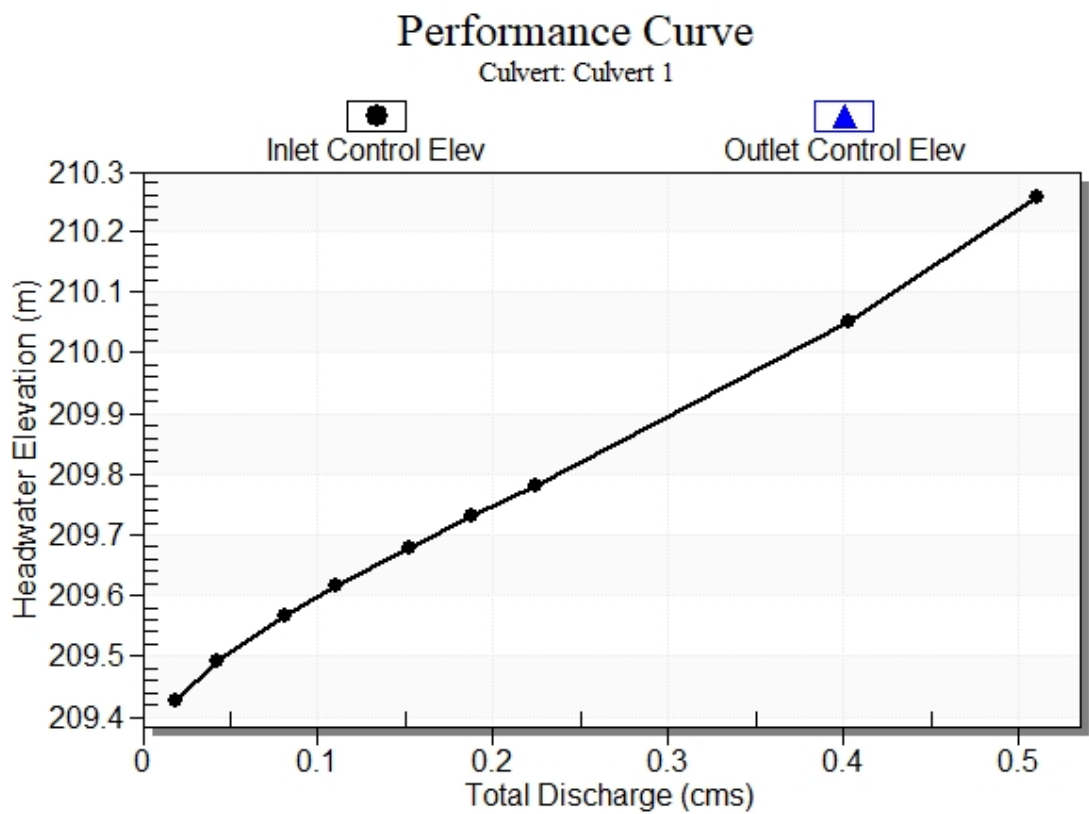
Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.02	209.18	0.01	0.14	1.65	0.39
0.04	209.19	0.02	0.19	2.69	0.42
0.08	209.20	0.03	0.25	3.92	0.44
0.11	209.21	0.04	0.28	4.71	0.46
0.15	209.22	0.05	0.31	5.70	0.47
0.19	209.22	0.05	0.34	6.47	0.48
0.22	209.23	0.06	0.36	7.18	0.49
0.40	209.25	0.08	0.45	10.15	0.52

Total Rating Curve

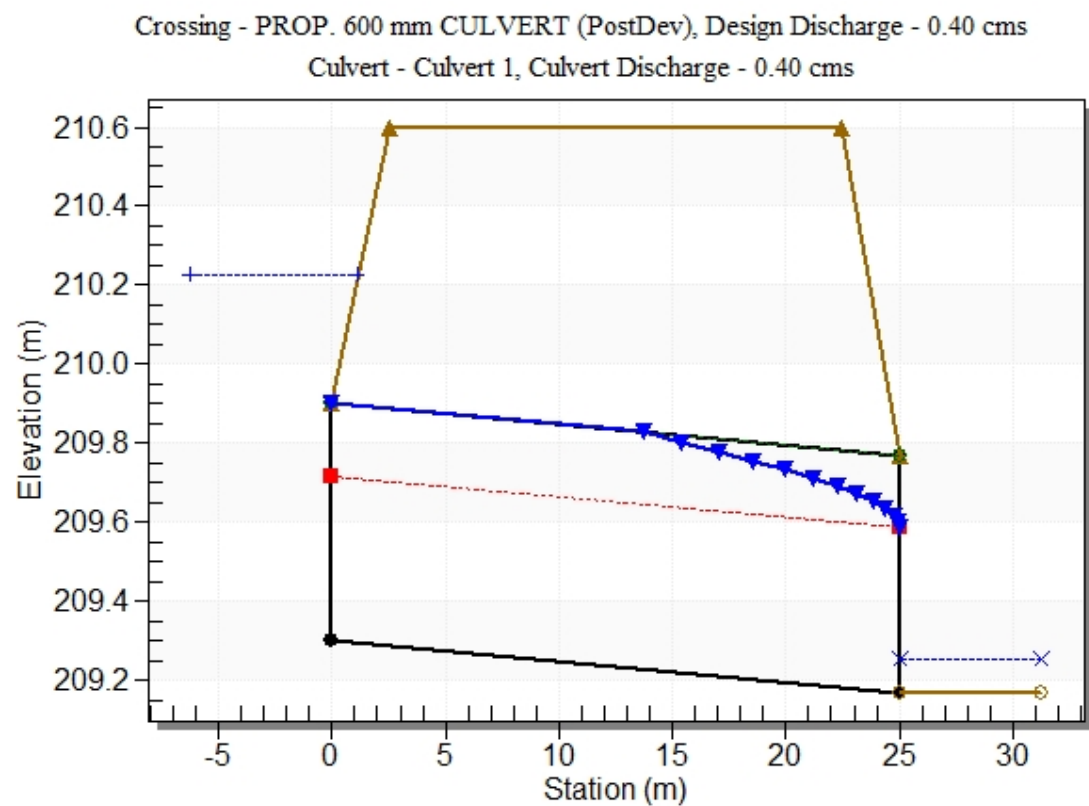
Crossing: PROP. 600 mm CULVERT (PostDev)



Culvert Performance Curve Plot: Culvert 1



Water Surface Profile Plot for Culvert: Culvert 1



Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 209.30 m

Outlet Station: 25.00 m

Outlet Elevation: 209.17 m

Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Circular

Barrel Diameter: 600.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

Tailwater Channel Data - PROP. 600 mm CULVERT (PostDev)

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 10.00 m

Side Slope (H:V): 10.00 (1:1)

Channel Slope: 0.0125

Channel Manning's n: 0.0450

Channel Invert Elevation: 209.17 m

Roadway Data for Crossing: PROP. 600 mm CULVERT (PostDev)

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 50.00 m

Crest Elevation: 210.60 m

Roadway Surface: Paved

Roadway Top Width: 20.00 m



C.C. Tatham & Associates Ltd.
Consulting Engineers
Collingwood Bracebridge Orillia Barrie

Project: BlueVista

Date: December 2018

File No.: 117159

Designed: ARO

Subject: 100 - Year Peak Flows

Checked: DRT

(Municipal Standard - TOBM)

<u>IDF Parameters</u>		<u>Peak Rainfall Intensity</u>	
5 YR	100 YR	5 Year	= 78.30 mm/hr
A 29.1	47.7	100 Year	= 132.69 mm/hr
B -0.71	-0.738		

Catchment 201 Rear Lot Grass Swale to Dry Pond

Drainage Area (ha)	0.06
5 year Runoff Coefficient (C)	0.48
100 year Runoff Coefficient (C)	0.74
Time of Concentration (min)	15
5-Year Peak Flow (m ³ /s)	0.006
100 - Year Peak Flow (m³/s)	0.016

Catchment 201 Service Easement Swale to Dry Pond

Drainage Area (ha)	1.50
5 year Runoff Coefficient (C)	0.55
100 year Runoff Coefficient (C)	0.78
Time of Concentration (min)	15
5-Year Peak Flow (m ³ /s)	0.179
100 - Year Peak Flow to Swale (m³/s)	0.428

Overland Flow (100 Yr - 5 Yr) 0.249

Catchment 204 Rear Lot Grass Swale to North

Drainage Area (ha)	0.99
5 year Runoff Coefficient (C)	0.48
100 year Runoff Coefficient (C)	0.74
Time of Concentration (min)	15
5-Year Peak Flow (m ³ /s)	0.103
100 - Year Peak Flow (m³/s)	0.270

Catchment 205 Overland Flow Swale to Wet Pond

Drainage Area (ha)	11.14
5 year Runoff Coefficient (C)	0.55
100 year Runoff Coefficient (C)	0.78
Time of Concentration (min)	15
5-Year Peak Flow (m ³ /s)	1.333
100 - Year Peak Flow (m ³ /s)	3.182

Overland Flow (100 Yr - 5 Yr) 1.850

Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Jan 15 2019

Swale 1: Catchment 201 Rear Lot Grass Swale to Dry Pond

Triangular

Side Slopes (z:1) = 3.0000, 3.0000
Total Depth (m) = 0.1500

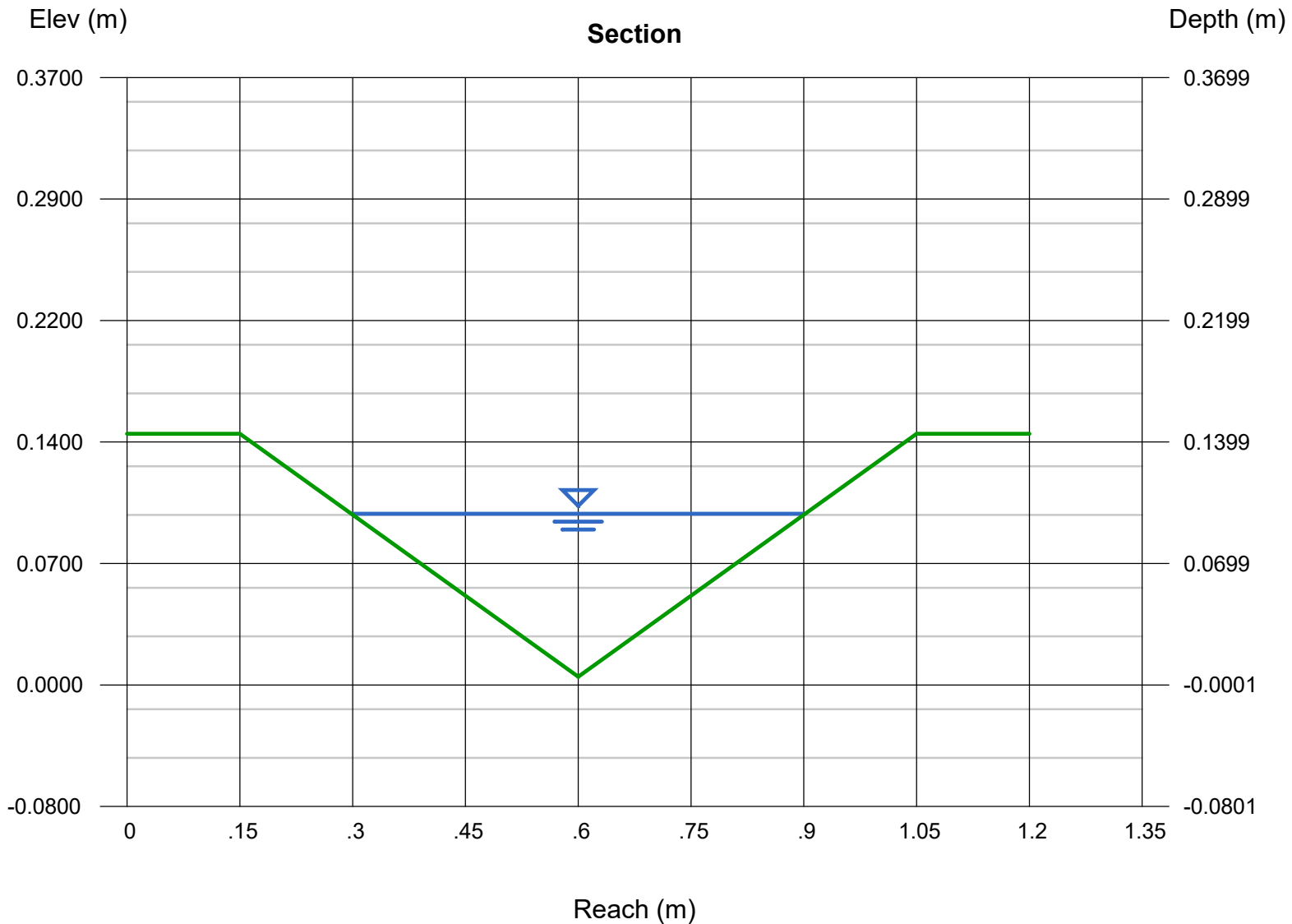
Invert Elev (m) = 0.0001
Slope (%) = 2.2500
N-Value = 0.035

Calculations

Compute by: Known Q
Known Q (cms) = 0.0160

Highlighted

Depth (m) = 0.1006
Q (cms) = 0.016
Area (sqm) = 0.0304
Velocity (m/s) = 0.5272
Wetted Perim (m) = 0.6361
Crit Depth, Yc (m) = 0.0914
Top Width (m) = 0.6035
EGL (m) = 0.1148



Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Jan 15 2019

Swale 2: Catchment 201 Service Easement Swale to Dry Pond

Triangular

Side Slopes (z:1) = 3.0000, 3.0000
Total Depth (m) = 0.3500

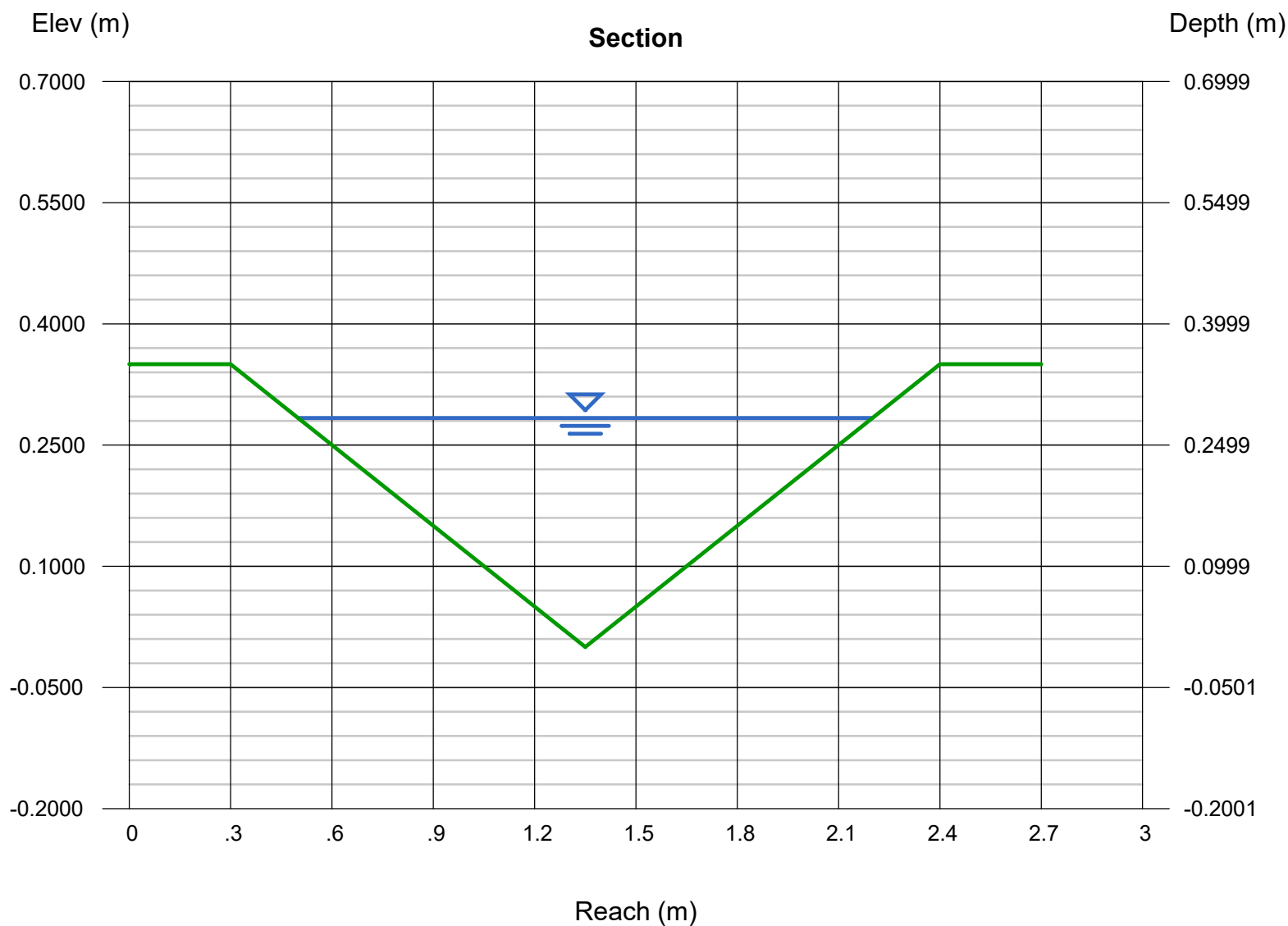
Invert Elev (m) = 0.0001
Slope (%) = 2.0000
N-Value = 0.035

Calculations

Compute by: Known Q
Known Q (cms) = 0.2490

Highlighted

Depth (m) = 0.2835
Q (cms) = 0.249
Area (sqm) = 0.2411
Velocity (m/s) = 1.0330
Wetted Perim (m) = 1.7928
Crit Depth, Yc (m) = 0.2713
Top Width (m) = 1.7008
EGL (m) = 0.3379



Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Jan 15 2019

Swale 3: Catchment 204 Grass Swale to North

Triangular

Side Slopes (z:1) = 3.0000, 3.0000
Total Depth (m) = 0.3000

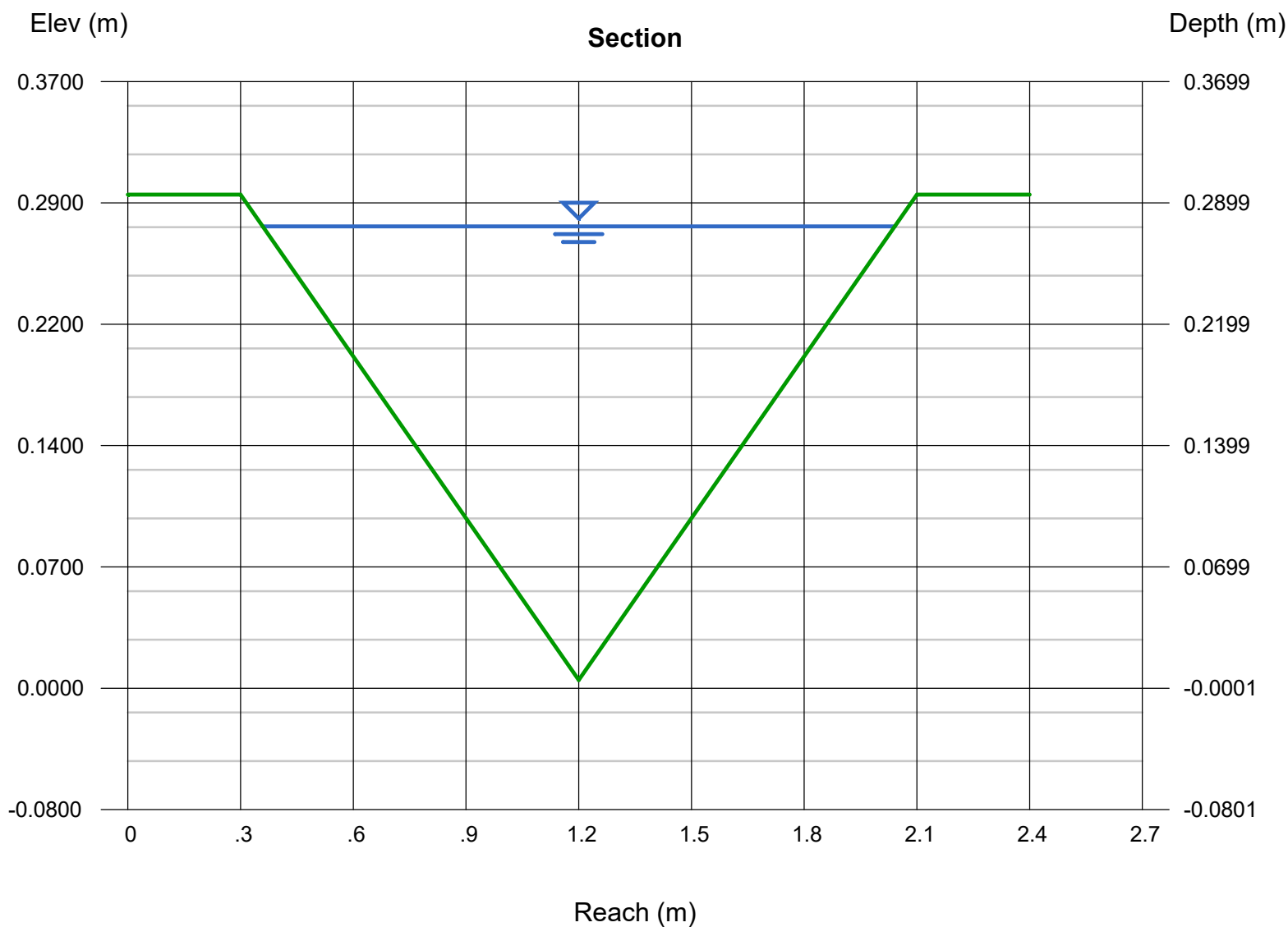
Invert Elev (m) = 0.0001
Slope (%) = 2.4000
N-Value = 0.035

Calculations

Compute by: Known Q
Known Q (cms) = 0.2700

Highlighted

Depth (m) = 0.2804
Q (cms) = 0.270
Area (sqm) = 0.2359
Velocity (m/s) = 1.1446
Wetted Perim (m) = 1.7735
Crit Depth, Yc (m) = 0.2804
Top Width (m) = 1.6825
EGL (m) = 0.3472



Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Jan 15 2019

Swale 4: Catchment 205 Overland Flow Swale to Wet Pond

Trapezoidal

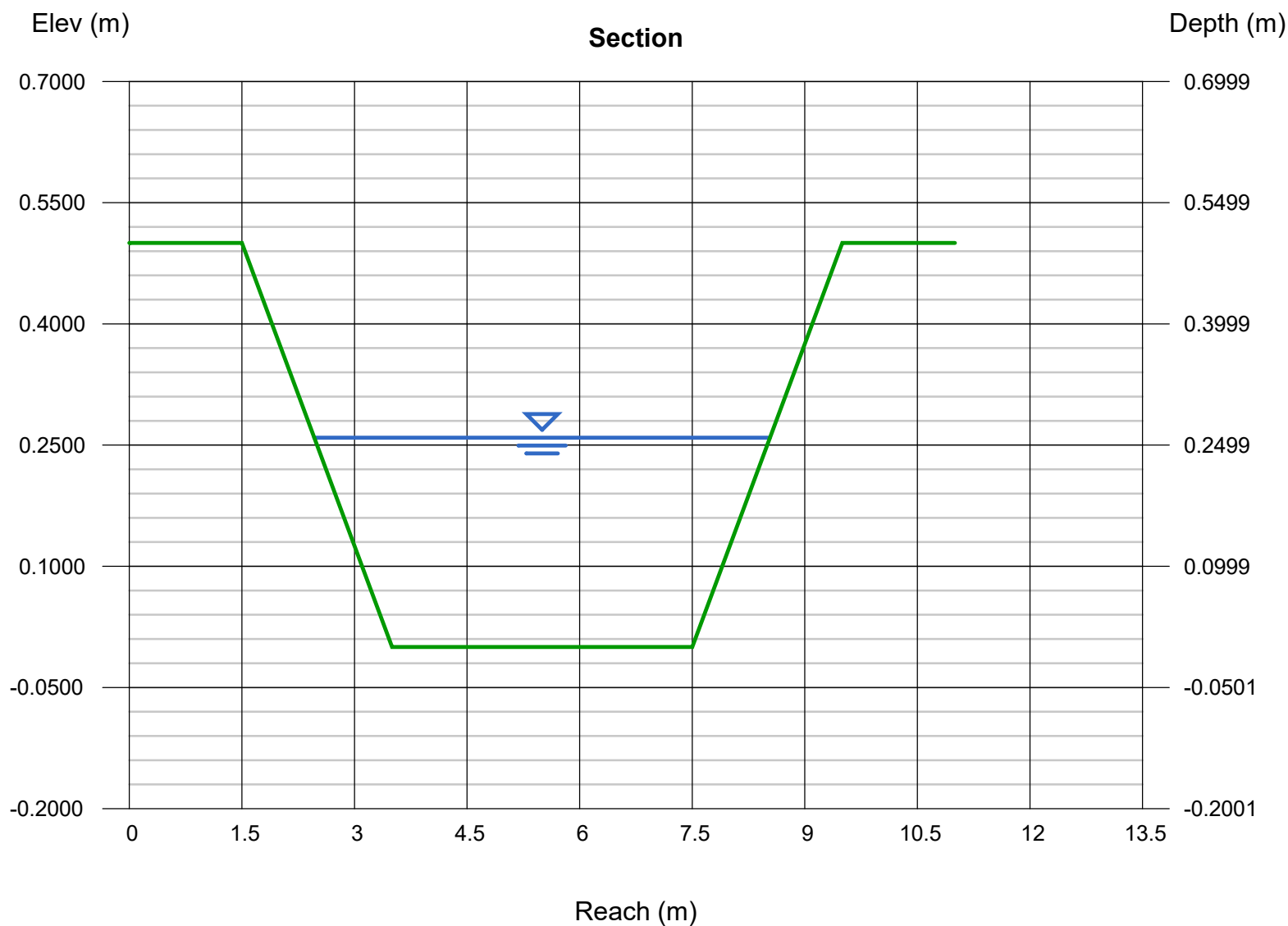
Bottom Width (m) = 4.0000
Side Slopes (z:1) = 4.0000, 4.0000
Total Depth (m) = 0.5000
Invert Elev (m) = 0.0001
Slope (%) = 2.0000
N-Value = 0.035

Calculations

Compute by: Known Q
Known Q (cms) = 1.8500

Highlighted

Depth (m) = 0.2591
Q (cms) = 1.8500
Area (sqm) = 1.3048
Velocity (m/s) = 1.4178
Wetted Perim (m) = 6.1364
Crit Depth, Yc (m) = 0.2560
Top Width (m) = 6.0726
EGL (m) = 0.3616



APPENDIX F: WATER QUALITY CALCULATIONS

BlueVista Subdivision

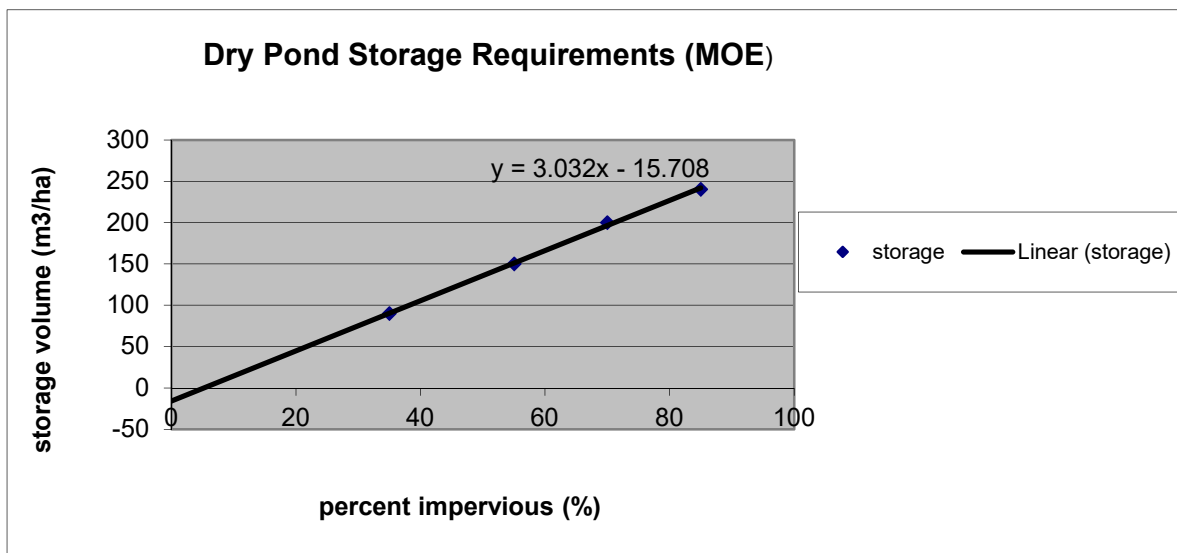
FILE No. 117159

Nov-18

MOE Manual Storage Requirements

Dry Pond

% imp	storage
35	90
55	150
70	200
85	240



% imp	50	
Storage Volume (m ³ /ha)	135.892	
Drainage Area (ha)	1.56	
Required Storage Volume (m³)	212	
Provided Storage Volume (m³)	512	ok

BlueVista Subdivision

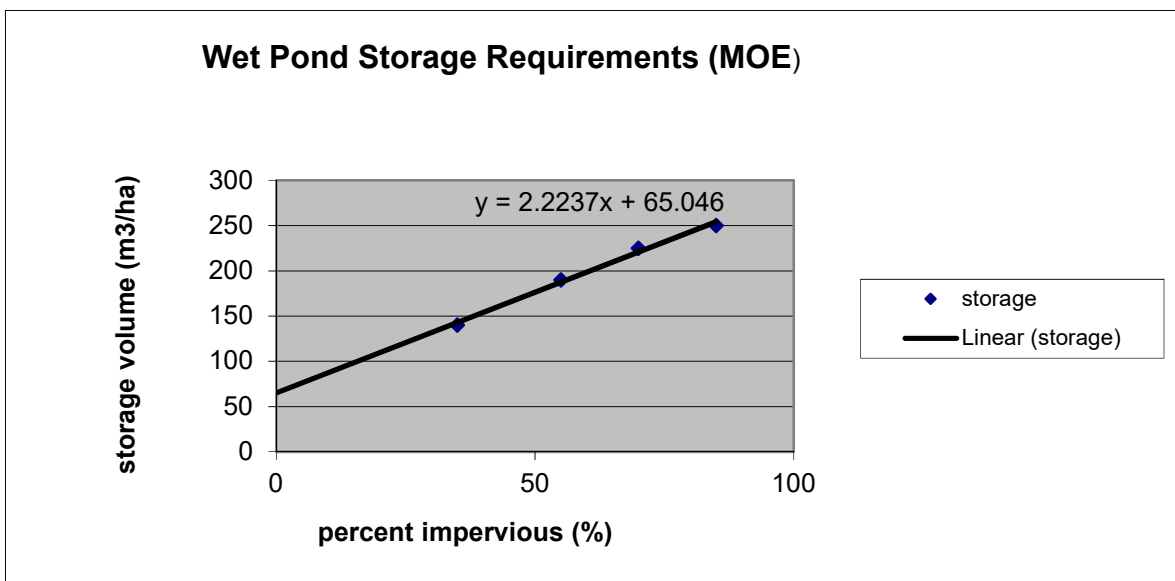
FILE No. 117159

Nov-18

MOE Manual Storage Requirements

Wet Pond

% imp	storage
35	140
55	190
70	225
85	250



% imp	50	
Storage Volume (m³/ha)	176	
Drainage Area (ha)	11.14	
Storage Volume (m³)	1961	
Permanent Pool Volume (m³)	1515	
Provided Permanent Pool Volume (m³)	3112	ok
Active Storage Volume (m³)	446	
25 mm Storm Runoff (mm)	11.855	
25 mm Storm Runoff Volume (m³)	1321	
Required Extended Detention Storage (m³)	1321	
Provided Extended Detention Storage (m³)	3963	ok



C.C. Tatham & Associates Ltd.

Consulting Engineers

Collingwood

Bracebridge

Orillia

Barrie

Project: BlueVista Subdivision

Date: December 2018

File No.: 117159

Designed: ARO

Subject: Erosion Control Calculations

Checked: DRT

SIMPLIFIED APPROACH (AS PER MOE-SWMPPD MANUAL SECTION C.4)

Catchments:	201	
Total Area (ha):	1.56 ha	
Total Directly Connected Impervious Area:	50%	
SCS Soil Group	A&B	
Source Control (m ³):	0	
Required Pond Active Storage Volume (m ³ /ha):	225	*Fig. C1 MOE SWM Manual
Active Storage Volume Required (m ³):	351	
Active Storage Volume Provided (m ³):	512	*Active Storage Volume Controlled by Minor Orifice
Therefore, the Storage Volume provided is greater than required.		



C.C. Tatham & Associates Ltd.

Consulting Engineers

Collingwood

Bracebridge

Orillia

Barrie

Project: BlueVista Subdivision

Date: December 2018

File No.: 117159

Designed: ARO

Subject: Erosion Control Calculations

Checked: DRT

SIMPLIFIED APPROACH (AS PER MOE-SWMPPD MANUAL SECTION C.4)

Catchments:	205	
Total Area (ha):	11.14 ha	
Total Directly Connected Impervious Area:	50%	
SCS Soil Group	A&B	
Source Control (m ³):	0	
Required Pond Active Storage Volume (m ³ /ha):	225	*Fig. C1 MOE SWM Manual
Active Storage Volume Required (m ³):	2,507	
Active Storage Volume Provided (m ³):	3,963	*Active Storage Volume Controlled by Minor Orifice
Therefore, the Storage Volume provided is greater than required.		

**C.C. Tatham & Associates Ltd.**

Consulting Engineers

Collingwood Bracebridge Orillia Barrie Ottawa

Project: BlueVista Subdivision

Date: November 2018

File No.: 117159

Designed: ARO

Subject: Water Quality Calculations

Checked: DRT

$$TSS\ Removal = 1 - [(1 - R_p) - (1 - R_p)R_s]$$

where:

 R_p = % TSS Removal provided by Primary Treatment Strategy R_s = % TSS Removal provided by Secondary Treatment Strategy**Catchment 201**

Drainage Area = 1.56 ha Imperviousness = 50%

Controls:

Device	Target Total Suspended Solids (TSS) Removal
Split Primary Treatment Grass Swale	50% *
Split Primary Treatment OGS Unit **	50% ***
Secondary Treatment Dry Pond	60%

* Chapter 4.8 Low Impact Development Stormwater Management Planning and Design Guide, CVC 2011.

** Oil-Grit Separator (OGS)

*** Unit Sized to provide 80% TSS removal, safety factor applied

TSS Removal Provided By Controls = 80%

Catchment 203

Drainage Area = 0.33 ha Imperviousness = 45%

Controls:

Device	Target Total Suspended Solids (TSS) Removal
Primary Treatment *	0%
Secondary Treatment **	0%

* No primary treatment recommended

** No secondary treatment recommended

TSS Removal Provided By Controls = 0%

Catchment 205

Drainage Area = 11.14 ha Imperviousness = 50%

Controls:

Device	Target Total Suspended Solids (TSS) Removal
Primary Treatment Impervious to Grass	50%
Secondary Treatment Wet Pond	80%

TSS Removal Provided By Controls = 90%

Site TSS Removal Efficiency

Catchment	Outlet	Area (ha)	TSS Removal
201	Outlet 1	1.56	80%
203	Outlet 1	0.33	0%
205	Outlet 2	11.14	90%

TSS Removal Provided By Controls = 87%

* Discharge from Catchments 202, and 204 are considered clean and do not require quality treatment.

Detailed Stormceptor Sizing Report – Blue Mountains

Project Information & Location			
Project Name	Blue Mountains	Project Number	-
City	Blue Mountains	State/ Province	Ontario
Country	Canada	Date	11/22/2018
Designer Information		EOR Information (optional)	
Name	Brandon O'Leary	Name	Alysse Overholt
Company	Forterra	Company	C.C. Tatham & Associates Ltd.
Phone #	905-630-0359	Phone #	
Email	brandon.oleary@forterrabp.com	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Blue Mountains
Recommended Stormceptor Model	EFO8
TSS Removal (%) Provided	84
PSD	Fine Distribution
RainFall Station	OWEN SOUND MOE

The recommended Stormceptor model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

EFO Sizing Summary			
EFO Model	% TSS Removal Provided	% Runoff Volume Captured Provided	Standard EFO Hydrocarbon Storage Capacity
EFO4	67	76	265 L (70 gal)
EFO6	78	89	610 L (160 gal)
EFO8	84	96	1070 L (280 gal)
EFO10	88	98	1670 L (440 gal)
EFO12	90	99	2475 L (655 gal)
Parallel Units / MAX	Custom	Custom	Custom

OVERVIEW

Stormceptor® EF is a continuation and evolution of the most globally recognized oil-grit separator (OGS) stormwater treatment technology - **Stormceptor®**. Also known as a hydrodynamic separator, the enhanced flow Stormceptor EF is a high performing oil-grit separator that effectively removes a wide variety of pollutants from stormwater and snowmelt runoff at higher flow rates as compared to the original Stormceptor. Stormceptor EF captures and retains sediment (TSS), free oils, gross pollutants and other pollutants that attach to particles, such as nutrients and metals. Stormceptor EF's patent-pending treatment and scour prevention technology and internal bypass ensures sediment is retained during all rainfall events.

Design Methodology

Stormceptor is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology using local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective. The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. The Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing:

- Site parameters
- Continuous historical rainfall data, including duration, distribution, peaks & inter-event dry periods
- Particle size distribution, and associated settling velocities (Stokes Law, corrected for drag)
- TSS load
- Detention time of the system

Hydrology Analysis			
PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of Stormceptor are based on the average annual removal of TSS for the selected site parameters. The Stormceptor is engineered to capture sediment particles by treating the required average annual runoff volume, ensuring positive removal efficiency is maintained during each rainfall event, and preventing negative removal efficiency (scour). Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.			
Rainfall Station			
State/Province	Ontario	Total Number of Rainfall Events	4492
Rainfall Station Name	OWEN SOUND MOE	Total Rainfall (mm)	18531.0
Station ID #	6132	Average Annual Rainfall (mm)	463.3
Coordinates	44°35'N, 80°56'W	Total Evaporation (mm)	912.7
Elevation (ft)	580	Total Infiltration (mm)	9225.3
Years of Rainfall Data	40	Total Rainfall that is Runoff (mm)	8393.0
Notes			
• Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules. • Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed. • For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.			

ONLINE APPLICATION

Stormceptor EF's internal bypass and patent-pending scour prevention technology has demonstrated very effective retention of pollutants in third-party testing and verification following the Canadian ETV's **Procedure for Laboratory Testing of Oil-Grit Separators**. Sediment scour prevention demonstrated an effluent concentration of less than 10 mg/L for sediment particles ranging from 1 to 1,000 microns, even during peak influent flow rates associated with infrequent high intensity storm events. While Stormceptor EF will capture oil, only the Stormceptor EFO configuration has been third-party tested and verified to retain greater than 99% of captured oil. Based on these verified performance attributes, the most efficient and widely accepted application of Stormceptor EF is an online configuration, which allows all upstream conveyance flows to enter and exit the unit. The online application eliminates the need for costly additional bypass structures, piping and installation expense.

FLOW ENTRANCE OPTIONS

Single Inlet Pipe – A common design which includes one inlet pipe and one outlet pipe. A 90-degree (maximum) bend is also accepted with this configuration.

Inlet Grate – Allows surface runoff to enter the unit from grade. The inlet grate option can also be used in conjunction with one inlet pipe or multiple inlet pipes. A removable flow deflector is added in the Stormceptor EF4/EFO4.

Maximum Pipe Diameter		
Model	Inlet (In/mm)	Outlet (In/mm)
EF4 / EFO4	24 / 610	24 / 610
EF6 / EFO6	36 / 915	36 / 915
EF8/ EFO8	48 / 1220	48 / 1220
EF10/EFO10	72 / 1828	72 / 1828
EF12/EFO12	72 / 1828	72 / 1828

Multiple Inlet Pipe – Allows for multiple inlet pipes of various diameters to enter the unit.

Maximum Pipe Diameter		
Model	Inlet (In/mm)	Outlet (In/mm)
EF4 / EFO4	18 / 457	24 / 610
EF6 / EFO6	30 / 762	36 / 915
EF8/ EFO8	42 / 1067	48 / 1220
EF10/EFO10	60 / 1524	72 / 1828
EF12/EFO12	60 / 1524	72 / 1828

Drainage Area	
Total Area (ha)	1.64
Imperviousness %	50

Up Stream Storage	
Storage (ha-m)	Discharge (cms)
0.000	0.000

Up Stream Flow Diversion	
Max. Flow to Stormceptor (cms)	

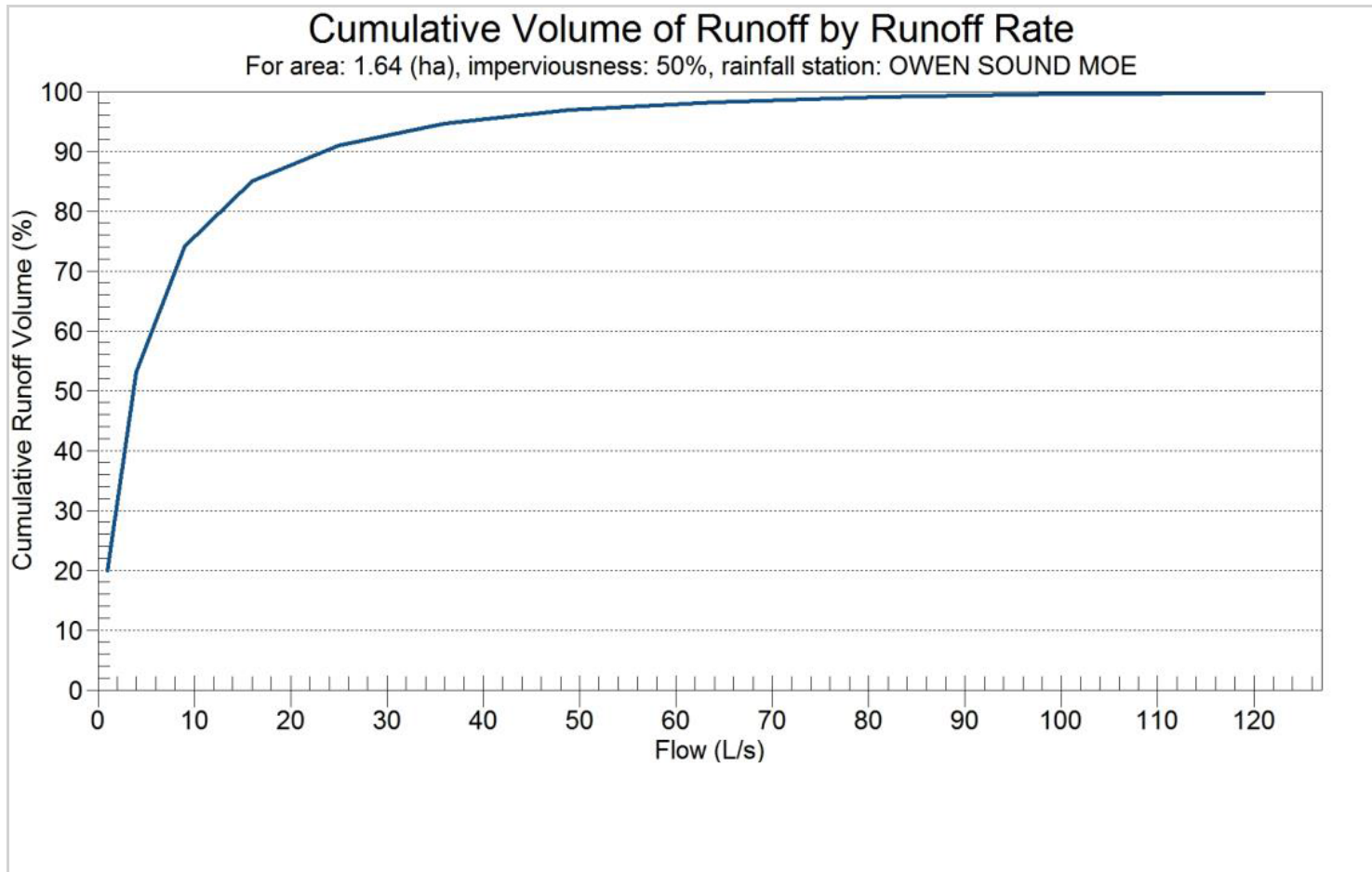
Water Quality Objective	
TSS Removal (%)	80.0
Runoff Volume Capture (%)	90.00
Oil Spill Capture Volume (L)	
Peak Conveyed Flow Rate (L/s)	
Water Quality Flow Rate (L/s)	

Design Details	
Stormceptor Inlet Invert Elev (m)	
Stormceptor Outlet Invert Elev (m)	
Stormceptor Rim Elev (m)	
Normal Water Level Elevation (m)	
Pipe Diameter (mm)	
Pipe Material	
Multiple Inlets (Y/N)	No
Grate Inlet (Y/N)	No

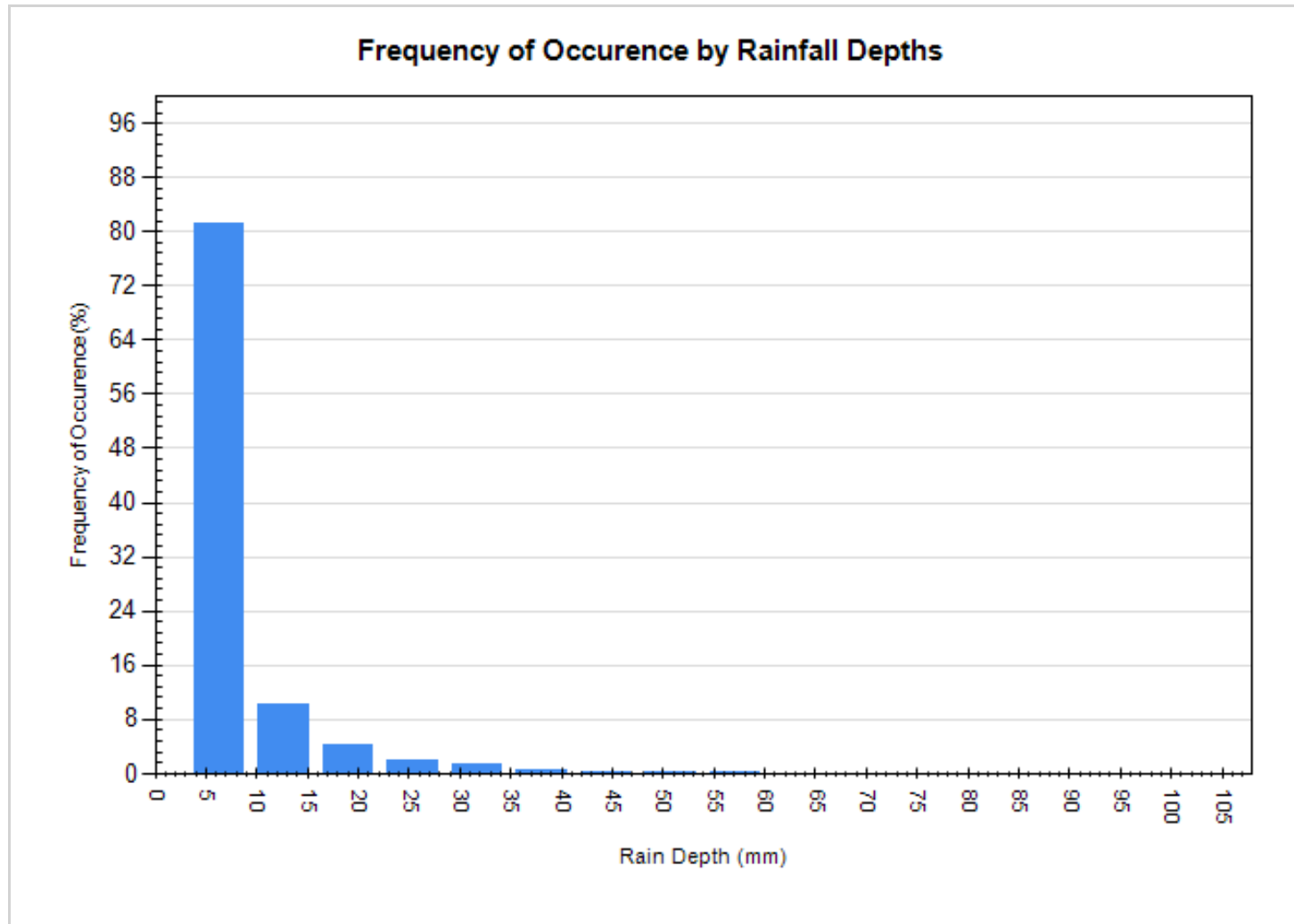
Particle Size Distribution (PSD)		
Removing the smallest fraction of particulates from runoff ensures the majority of pollutants, such as metals, hydrocarbons and nutrients are captured. The table below identifies the Particle Size Distribution (PSD) that was selected to define TSS removal for the Stormceptor design.		
Fine Distribution		
Particle Diameter (microns)	Distribution %	Specific Gravity
20.0	20.0	1.30
60.0	20.0	1.80
150.0	20.0	2.20
400.0	20.0	2.65
2000.0	20.0	2.65

Site Name		Blue Mountains	
Site Details			
Drainage Area		Infiltration Parameters	
Total Area (ha)	1.64	Horton’s equation is used to estimate infiltration	
Imperviousness %	50	Max. Infiltration Rate (mm/hr)	61.98
Oil Spill Capture Volume (L)		Min. Infiltration Rate (mm/hr)	10.16
		Decay Rate (1/sec)	0.00055
		Regeneration Rate (1/sec)	0.01
Surface Characteristics		Evaporation	
Width (m)	256.00	Daily Evaporation Rate (mm/day)	2.54
Slope %	2	Dry Weather Flow	
Impervious Depression Storage (mm)	0.508	Dry Weather Flow (lps)	0
Pervious Depression Storage (mm)	5.08		
Impervious Manning’s n	0.015		
Pervious Manning’s n	0.25		
Maintenance Frequency		Winter Months	
Maintenance Frequency (months) >	12	Winter Infiltration	0
TSS Loading Parameters			
TSS Loading Function		Build Up/ Wash-off	
Buildup/Wash-off Parameters		TSS Availability Parameters	
Target Event Mean Conc. (EMC) mg/L	125	Availability Constant A	0.057
Exponential Buildup Power	0.40	Availability Factor B	0.04
Exponential Washoff Exponent	0.20	Availability Exponent C	1.10
		Min. Particle Size Affected by Availability (micron)	400

Cumulative Runoff Volume by Runoff Rate			
Runoff Rate (L/s)	Runoff Volume (m³)	Volume Over (m³)	Cumulative Runoff Volume (%)
1	27733	110709	20.0
4	73526	64922	53.1
9	102611	35848	74.1
16	117729	20714	85.0
25	126035	12410	91.0
36	130960	7481	94.6
49	134109	4334	96.9
64	135992	2449	98.2
81	137094	1347	99.0
100	137680	760	99.5
121	138080	361	99.7
144	138277	164	99.9
169	138350	91	99.9
196	138396	45	100
225	138430	11	100
256	138441	0	100
289	138441	0	100



Rainfall Event Analysis				
Rainfall Depth (mm)	No. of Events	Percentage of Total Events (%)	Total Volume (mm)	Percentage of Annual Volume (%)
6.35	3645	81.1	5719	30.9
12.70	458	10.2	4102	22.1
19.05	191	4.3	2957	16.0
25.40	89	2.0	1936	10.5
31.75	57	1.3	1599	8.6
38.10	23	0.5	800	4.3
44.45	12	0.3	501	2.7
50.80	10	0.2	472	2.5
57.15	4	0.1	219	1.2
63.50	1	0.0	63	0.3
69.85	0	0.0	0	0.0
76.20	0	0.0	0	0.0
82.55	1	0.0	79	0.4
88.90	1	0.0	84	0.5
95.25	0	0.0	0	0.0
101.60	0	0.0	0	0.0



For Stormceptor Specifications and Drawings Please Visit:
<http://www.imbriumsystems.com/technical-specifications>

SECOND NATURE DEVELOPMENT (PHASE 3)

WINDFALL DEVELOPMENT (PHASE 4B)

LA SCANDINAVE SPA

MONTERRA GOLF COURSE

BLUE VISTA

GSCA WATERSHED

NVCA WATERSHED

INTERMITTENT TRIBUTARY

GREY ROAD 21 (OSLER BLUFF ROAD)

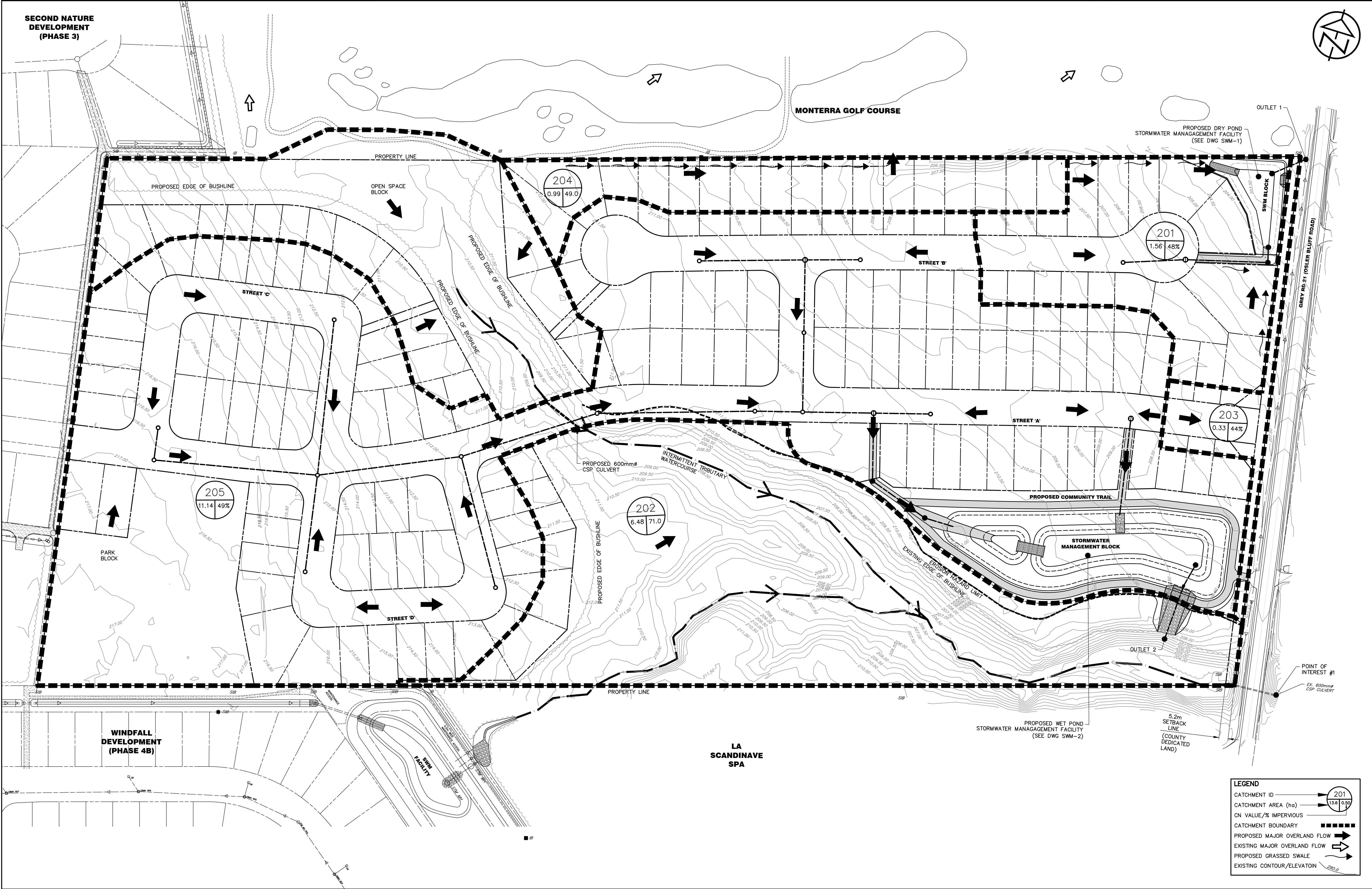
POINT OF INTEREST #1

EX. 600mm CSP CULVERT

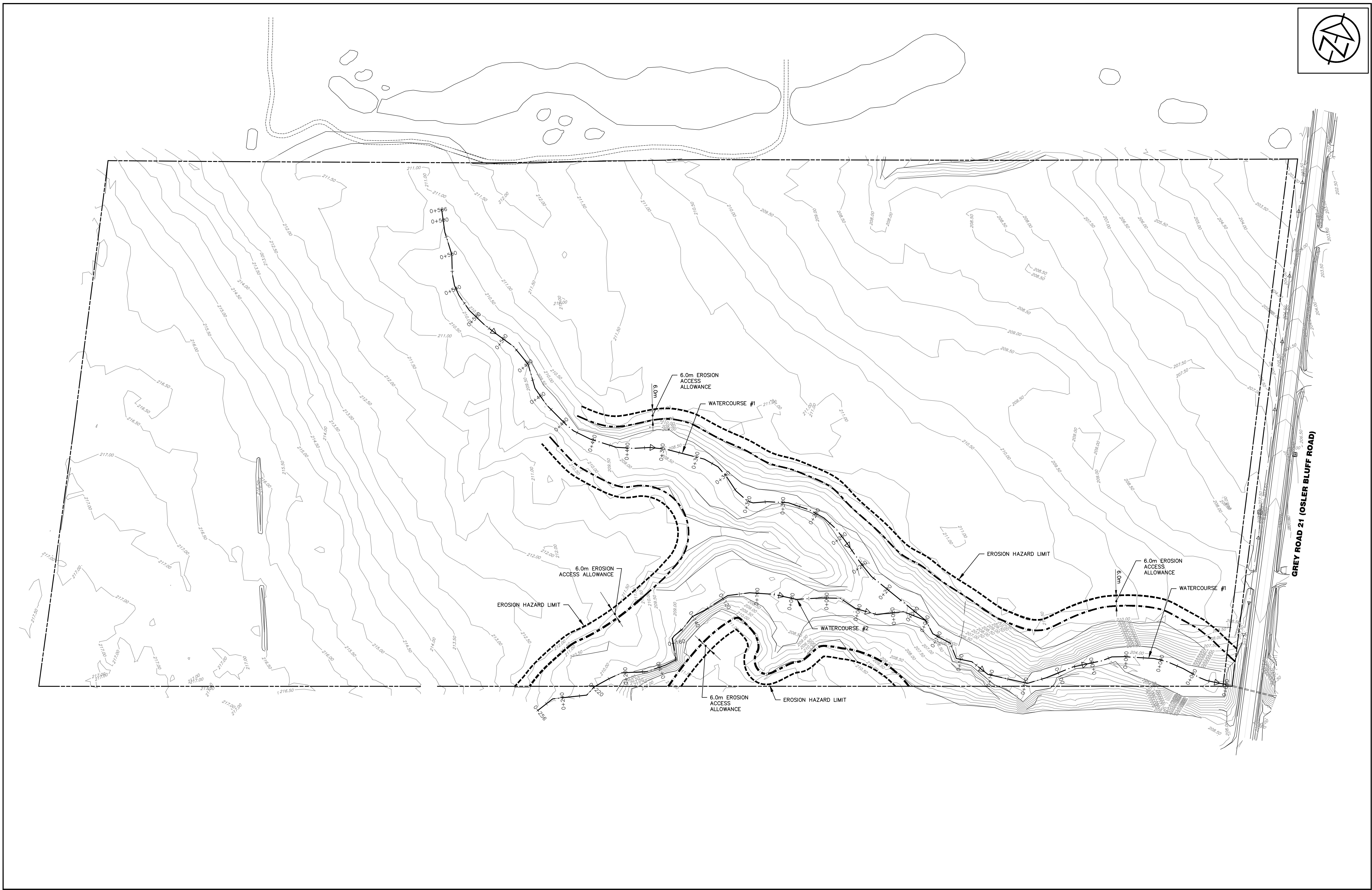
LEGEND

- CATCHMENT ID: 201
- CATCHMENT AREA (ha): 13.6
- CN VALUE: 59
- CATCHMENT BOUNDARY: Dashed line
- EXISTING MAJOR OVERLAND FLOW: Arrow
- EXISTING CONTOUR/ELEVATION: Solid line

DWG. **DP-1**



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1.		DRAFT PLAN APPROVAL		FEB/19		RS		SCALE: 1:1,000		JOB NO. 117159	
NO.		REVISIONS		DATE		INITIAL		DESIGN: DRT		CHECKED: DRT	
								DRAWN: DEP/RD		DATE: APRIL/18	
										DWG. DP-2	



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NO.	REVISIONS	DATE	INITIAL

APPROVED

PRELIMINARY

BLUE VISTA
TOWN OF THE BLUE MOUNTAINS

NATURAL HAZARDS PLAN



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie Ottawa

SCALE: 1:1,000

JOB NO. 117159

DESIGN: DRT

CHECKED:	DRT
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DRAWN: DEP

DATE:	APRIL/18
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DWG. **HAZ-2**

DWG. **HAZ-2**